

Communications

R.J. Marks II Class Notes

Professor Hal Sabbaugh

Text: Wozencraft & Jacobs

Rose-Hulman Institute of Technology (1971)

COMMUNICATION SYSTEMS

COMMUNICATION SYSTEMS

3-19-71

MON 2:12, 2:23, 2:24

COMM PROB
EX ON 78

(3.4 3.5) 3.4 3.6 3.7 3.8

CORP. REC.

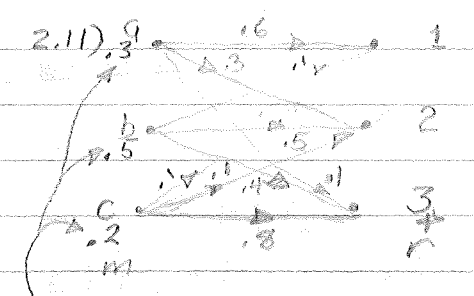
ALL OF CHAPT. 4 MATCHED FILTER

SKIP CHAPT. 5, 6

CHAPT 7: 1, 2

CHAPT 8: 1, 2, 3, 5

LECTURE



APPRIORI PROB = PROB. THAT a, b, c WERE SENT AFTER HEARING A 1, 2, 3

$P[m_k]$ = APPRIORI PROB. OF k^{th} MESSAGE

$P[r_j | m_k]$ = CONDITIONAL PROB OF RECEIVING THE j^{th} r GIVEN OR CONDITIONED UPON TRANSMITTING THE k^{th} MESSAGE

$P[m_k]P[r_j | m_k] = P[m_k, r_j] = P[m_k | r_j]P[r_j]$
 $P[m_k, r_j]$ = PROB. OF THE JOINT EVENT m_k TRANSMITTED AND r_j IS RECEIVED (APOSTERIORI PROB) (CONDITIONAL)

▷ BAYES RULE

$$P[m_k | r_j] = \frac{P[m_k, r_j]}{P[r_j]}$$

3-19-71

MON 2:12, 2:23, 2:24

COMM PROB EX ON 78
CORP. REC

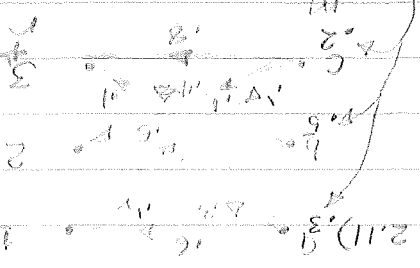
ALL OF CHAPT 11 MATCHED FILTER

SKIP CHAPT 5, 6

CHAPT 7, 2

CHAPT 8: 1, 2, 3, 5

LECTURE



APRIORI PROB = PROB. THAT a, b, c WERE

SENT AFTER HEARING A 1, 2, 3

$P[m_k] =$ APRIORI PROB. OF k^{th} MESSAGE

$P[r_j/m_k] =$ CONDITIONAL PROB

OF RECEIVING THE j^{th} r GIVEN

OR CONDITIONED UPON TRANSMITTING

THE k^{th} MESSAGE

$$(P[m_k]P[r_j/m_k]) = P[m_k, r_j] = P[m_k/r_j]P[r_j]$$

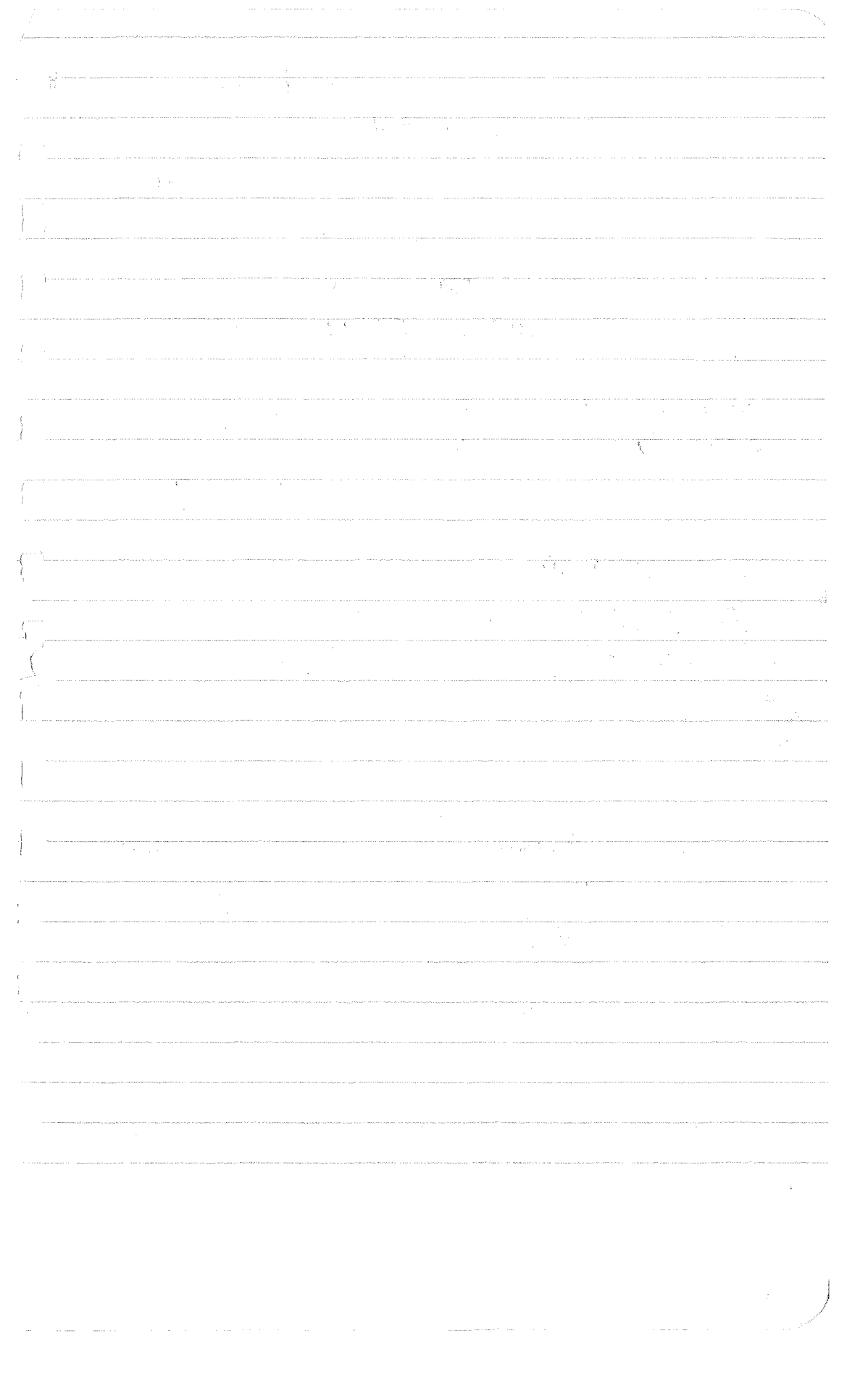
$P[m_k, r_j] =$ PROB. OF THE JOINT

EVENT m_k TRANSMITTED AND

r_j IS RECEIVED (APRIORI PROB)

BAYES RULE

$$P[m_k|r_j] = \frac{P[m_k, r_j]}{P[r_j]}$$



$\hat{m}(1,3) = a$
 $\hat{m}(2,3) = b$
 $\hat{m}(3,3) = b$
 c) b DOMINATES $\Rightarrow P[E] = .50$
 b) $P[C] = .18 + .25 + .20 = .63 \Rightarrow P[E] = .37$

- $\hat{m}(1) = a$ (.18)
- $\hat{m}(2) = b$ (.25)
- $\hat{m}(3) = b$ (.20)

RECEIVER DECISION RULE

$P[3] = .39$
 $P[1, a] = .18; P[1, b] = .05$
 $P[2, a] = .09; P[2, b] = .25$
 $P[3, a] = .03; P[3, b] = .20$
 $P[1, c] = .02; P[2, c] = .02; P[3, c] = .16$
 $= .36$

$P[r_j] = P[r_j, m_1] + P[r_j, m_2] + P[r_j, m_3]$
 $P[1] = P[1, a] + P[1, b] + P[1, c]$
 $P[2] = P[2, a] + P[2, b] + P[2, c]$
 $P[3] = P[3, a] + P[3, b] + P[3, c]$
 $= (.3)(.3) + (.5)(.5) + (.2)(.1)$

MAXIMIZING \Rightarrow MAXIMIZING $P[r_j/m_k]$

$$P[m_k, r_j] = \frac{P[r_j]}{P[m_k] P[r_j/m_k]}$$

WANT VALUE OF m_k TO MAX. $P[m_k/r_j]$

$$P[m_k/r_j] = \frac{P[m_k, r_j]}{P[r_j]}$$

7

1

2

3

4

5

6

7

8

9

0

1

2

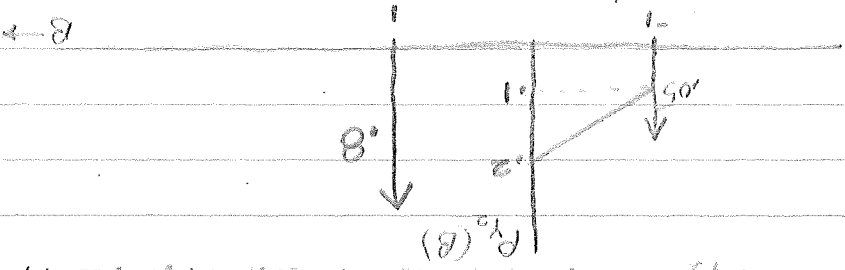
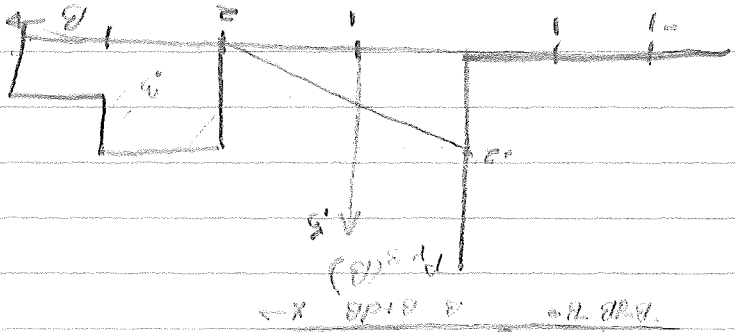
3

4

5

6

7

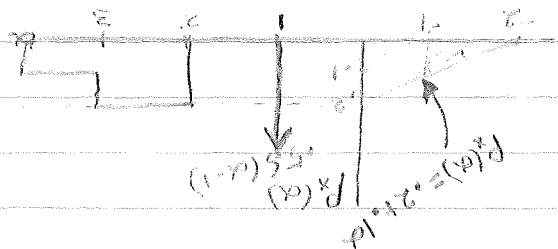
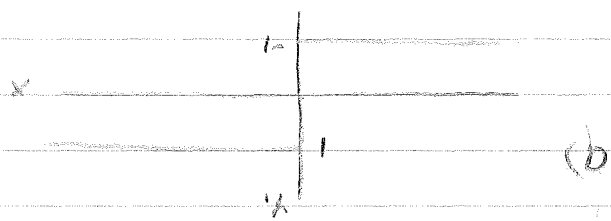


$$R_0(B) = 0.5 \delta(B+1) + 0.8 \delta(B-1) + 2 + 1.8$$

$-1 < B < 0$

FOR $-1 < B < 0$, $R_0(B) = 2 + 1.8$

$$R_1(B) = 2.5(B+1) + 0.8 \delta(B-1)$$



2.18

$$R_0(A) = 2 + 1.8$$

()

()

()

()

()

()

()

()

()

()

()

()

()

()

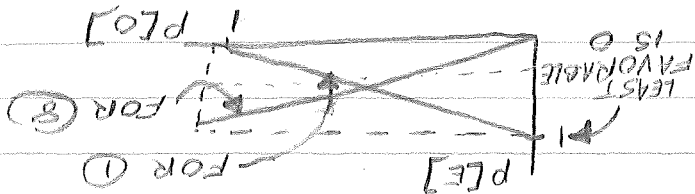
()

()

()

()

$$P[E^c] = P[0]$$



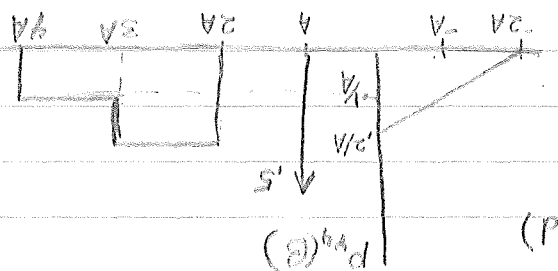
$$P[E^c] = 1 - P[0]$$

HINT: $(0,0,0)$ $P[C] = P[0]$ WAS TRANSFERRED
& PROB. OF MAKING CORR. CHOICE

$$2,1,2) (a,b,c) = (0,0,0), (0,0,1), \dots, (1,1,1)$$

3-23-71

$$P_{15}(B) = .15(B-1) + .15(B-2) + .15(B-3) + .05(B-4) + .0875(B-4) + .15(B+1) + .0125(B+2)$$



$$\boxed{p_n(p-s) = (p-s)p_n} \Rightarrow p_n(p-s) = p_n(p-s)$$

\Rightarrow $U = \text{IND OF } n$

$$= p_n(p-s) = p_n(p-s) \\ = p_n(p-s) = p_n(p-s) \\ = p_n(p-s) = p_n(p-s)$$

$$\Rightarrow p_r(p/m) > p_l(m) \Rightarrow p_r(p/m) > p_l(m)$$

$$p_l(m) = p_r(p/m) = p_l(m)$$

WANT TO MAXIMIZE A POSTERIORI PRP.

OF RANDOM EVENT
EVENT M

JOINT DISTRIBUTION
FUNCTION

$$= p(p, m)$$

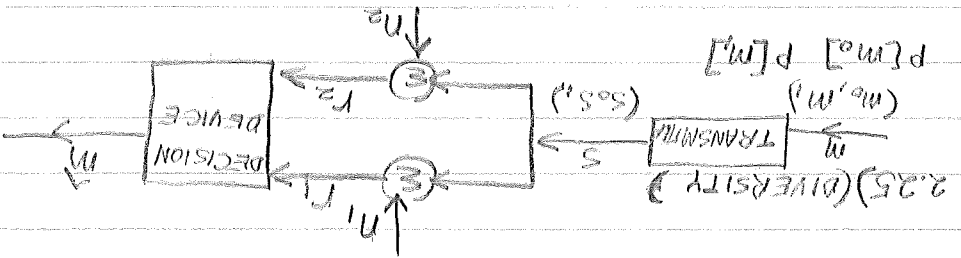
$$p_r(p/m) = p_l(m) = p_l(m)$$

BAYES MIXED RULE:

$$r_1 = s + n_1, r_2 = s + n_2$$

$$E E = \text{ENERGY} \propto V^2$$

$$s_0 = (-1)^0 V = V, s_1 = (-1)^1 V = -V$$



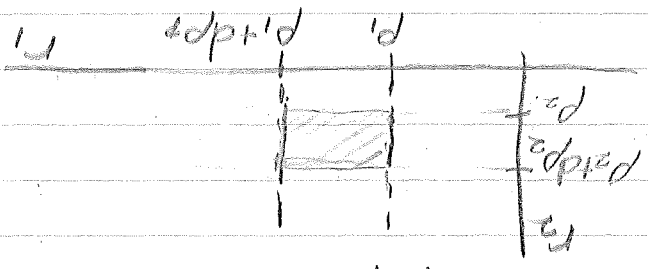
WE MUST EXAMINE THE TWO VARIABLE CASE



WANT $P[m_0/n = p_1, r_2 = p_2]$

$P[m_0/n = p_1, r_2 = p_2] > P[m_1/n = p_1, r_2 = p_2]$

$\Rightarrow P_{r_1, r_2}(p_1, p_2 | m_0) > P_{r_1, r_2}(p_1, p_2 | m_1)$



BY ANALOGY

$P_{r_1, r_2}(p_1 | m_1) = P_{r_1, r_2}(p_2 | m_2)$

$(n_1 \frac{1}{2} p_2 \text{ INP FROM } m_2)$

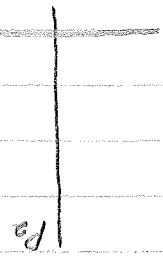
$= P_{r_1}(p_1 | s_1) P_{r_2}(p_2 | s_2)$

$\frac{1}{(p_2 - s_2)^2 / 20^2} e^{-\frac{2\pi \theta_2}{20^2}}$

$P_{r_2}(p_2 | s_2) = \frac{1}{\sqrt{20^2}} e^{-\frac{p_2 - s_2}{\sqrt{20^2}}}$

$P_{r_2}(p_1 | s_2) P_{r_1}(p_2 | s_1) = \frac{1}{(p_2 - s_2)^2 + (p_1 + s_1)^2} e^{-\frac{2\pi \theta_2}{20^2}}$

$P_{r_1, r_2}(p_1, p_2 | m_1) P_{r_1, r_2}(p_1, p_2 | m_2) = \frac{1}{2\pi \theta_1 \theta_2} e^{-\frac{2\pi \theta_1 \theta_2}{20^2}}$



At $p_1 = p_2$

$$P(m_0) = \frac{1}{2\pi\sigma^2} \int [(p_1 - s_0)^2 + (p_2 - s_0)^2] P(p_1, p_2) P(m_0) = \frac{1}{2\pi\sigma^2} \int \frac{1}{\sigma^2} e^{-\frac{1}{2\sigma^2} [(p_1 - s_0)^2 + (p_2 - s_0)^2]} P(p_1, p_2) P(m_0)$$

ALL THAT IS NEEDED IS EXPONENTS

$$(p_1 - s_0)^2 + (p_2 - s_0)^2 > (p_1 - s_1)^2 + (p_2 - s_1)^2$$

$$P(m_0) = P(m_1) \Rightarrow s_0 = s_1$$

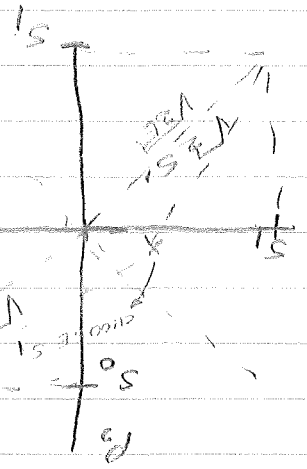
FOR GAUSSIAN NOISE,

WILL CHOOSE SIGNAL

CLOSEST TO VOLTAGE

$$s_0 = \sqrt{E} \quad p_1$$

DECISION BOUNDARY

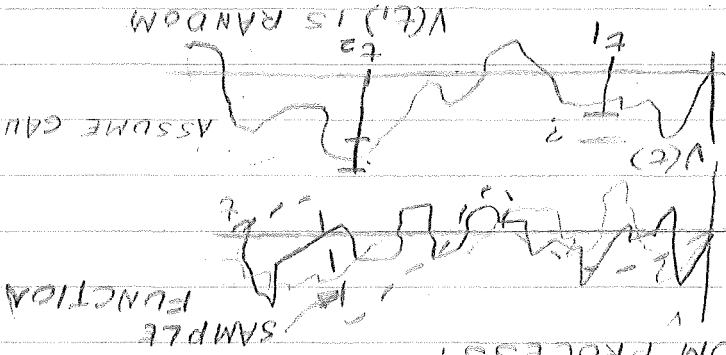


THE FARTHER APART THE POINTS,
THE BETTER THE DECISION,

3-27-71

CHART, 3

RANDOM PROCESS:



$$p_{x(t)}(a, t_1)$$

SINGLE VAR. = $v(a, t_1)$

$$p_{x(t_1), x(t_2)}(a_1, a_2)$$

$$p_{x(t_1), \dots, x(t_n)}(a_1, \dots, a_n)$$

IF EACH IS GAUSSIAN & IS GAUSSIAN

IF p IS DEPENDENT ONLY ON Δt ,

SYSTEM IS STATIONARY

NEED ONLY X_2 & X TO DEFINE

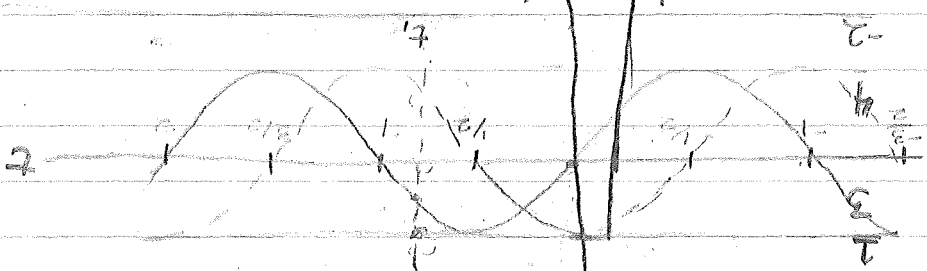
GAUSSIAN PRODUCT

READ: 3.1, 3.2, 3.4, 3.5

3.1 $x(w_1 t) = 1$ $x(w_2 t) = 2$ $x(w_3 t) = \sin \pi t$

$x(w_4 t) = 2$ $x(w_4 t) = \sin \pi t$

$x(t, w_3)$



a) $P[w_1] = \frac{1}{2} A$

$P_x(t_1)(\alpha) = \frac{1}{4} \delta(\alpha-1) + \frac{1}{4} \delta(\alpha+2)$

$+ \frac{1}{4} \delta(\alpha - \sin \pi t_1) + \frac{1}{4} \delta(\alpha - \cos \pi t_1)$

$P_x(t_1)(\alpha) = \int_{-\infty}^{\infty} \alpha P_x(t) (\alpha) d\alpha$

$= \frac{1}{4} (1 - 2 + \sin \pi t + \cos \pi t)$

$x(t_1)x(t_2) = \int_{-\infty}^{\infty} \alpha \beta P_x(t_1)x(t_2) d\alpha d\beta$

$= R(t_1, t_2) = \text{CORRELATION FUNC.}$

TO CALCULATE: $P_x(t_1)x(t_2)$

$= P_x(t_1)(\alpha) = P_x(t_2)(\alpha) P_x(t_1, t_2)$

WHAT IS $P_x(t_2)(\alpha) P_x(t_1)(\alpha)$?

LET $t_1 = t_2$ THEN ONLY VALUES

OF α ARE $-1, 2, \pm 1, 0, 1$

THEN, IF $\alpha = 1$, $P_x(t_2)(\alpha) P_x(t_1)(\alpha) = 1$

$= \delta(\beta-1)$ (MOST STAY ON)

THEN, IF $\alpha = 2$, $P_x(t_2)(\alpha) P_x(t_1)(\alpha) = 2$

$= \delta(\beta+2)$

THEN, IF $\alpha = 1, 0, 1$, $P_x(t_2)(\alpha) P_x(t_1)(\alpha) = 1$

$= \delta(\beta - \sin \pi t_1)$

(CONT.)

$$\therefore p = \frac{1}{2}$$

$$+ \delta(\alpha + 707) \delta(\beta - 707) + \delta(\alpha - 707) \delta(\beta - 707) + \delta(\alpha + \beta) \delta(\beta + 2)$$

(c)

$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$
$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$
$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$
$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$

$$P_{\text{prob}} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} P_X(x) P_Y(y) \delta(x - \frac{1}{2}) \delta(y - \frac{1}{2}) dx dy$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \delta(x - \frac{1}{2}) \delta(y - \frac{1}{2}) dx dy$$

CAN'T PUT AS $f(t_2 - t_1) \Rightarrow$ ORDER STATIONARY
NOT SECOND

$$\text{FOR } t_1 = -1/4$$

$$\therefore X(t_1)X(t_2) = \frac{1}{2} + 1 - \frac{1}{2} \cos(\pi t_2)$$

$$+ \frac{1}{2} \cos(\pi t_2) = \frac{1}{2} + \frac{1}{2} \cos(\pi t_2)$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \delta(\beta - \cos(\pi t_2) + \cos(\pi t_2) + \cos(\pi t_2) \delta(\beta - \cos(\pi t_2))$$

$$= \int_{-\infty}^{\infty} \delta(\beta - \frac{1}{2}) \delta(\beta - 2\cos(\pi t_2) - 2\cos(\pi t_2) + 2\cos(\pi t_2)) d\beta$$

$$+ \cos(\pi t_2) \delta(\beta - \frac{1}{2}) = \cos(\pi t_2) \delta(\beta - \frac{1}{2})$$

$$= \int_{-\infty}^{\infty} \delta(\beta - \frac{1}{2}) \delta(\beta - \frac{1}{2}) d\beta$$

$$= \int_{-\infty}^{\infty} \delta(\beta - \frac{1}{2}) \delta(\beta - \frac{1}{2}) d\beta$$

$$= \int_{-\infty}^{\infty} \delta(\beta - \frac{1}{2}) \delta(\beta - \frac{1}{2}) d\beta$$

$$= \int_{-\infty}^{\infty} \delta(\beta - \frac{1}{2}) \delta(\beta - \frac{1}{2}) d\beta$$

$$= \int_{-\infty}^{\infty} \delta(\beta - \frac{1}{2}) \delta(\beta - \frac{1}{2}) d\beta$$

$$\Rightarrow X(t_1)X(t_2) = X(\frac{1}{2})X(\frac{1}{2})$$

$$= \delta(\beta - \cos(\pi t_2))$$

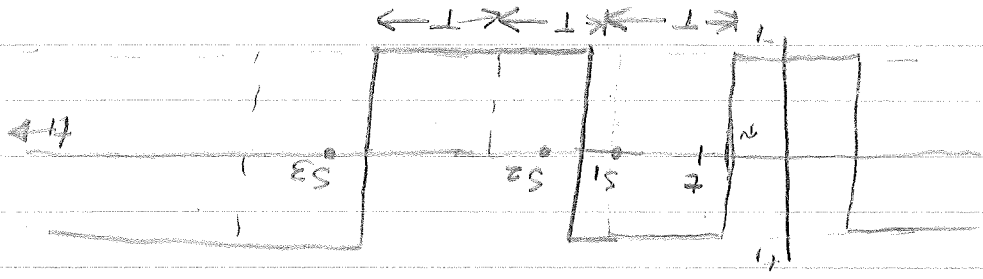
$$\text{THEN, IF } \alpha = 707, P_X(x) = \delta(x - 707)$$

PAIRS OF VALUES OF $X(t)$ AND $X(s)$
 PRODUCT OF ALL POSSIBLE

$$R_X(t, s) = X(t)X(s) = \frac{1}{4}(1-1+1) = 0$$

CORRELATION FUNCTION

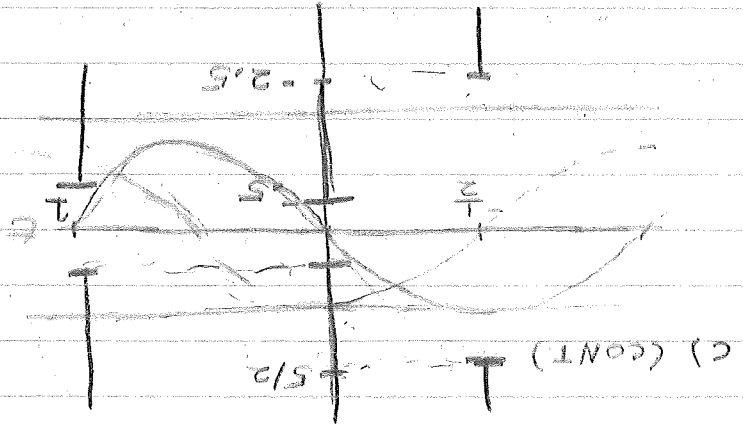
∴ WHEN $|t-s| > T$, THE
 THE VALUE OF $X(t)$ IN j TH INTERVAL
 j TH INTERVAL, IS IND. OF w_j
 ∴ THE VALUE OF $X(t)$ IN THE



$$X(t) = \sum_{-\infty}^{\infty} w_j \mu(t - \lambda_j - T)$$

3-12) R.V.
 5-2-71 010 3-9, 3-10

$$P = 2/3 = \frac{10}{15}$$



WHEN t AND s ARE IN SAME INTERVAL

EX) LET $s = s_1$

$$\Rightarrow x(t) = x(s_1) = \pm 1$$

$$\therefore x(t)x(s_1) = R_x(t, s_1) = 1$$

$$\therefore \overline{x(t)x(s)} = 1 = P[t \text{ \& } s \text{ ARE IN SAME INTERVAL}]$$

$$+ 0 \cdot P[t \text{ \& } s \text{ ARE NOT IN SAME INTERVAL}]$$

$$= P[t \text{ \& } s \text{ ARE IN SAME INTERVAL}]$$

FROM THE FIGURE, t \& s WILL LIE

IN THE SAME T SEC. INTERVAL IFF

$$s - T < t < s$$

$s > t$ (FOR EX, IN THE FIGURE)

$$P[s - T < t < s] = (t - s + T) \cdot \frac{1}{T} = 1 - \frac{s - t}{T}$$

$$= 1 - \frac{u}{T}$$

$$(u = s - t)$$

FOR $s < t$



LET $s < t$, THEN $s \text{ \& } t$ BELONG TO

THE SAME INTERVAL IFF

$$t - T < s$$

$$\Rightarrow P[t - T < s] = 1 + \frac{t}{T}$$

$$(u = s - t)$$

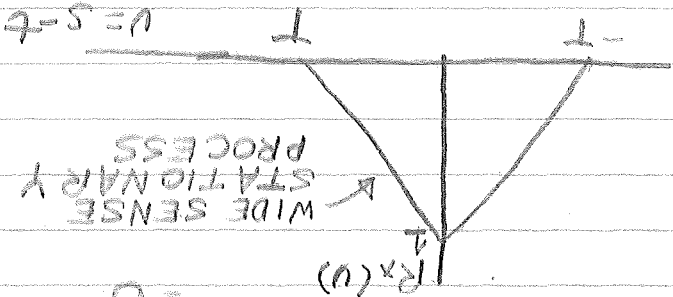
$$\therefore R_x(t, s) = R_x(s - t) = 1 + \frac{t}{T}$$

$$= 1 - \frac{u}{T}$$

$$u > 0$$

$$|u| > T$$

WIDE SENSE
STATIONARY
PROCESS



AMBIGUITY FUNCTIONS

$$x(t)$$

$$x_p(t) = x(t + \tau)$$

DEFINE A SIGNAL SPACE

$$\{x(t), y(t), z(t), \dots\}$$

PLUS A METRIC OR 'DISTANCE'

BETWEEN SIGNALS

$$d(x, y) = \int_{-\infty}^{\infty} |x(t) - y(t)|^2 dt$$

$$d(x, x_p) = \int_{-\infty}^{\infty} |x(t) - x_p(t)|^2 dt$$

$$= \int_{-\infty}^{\infty} [x(t) - x(t + \tau)]^2 dt$$

$$= \int_{-\infty}^{\infty} [x(t) - x(t + \tau)] dt$$

$$= \int_{-\infty}^{\infty} [x(t) x(t) + x(t + \tau) x(t + \tau)] dt$$

$$- \int_{-\infty}^{\infty} [x(t) x(t + \tau) + x(t + \tau) x(t)] dt$$

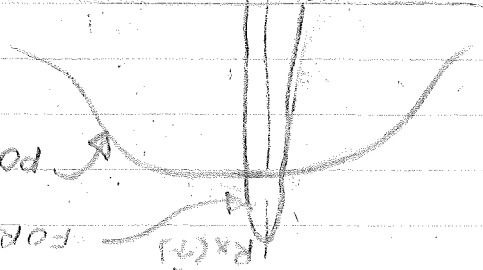
$$(Rx(t)) = \int_{-\infty}^{\infty} x(t) x(t + \tau) dt$$

$$\Rightarrow d(x, x_p) = Rx(0) + Rx(0) - Rx(\tau) - Rx(\tau)$$

$$= 2(Rx(0) - Rx(\tau))$$

FOR LITTLE AMBIGUITY

POOR



(4-1)

$$\hat{p}_n$$

$$\hat{p}_n = \frac{1}{n} \sum_{i=1}^n x_i$$

MUST MAXIMIZE: $P[M_n] \hat{p}_n (p/s - s)$; $\hat{x} = 0.1$

FOR $\hat{x} = k$, $\Rightarrow m = M_k$

NOW, $P[M_n] = 1/2$ FOR $\hat{x} = 0.1$

AS $P[M_n]$ IS INDEPENDENT OF \hat{x} ,

HENCE, CHOOSE $M = M_k$ IF

$P_n(p/s - s_k)$ IS MAX FOR $k = k$.

$$r_{2i} = n + s_{2i}$$

$$r = n \begin{bmatrix} 1 \\ 1 \end{bmatrix} + s \text{ OR } r_i = n + s_i$$

FORGET VECTOR NATURE: $r = n + s$

GIVEN p_n , WHAT IS $P_n(p/s = \hat{x})$?

$$n = n + s$$

$$P_n(p/s = s_k) = P_n(p - s_k / s = s_k)$$

$$= P_n(p - s_k) \text{ (STATISTICALLY INDEP. OF S)}$$

BECAUSE NOISE IS 0-MEAN GAUSSIAN

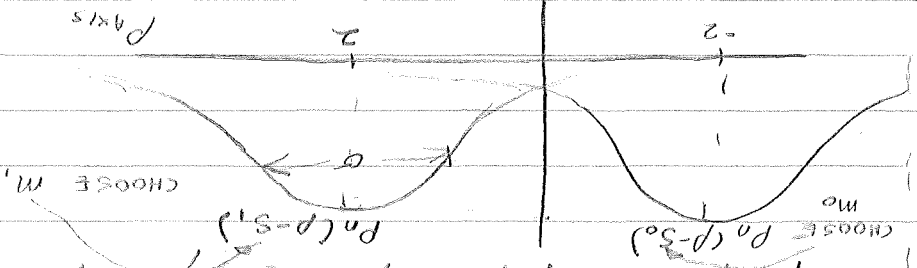
$$P_n(p - s_k) = \frac{1}{\sqrt{2\pi} \sigma} \exp\left(-\frac{1}{2\sigma^2} (p - s_k)^2\right)$$

$$\Rightarrow P_n(p - s_0) = \frac{1}{\sqrt{2\pi} \sigma} \exp\left(-\frac{1}{2\sigma^2} (p + 2)^2\right)$$

$$P_n(p - s_1) = \frac{1}{\sqrt{2\pi} \sigma} \exp\left(-\frac{1}{2\sigma^2} (p - 2)^2\right)$$

$$P_n(p - s_1) > P_n(p - s_0)$$

CHOOSE M_1



$$P[C/m_0] = \frac{1}{\sqrt{2\pi} \sigma} \exp\left(-\frac{1}{2\sigma^2} (p + 2)^2\right) dp$$

$$= \frac{1}{\sqrt{2\pi} \sigma} \exp\left(-\frac{1}{2\sigma^2} (p - 2)^2\right) dp$$

(CURRENT)

(NO CHANGE IN P[C])

→ SHIFTED TO RIGHT ONE UNIT

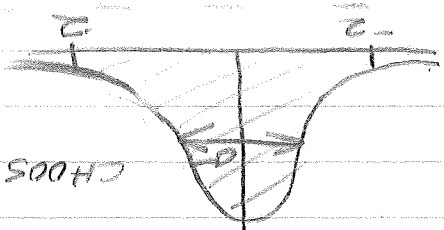
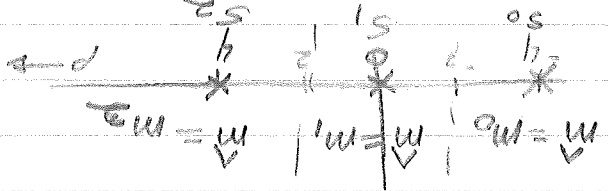
b) $P_0(p/s) = \sqrt{\frac{1}{2\pi}} \cdot e^{-\frac{1}{2} \left(\frac{p-1.5}{0.2} \right)^2}$
 $P_1(p/s) = \sqrt{\frac{1}{2\pi}} \cdot e^{-\frac{1}{2} \left(\frac{p-1.5}{0.2} \right)^2}$
 $P_2(p/s) = \sqrt{\frac{1}{2\pi}} \cdot e^{-\frac{1}{2} \left(\frac{p-1.5}{0.2} \right)^2}$
 $P_3(p/s) = \sqrt{\frac{1}{2\pi}} \cdot e^{-\frac{1}{2} \left(\frac{p-1.5}{0.2} \right)^2}$

INVESTIGATE

$$P[C] = 1 - \frac{1}{3} [P[C/m_0] + P[C/m_1] + P[C/m_2]]$$

$$P[m_1] = \frac{1}{3} \text{ V } \frac{1}{3}$$

FOR OPTIMUM RECEIVER WITH



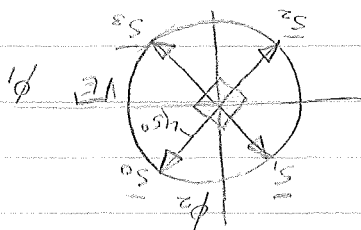
CHOOSE $\sigma = \int_{-\infty}^{\infty} p = 98.70$
 OF WHOLE THING

$$P[C] = 0.1 \Rightarrow P[C] = 99$$

$$\Rightarrow P[C] = P[C/m_0] + P[C/m_1] + P[C/m_2]$$

$$P[C/m_0] = \frac{1}{2} + \frac{1}{2} \sqrt{\frac{1}{2\pi}} \cdot e^{-\frac{1}{2} \left(\frac{0-2}{0.2} \right)^2} \int_{-\infty}^{\infty} p \cdot \frac{1}{2} \sqrt{\frac{1}{2\pi}} \cdot e^{-\frac{1}{2} \left(\frac{p-2}{0.2} \right)^2} dp$$

$$\Rightarrow P[C] = P[C/m_0] + P[C/m_1] + P[C/m_2]$$



4-2)

$\int_{-\infty}^{\infty} \phi_1 \phi_2 \text{ ORTHOGONAL } \int_{-\infty}^{\infty} \phi_1 \phi_2 = 0$
 $\int_{-\infty}^{\infty} \phi_1^2 dt = \int_{-\infty}^{\infty} \phi_2^2 dt = \text{ENERGY}$
 IF $E = 1$, ϕ_1, ϕ_2 ARE ORTHONORMAL

ENERGY = E_s

$s_0 = \sqrt{E_s} (\cos \phi_1 + \cos \phi_2)$

$s_1 = \sqrt{E_s} (\cos \phi_1 - \cos \phi_2)$

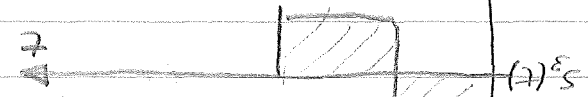
$s_2 = \sqrt{E_s} (\sin \phi_1 - \sin \phi_2)$

$s_3 = \sqrt{E_s} (\sin \phi_1 + \sin \phi_2)$



$\int s_1^2(t) dt = E$
 s_0 ORTH. TO s_1
 s_0 " " s_2
 s_0 " " s_3

$s_1 = -s_3$
 $s_2 = -s_0$



WE CAN DEFINE 2 ORTHONORMAL TIME FUNCTIONS, $\phi_1(t), \phi_2(t)$. THEN THE SIGNALS MAY BE WRITTEN:

$$\begin{aligned}
 s_0(t) &= \sqrt{E_s} (\sqrt{2} \phi_1(t) + \sqrt{2} \phi_2(t)) \\
 s_1(t) &= \sqrt{E_s} (\frac{1}{\sqrt{2}} \phi_1(t) + \frac{1}{\sqrt{2}} \phi_2(t)) \\
 s_2(t) &= -s_0(t) \\
 s_3(t) &= -s_1(t)
 \end{aligned}$$

HOW DO WE MAKE $n(t)$ TO A VECTOR

$$\begin{aligned}
 n_1 &= \int_{-\infty}^{\infty} n_1(t) \phi_1(t) dt \\
 n_2 &= \int_{-\infty}^{\infty} n_2(t) \phi_2(t) dt
 \end{aligned}$$

(ϕ_1, ϕ_2 ORTHONORMAL)

n_1 AND n_2 ARE GAUSSIAN R.V.

$$P[n_1] = P[n_2] \quad \lambda, \lambda = 0, 1, 2, 3$$

MUST MAXIMIZE APOSTERIORI PROBABILITY

$$P[m_2] p_r(p/s=s_2) \text{ vs } P[m_1] p_r(p/s=s_1)$$

$m(p) = m_2$ WHEN

$$P[m_2] p_r(p/s=s_2) > P[m_1] p_r(p/s=s_1)$$

BECAUSE $P[m_2] = \lambda$, WE HAVE

MAXIMUM LIKELIHOOD SITUATION

AND THE DECISION FUNC. BECOMES

$$p_r(p/s=s_2) \quad (n = n - s_2)$$

$$\text{NOW } P_r(p/s=s_2) = P^n(p-s_2)$$

$$= \frac{\pi^{n/2}}{2^n} e^{-\frac{1}{2} [(p-s_2)^2 + (p-s_2)^2]} / N_0$$

EXAMPLE:

$$P[C/m_0] = \int_0^\infty \int_0^\infty \frac{1}{N_0} e^{-(p_1 - s_1) + (p_2 - s_2)} \frac{d p_1 d p_2}{\sqrt{(p_1 - s_1)^2 + (p_2 - s_2)^2}} = \int_0^\infty \int_0^\infty \frac{1}{N_0} e^{-(p_1 - s_1) + (p_2 - s_2)} \frac{d p_1 d p_2}{\sqrt{(p_1 - s_1)^2 + (p_2 - s_2)^2}}$$

$$= \int_0^\infty \int_0^\infty \frac{1}{N_0} e^{-(p_1 - s_1) + (p_2 - s_2)} \frac{d p_1 d p_2}{\sqrt{(p_1 - s_1)^2 + (p_2 - s_2)^2}}$$

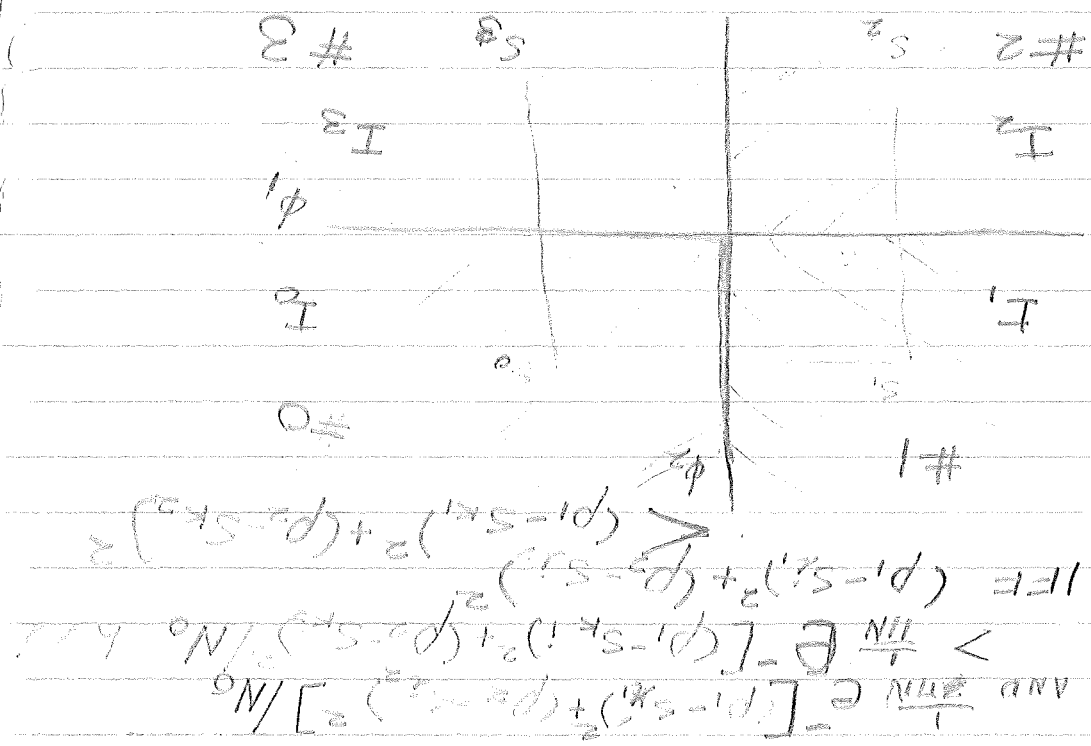
$$= \int_0^\infty \int_0^\infty \frac{1}{N_0} e^{-(p_1 - s_1) + (p_2 - s_2)} \frac{d p_1 d p_2}{\sqrt{(p_1 - s_1)^2 + (p_2 - s_2)^2}}$$

$$= \int_0^\infty \int_0^\infty \frac{1}{N_0} e^{-(p_1 - s_1) + (p_2 - s_2)} \frac{d p_1 d p_2}{\sqrt{(p_1 - s_1)^2 + (p_2 - s_2)^2}}$$

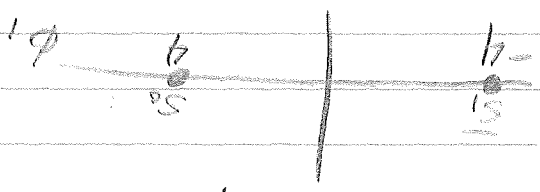
$$= \int_0^\infty \int_0^\infty \frac{1}{N_0} e^{-(p_1 - s_1) + (p_2 - s_2)} \frac{d p_1 d p_2}{\sqrt{(p_1 - s_1)^2 + (p_2 - s_2)^2}}$$

$$= \iint p r (p/s = s_1) d p$$

$$P[C/m_0] = P[reI, |m_0]$$



$$P[m_0] = P[m_1] = \frac{1}{2}$$



a) LET $s_0(t) = 4\phi_1(t) \Rightarrow \underline{s_0} = 4\phi_1$
 $s_1(t) = -4\phi_1(t) \Rightarrow \underline{s_1} = -4\phi_1$
 $\Rightarrow N_0 = 8$

SPECTRAL DENSITY OF NOISE:
 $S(f) = \frac{N_0}{2} = 4$ WATT/SEC CYCLE/HERTZ

THEN $\int_{-\infty}^{\infty} \phi_1(t)\phi_2(t)dt = 0$
 $\int_{-\infty}^{\infty} \phi_1^2(t)dt = 1$ $\lambda = 1,2$

$$\phi_1(t) = \frac{1}{2} p(t)$$

$$\phi_2(t) = \frac{1}{2} p(t)$$

DEFINE AN ORTHONORMAL SET

	x	-x
y	1	-1

x AND x BETTER THAN x AND y (FURTHER APART)

$\frac{E_s}{N_0}$ = SIGNAL TO NOISE RATIO

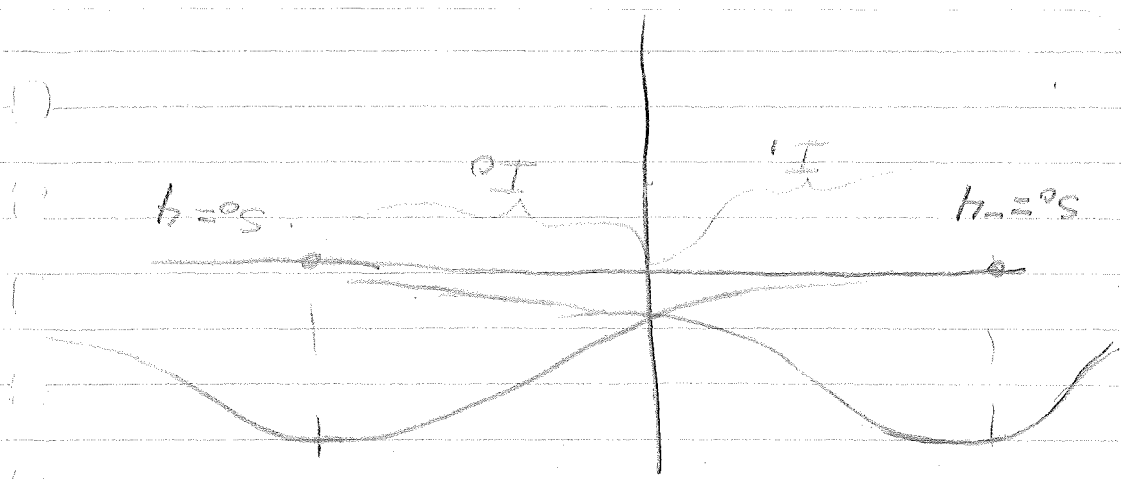
$$\Rightarrow P[c/m_0] = Q_2 \left(-\sqrt{\frac{E_s}{N_0}} \right)$$

$$\Rightarrow P[c/m_1] = Q_2 \left(-\sqrt{\frac{E_s}{N_0}} \right)$$

$$\Rightarrow P[c] = Q_2 \left(-\sqrt{\frac{E_s}{N_0}} \right)$$

$\Rightarrow \lambda = 0,12,3$

VIETNAM UNIVERSITY OF ELECTRONICS AND TECHNOLOGY



$$= \frac{\sqrt{N_0}}{1} \frac{e^{-\rho s}}{-(\rho s)^2} = \frac{2(\pi)^{1/2}}{8} \frac{e^{-\rho s}}{-(\rho s)^2}$$

$$\therefore p_n(\rho - s) = \frac{1}{-(\rho - s)^2} e^{-\frac{2\rho s}{2\pi}} = \frac{1}{-(\rho - s)^2} e^{-\frac{\rho s}{\pi}}$$

$$E[n^2] = \sigma^2 \text{ (FOR 0 MEAN)} = \frac{N_0}{2} = \frac{2}{N_0} \int_{-\infty}^{\infty} \phi_1(t_1) \phi_1(t_1) dt_1 = \frac{2}{N_0}$$

$$= \frac{2}{N_0} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \delta(t_1 - t_2) \phi_1(t_1) \phi_1(t_2) dt_1 dt_2$$

AUTOCORRELATION OF WHITE NOISE

$$E[n^2] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E[n_w(t_1) n_w(t_2)] \phi_1(t_1) \phi_1(t_2) dt_1 dt_2$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} n_w(t_1) n_w(t_2) \phi_1(t_1) \phi_1(t_2) dt_1 dt_2$$

$$n^2 = \int_{-\infty}^{\infty} n_w(t) \phi_1(t) dt \int_{-\infty}^{\infty} n_w(t_2) \phi_1(t_2) dt_2$$

$$E[n] = \int_{-\infty}^{\infty} E[n_w(t)] \phi_1(t) dt = 0$$

$$n = \int_{-\infty}^{\infty} n_w(t) \phi_1(t) dt \quad (A.D)$$

BY DEFINITION:

ALL VECTORS ARE ONE DIMENSIONAL

IN THE FIRST PROBLEM,

$$p_n(\rho - s) > p_n(\rho - s\pi)$$

$$\therefore m(\rho) = m_0 \quad \text{I.F.}$$

(cont)

$$\therefore P_n(\alpha) = \frac{1}{T} e^{-\alpha^2} \in \frac{(s_1^2 + \alpha^2) / 2 N_0}{T}$$

TWO ORTHOGONAL FUNC, $\phi_1(t), \phi_2(t)$
FOR THE PROJECTIONS ONTO

\therefore NOISE COMPONENTS INDEPENDENT

$$= \frac{1}{N_0} \int_{-\infty}^{\infty} \phi_1(t) \phi_2(t) dt = 0$$

$$E[n_1 n_2] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E[n_w(t_1) n_w(t_2)] \phi_1(t_1) \phi_2(t_2) dt_1 dt_2$$

$$E[n_1^2] = E[n_2^2] = N_0/2$$

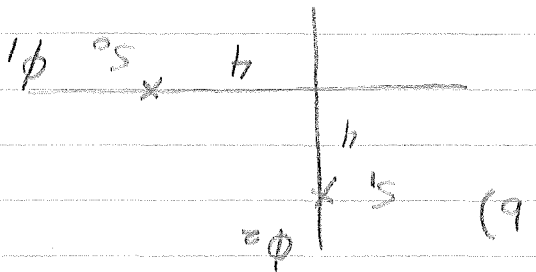
$$E[n_1] = E[n_2] = 0$$

$$n_2 = \int_{-\infty}^{\infty} n_w(t) \phi_2(t) dt$$

$$n_1 = \int_{-\infty}^{\infty} n_w(t) \phi_1(t) dt$$

$$n = [n_1, n_2]$$

$$S_n = [4, 0], S_1 = [0, 4]$$



$$\Rightarrow P[C] = Q(-2)$$

$$P[C/m_1] = P[C/m_2] = Q(-2)$$

$$= Q(-2)$$

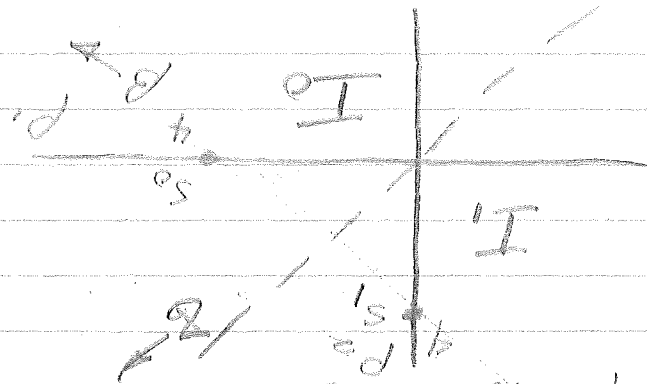
$$\Rightarrow P[C/m_0] = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{-\frac{p^2}{2}} dp$$

$$\text{LET } \phi = \frac{p}{\sqrt{2}}, dp = \sqrt{2} d\phi$$

$$P[C/m_0] = \int_{-\infty}^{\infty} \frac{1}{\sqrt{2\pi}} e^{-\frac{p^2}{2}} dp = \int_{-\infty}^{\infty} \frac{1}{\sqrt{2\pi}} e^{-\frac{(\sqrt{2}\phi)^2}{2}} \sqrt{2} d\phi$$

$$P_n(p-s) = \frac{1}{2\pi N_0} e^{-\frac{(p_1-4)^2 + p_2^2}{2N_0/2}}$$

$$P_n(p-s) = \frac{1}{\pi N_0} e^{-\frac{(p_1^2 + (p_2-4)^2)/N_0}{}}$$



$$P[C/m_0] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_2 dp_1 p_2 \frac{1}{\pi N_0} e^{-\frac{(p_1-4)^2 + p_2^2}{2N_0}}$$

LET $\beta = p_1 - 4$
 $P[C/m_0] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_2 dp_2 \int_{-\infty}^{\infty} p_2 dp_1 \frac{1}{\pi N_0} e^{-\frac{\beta^2 + p_2^2}{2N_0}}$

LET $\alpha = \beta + 4$
 $\beta = \alpha - 4$

THEN $P[C/m_0] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} p_2 dp_2 \int_{-\infty}^{\infty} p_2 dp_1 \frac{1}{\pi N_0} e^{-\frac{(\alpha-4)^2 + p_2^2}{2N_0}}$

$$= \frac{1}{\pi N_0} \int_{-\infty}^{\infty} p_2 dp_2 \int_{-\infty}^{\infty} p_2 dp_1 e^{-\frac{(\alpha-4)^2 + p_2^2}{2N_0}}$$

$$P[C/m_1] = Q(-\sqrt{2})$$

$$\Rightarrow P[C] = Q(-\sqrt{2}) < Q(-2)$$

RECEIVER IMPLEMENTATION

M-MESSAGE, $L=0, \dots, M-1$

N-DIMENSIONS $j=1, \dots, N$

RECEIVER CALCULATES:

$$\underline{r} = (r_1, \dots, r_N)$$

$$r_j = \int_{-\infty}^{\infty} r(t) \phi_j(t) dt$$

= PROJECTION OF $r(t)$ ONTO $\phi_j(t)$

DECISION FUNCTION

$$|r - s_k|^2 = N_0 \ln P[M_k]$$

$$\text{FOR W.G.N, } s_{kf} = \frac{1}{N_0} \int_0^T s_k^2 = \frac{2}{N_0}$$

$M = M^*$ IF DECISION FUNCTION

IS MINIMUM FOR $k = k$

$$\text{NOW } |r - s_k|^2 = \frac{1}{N_0} (r_j - s_{kj})^2 = |r_j - 2r_{js} + s_j|^2$$

$$\exists r_{js} = \frac{1}{N_0} r_{js}$$

HENCE, BECAUSE OF THE (-) SIGN

BEFORE r_{js} , MUST MAXIMIZE

r_{js} IN ORDER TO MINIMIZE

$$|r - s_k|^2$$

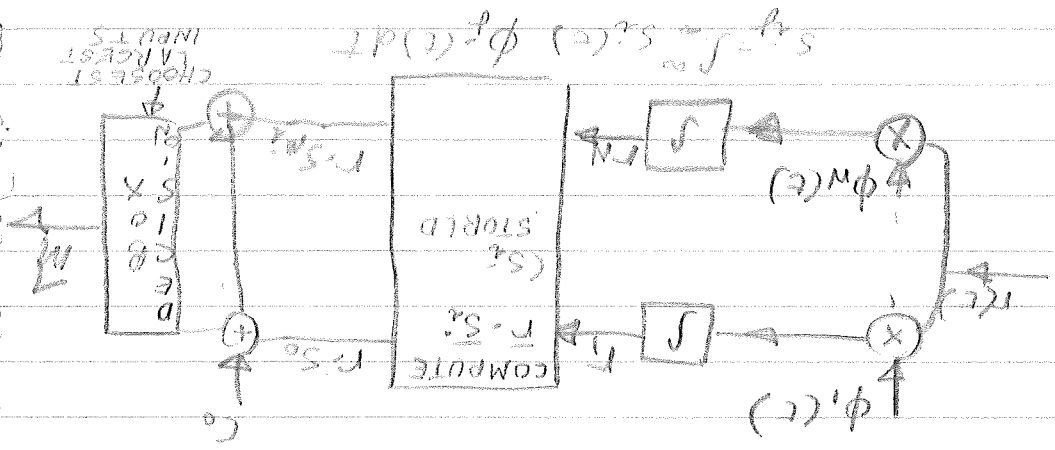
REALLY, WE MUST MAXIMIZE

$$r_{js} + c_{js} = \frac{1}{N_0} (N_0 \ln P[M_k]) - |s_j|^2$$

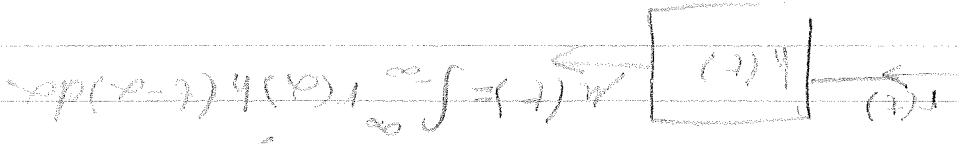
$$L = 0, \dots, M-1$$

CORRELATION RECEIVER COMPUTES THE (CROSS) CORRELATION FUNCTION $F \cdot S_i$, EITHER ANALOGICALLY OR DIGITALLY

NOTE $F \cdot S_i = \int_{-\infty}^{\infty} r(t) S_i^*(t) dt$
 OR $r_i = \int_{-\infty}^{\infty} r(t) \phi_i^*(t) dt$



MATCHED FILTERS (P. 336)



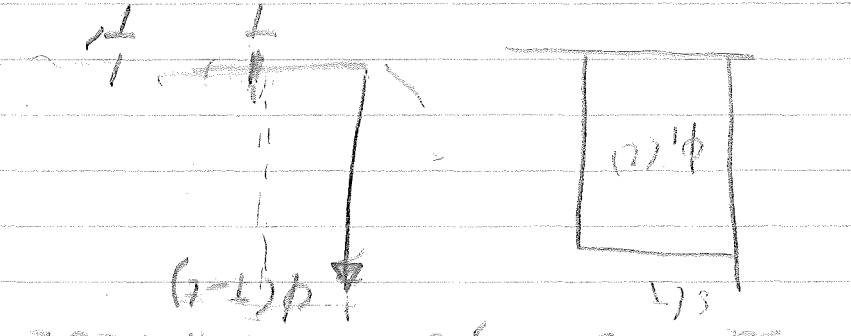
WE WANT TO GENERATE

THE COMPONENTS, NOT TERMS
 $r_i = \int_{-\infty}^{\infty} r(t) \phi_i(t) dt$
 CONSIDER;

$h(t) = \phi_i^*(T-t)$; THE N

$x(t) = \int_{-\infty}^{\infty} r(t-\alpha) d\alpha$

FOR CAUSALITY ON $\phi(T-t)$, WE
 MUST ~~THE~~, WE FORGIVE THAT
 EACH BASIS FUNC., VANISH
 IDENTICALLY OUTSIDE SOME
 FINITE INTERVALS!



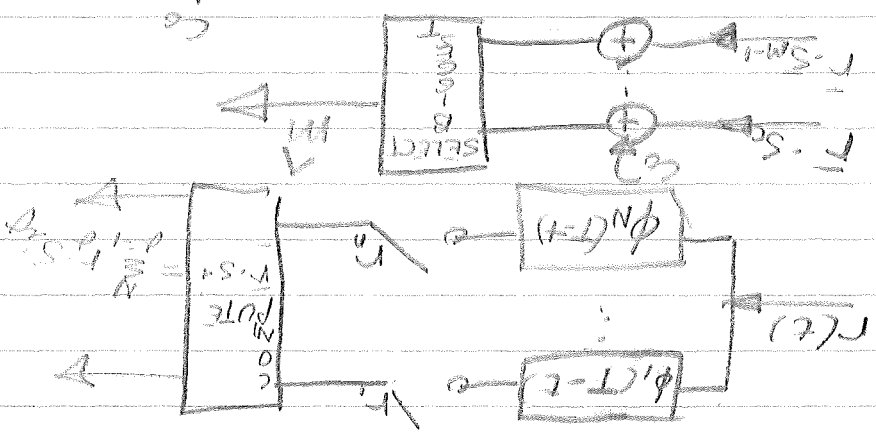
$h(t)$ MUST BE CAUSE
 $h(t) = 0$, SUPER IMPULSE
 $h(t) = \int_{-\infty}^{\infty} r(\alpha) (\phi_1(\alpha)) d\alpha$
 SAMPLE AT $t=0$ AND $t=T$
 $= \int_{-\infty}^{\infty} r(\alpha) \phi_1(\alpha) d\alpha$

CAN MATCH DIRECTLY TO S.C.

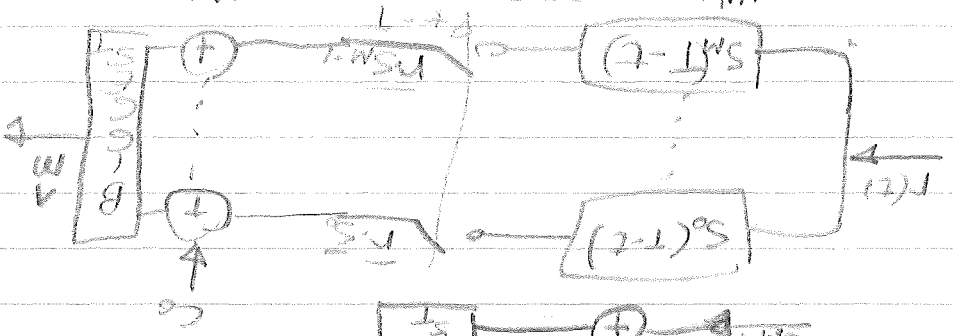
$$U(t) = \int_{-\infty}^{\infty} r(\alpha) S_c(T - (t-\alpha)) d\alpha$$

$$= \int_{-\infty}^{\infty} r(\alpha) S_c(T + \alpha - t) d\alpha$$

$$\therefore U(T) = \int_{-\infty}^{\infty} r(\alpha) S_c(\alpha) d\alpha$$



MATCHING DIRECTLY TO SIGNAL



$$P[E] = Q\left[\frac{\sqrt{2E_s}}{\sqrt{2N_0}}\right] = Q\left[\frac{\sqrt{2E_s}}{\sqrt{2N_0}}\right]$$

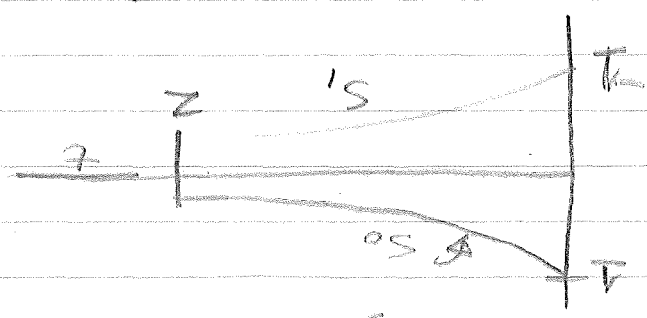
$$E_s (\text{REALLY}) = \int_0^T e^{-2t} dt = \frac{1}{2}(1 - e^{-2T})$$

$$E_s = \int_0^T e^{-2t} dt = \frac{1}{2}$$

ASSUMING $S_N(f) = N_0/2$

$$P[E] = Q\left[\frac{\sqrt{2E_s}}{\sqrt{2N_0}}\right] = Q\left[\frac{\sqrt{2E_s}}{\sqrt{2N_0}}\right]$$

DISTANCE BETWEEN SIGNALS



4-15) $s_0 = e^{-t} u(t); s_1(t) = e^{-t} u(t)$

MESSAGES:

$$P[E] = Q \left[\frac{d}{d_{\text{VAND}}} \right]$$

WHERE $d_2 = |s_0 - s_1|^2$

$$= \int_{-\infty}^{\infty} [s_1(t) - s_0(t)]^2 dt = \frac{3}{16}$$

$$\Rightarrow P[E] = Q \left[\frac{10^{-4}}{4} \right] \approx 10^{-4}$$

b) FOR EQUALLY LIKELY BINARY

$(C_0 = C_1, \text{HENCE, IGNORE})$

PROBABLE

AND BOTH ARE EQUALLY

$s_0(t) = \text{ENERGY IN } s_1(t)$

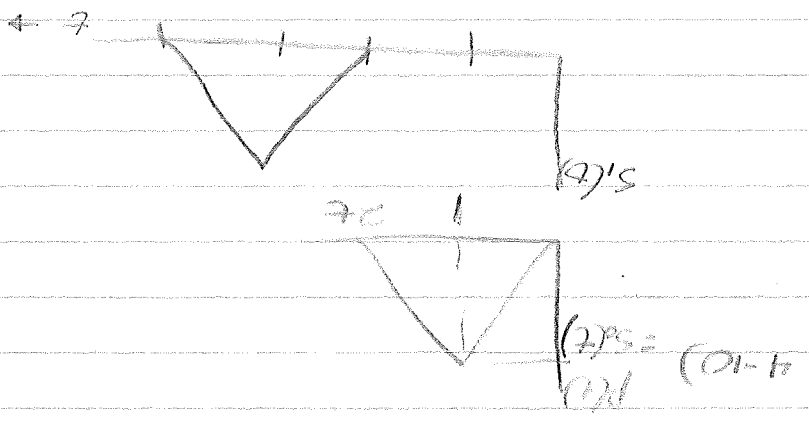
SINCE THE ENERGY OF

$\int_{-\infty}^{\infty} r(t) s_0(t) dt = \int_{-\infty}^{\infty} r(t) s_1(t) dt$

RECEIVING $r(t)$

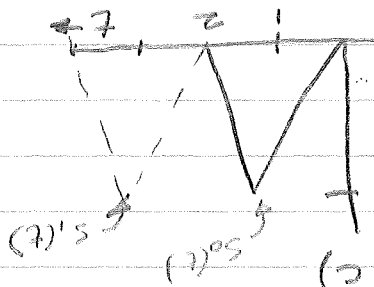
SELECTS m_0 AFTER

a) AN OPTIMUM RECEIVER

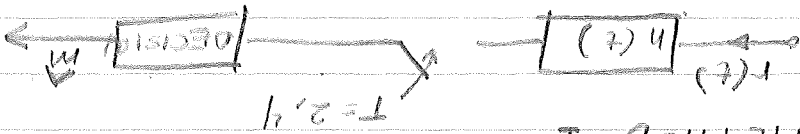


4-17-71

4-10(c)



C) METHOD 2

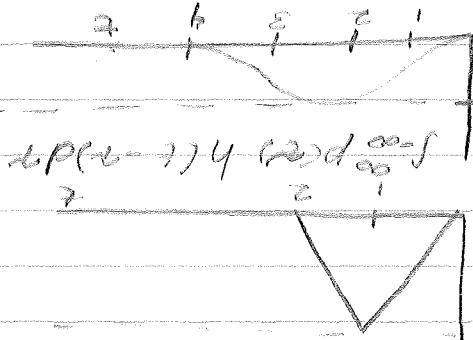


THE SAMPLE AT $T=2$ IS

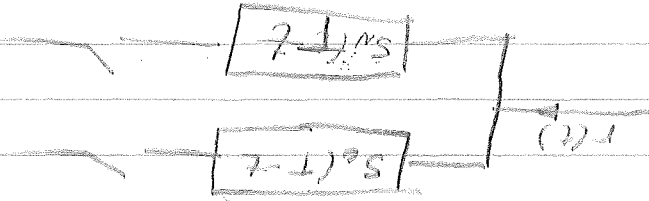
$$\int_{-\infty}^{\infty} r(t) s_0(t) dt,$$

THAT AT $T=4$ IS $\int_{-\infty}^{\infty} r(t) s_1(t) dt$

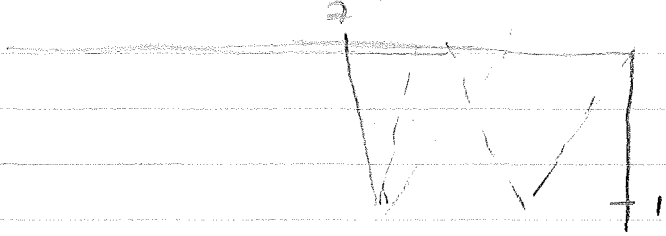
$$h(t) = s_0(2-t)$$



MATCH FILTER



$$t < 0 \Rightarrow * \leftarrow 0 \leq t$$



$$\int_{-\infty}^{\infty} p(r) s_0(t-r) dr = \int_{-\infty}^{\infty} p(r) s_0(2-t+r) dr$$

$$= \int_{-\infty}^{\infty} s_0(r) s_0(a-t+r) dr$$

$$= \int_{-\infty}^{\infty} s_0(T) s_0(t-r) dr$$

$$\int_{-\infty}^{\infty} r(\alpha) h(t-\alpha) d\alpha = e(t)$$

$$= \int_{-\infty}^{\infty} r(\alpha) s_0(T-t+\alpha) d\alpha$$

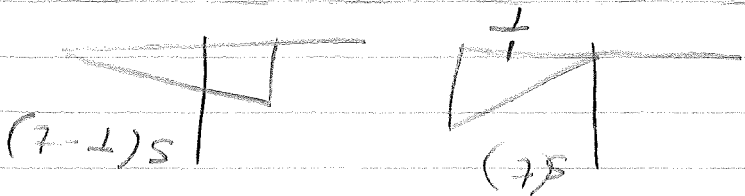
$$= \int_{-\infty}^{\infty} r(\alpha) s_0(\alpha) d\alpha$$

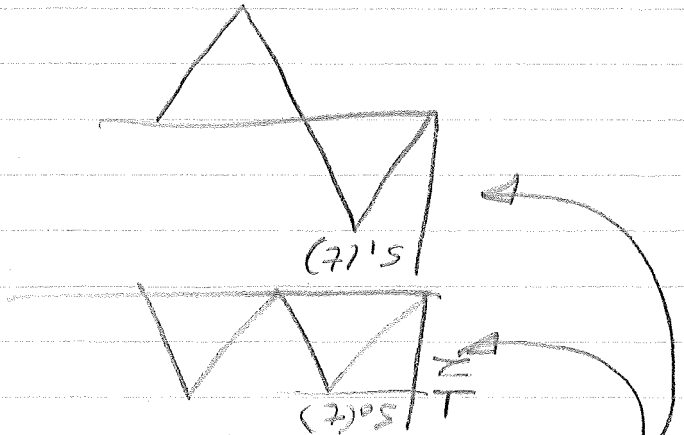
$$U(2) = \int_{-\infty}^{\infty} r(\alpha) s_0(\alpha) d\alpha$$

$$U(4) = \int_{-\infty}^{\infty} r(\alpha) s_0(\alpha-2) d\alpha$$

$$= \int_{-\infty}^{\infty} r(\alpha) s_1(\alpha) d\alpha$$

(cont.)





$$s_1(t) = p(t); s_0(t) = p(t)$$

SMALL ERROR (ENTRIPITAL)

$$s_0(t) = \frac{1}{2} [p(t) + p(t-2)]$$

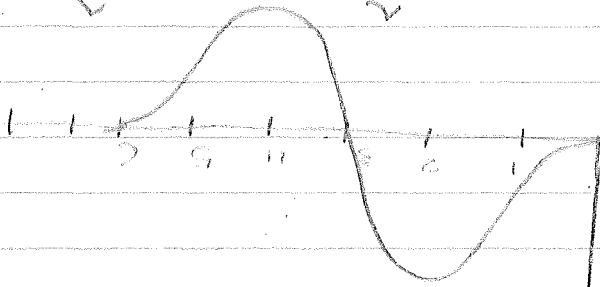
d) SAME ERROR PROP

(RIGHT GRAPH)

$$\int_{-\infty}^{\infty} r(t) [s_1(4+7t) - s_0(4+7t)] dt$$

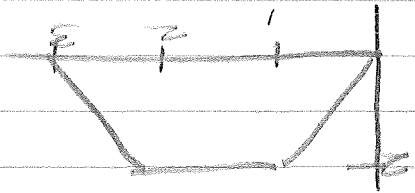
$$h(t) = s_1(4-t) - s_0(4-t)$$

FOR +, $m = s_0$
FOR -, $m = s_1$



$$\int_{-\infty}^{\infty} r(t) h(t-7) dt = \int_{-\infty}^{\infty} r(t) [s_0(t) - s_1(t)] dt$$

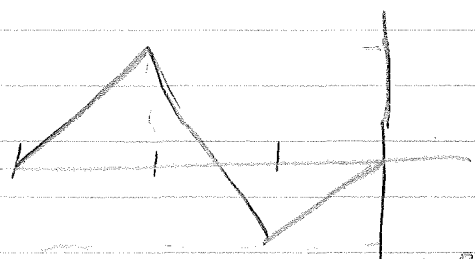
FOR $s_0(t) = p(t), s_1(t) = p(t-1)$
 $d^2 = \int_{-\infty}^{\infty} [s_0(t) - s_1(t)]^2 dt = \frac{3}{20}$
 $P[E] = Q\left[\frac{\sqrt{3/0.05}}{5}\right] \approx 4 \times 10^{-9}$



$P[E] = Q\left[\frac{\sqrt{3/0.05}}{1}\right]$

$= 2 \int_{1/3}^1 dx + 2 \int_{1/3}^1 (4x)^2 dx = 4$

$d^2 = \int_{-\infty}^{\infty} [s_0(t) - s_1(t)]^2 dt$



FOR $s_0(t) = p(t)$
 $s_1(t) = p(t-1)$
 $s_0(t) - s_1(t)$

$$\begin{aligned}
 & \mathcal{F}\mathcal{F}(f-g) = H(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = \\
 & \mathcal{F}\mathcal{F}' + \mathcal{F}\mathcal{F}(\mathcal{F}-\mathcal{F}) \mathcal{G} \\
 & \mathcal{F}\mathcal{G}(\mathcal{F}H) \mathcal{F} = (\mathcal{F}H(\mathcal{F})) \mathcal{G}
 \end{aligned}$$

$$\mathcal{F}(f) \mathcal{G} = \mathcal{F}P_2 + H \mathcal{F} - \mathcal{G} \int_{-\infty}^{\infty}$$

$$\begin{aligned}
 & \mathcal{F}\mathcal{F}'\mathcal{F}(\mathcal{F}(\mathcal{F}-\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty}) \\
 & (\mathcal{F}) H(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} =
 \end{aligned}$$

$$\begin{aligned}
 & \mathcal{F}\mathcal{F}'\mathcal{F}(\mathcal{F}H) \mathcal{G} \int_{-\infty}^{\infty} \mathcal{F}'\mathcal{F} \\
 & \mathcal{F}\mathcal{F}'\mathcal{F}(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} \mathcal{F}'\mathcal{F} =
 \end{aligned}$$

$$\mathcal{F}P(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} - (\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty}$$

$$\begin{aligned}
 & (\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = (\mathcal{F}) H \\
 & (\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = (\mathcal{F}) \mathcal{G}
 \end{aligned}$$

$$\mathcal{F}\mathcal{F}(\mathcal{F}-\mathcal{F}) * H(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = \mathcal{F}\mathcal{G}(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty}$$

COMPLEX CONVOLUTION

CHAPT. 7 : FIRST 2 SECTIONS

$$\mathcal{S}_0(f) = \mathcal{S}_0^*(f)$$

FOR REAL TIME FUNCTIONS:

$$\begin{aligned}
 & \mathcal{F}\mathcal{F}(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} H(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = \\
 & \mathcal{F}P_2 \int_{-\infty}^{\infty} (\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = \mathcal{F}P
 \end{aligned}$$

$$\mathcal{F}\mathcal{F}(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty} = \mathcal{F}\mathcal{G}(\mathcal{F}) \mathcal{G} \int_{-\infty}^{\infty}$$

4-24-71

$$7-4) \quad n(t) = R_c(t) \sqrt{2} \cos \omega_c t + n_s(t) \sqrt{2} \sin \omega_c t$$

$$n(t) n(t-\tau) = [n_c(t) \sqrt{2} \cos \omega_c t + n_s(t)$$

$$\sqrt{2} \sin \omega_c t] [n_c(t-\tau) \sqrt{2} \cos \omega_c(t-\tau) + n_s(t-\tau) \sqrt{2} \sin \omega_c(t-\tau)]$$

$$= n_c(t) n_c(t-\tau) 2 \cos \omega_c t \cos \omega_c(t-\tau) + n_s(t) n_s(t-\tau) 2 \sin \omega_c t \sin \omega_c(t-\tau)$$

$$+ n_c(t) n_s(t-\tau) 2 \cos \omega_c t \sin \omega_c(t-\tau) + n_s(t) n_c(t-\tau) 2 \sin \omega_c t \cos \omega_c(t-\tau)$$

$$= R_c(t) \sqrt{2} \cos \omega_c t + \cos 2 \omega_c t + \cos 2 \omega_c(t-\tau)$$

$$+ R_s(t) \sqrt{2} \sin \omega_c t + \sin \omega_c t + R_s(t-\tau) \sqrt{2} \sin \omega_c(t-\tau) + \sin \omega_c(t-\tau)$$

$$+ R_c(t-\tau) \sqrt{2} \cos \omega_c(t-\tau) - \cos \omega_c(t-\tau)$$

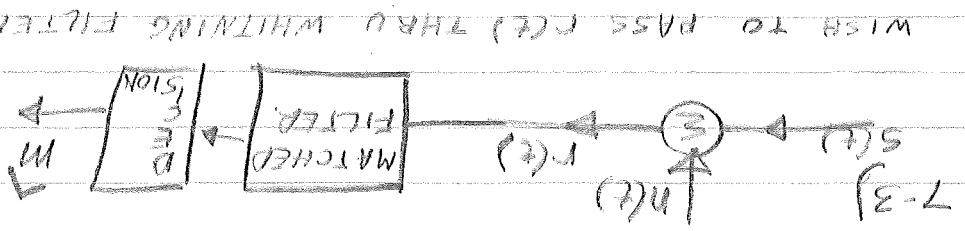
WANT 2 MAKE FUNCTION OF τ

$$n(t) n(t-\tau) = \cos \omega_c \tau [R_c(t) + R_s(t-\tau)] + R_s(t) [R_c(t-\tau) - R_s(t)] + \cos 2 \omega_c \tau + \omega_c \tau [R_c(t-\tau) - R_s(t-\tau)] + \sin \omega_c \tau [R_s(t) - R_s(t-\tau)] + \sin \omega_c(t-\tau) [R_s(t) + R_s(t-\tau)]$$

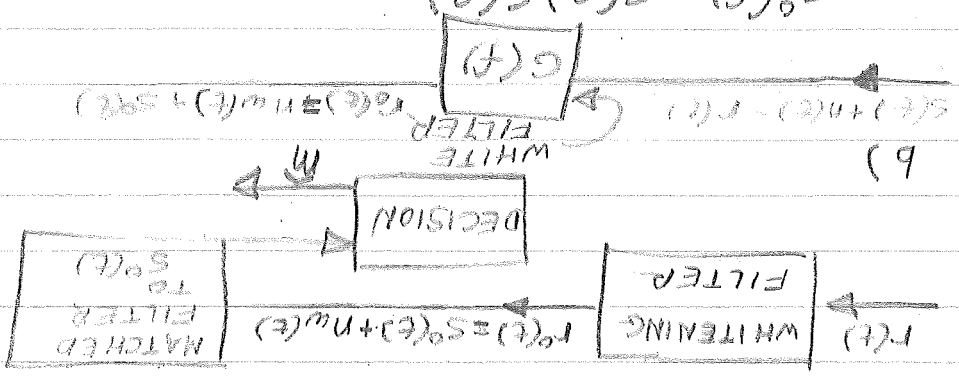
WIDE SENSE STATIONARY SUFFICIENT:

$$R_c(\tau) = R_s(\tau)$$

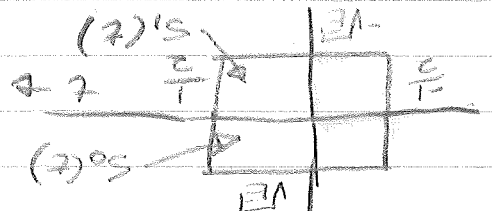
$$R_c(\tau) = -R_s(\tau)$$



WISH TO PASS $r(f)$ THRU WHITENING FILTER



$$S_0(f) = G(f)S(f)$$



WANNA FIND $G(f)$

$$S_w(f) = \frac{N_o}{f^{2+1}} = \frac{N_o}{f^3}$$

$$S_u(f) = \frac{N_o}{f^{2+1}} = \frac{N_o}{f^3}$$

$$S_w(f) = 1/G(f) \Rightarrow S_w(f) = \frac{N_o}{f^3}$$

$$\Rightarrow G(f) = \frac{N_o}{f^3}$$

$$\Rightarrow G(f)G^*(f) = \frac{N_o}{f^3} \frac{N_o}{f^3} = \frac{N_o^2}{f^6}$$

$$\Rightarrow G(f)G^*(f) = \frac{1}{f^6}$$

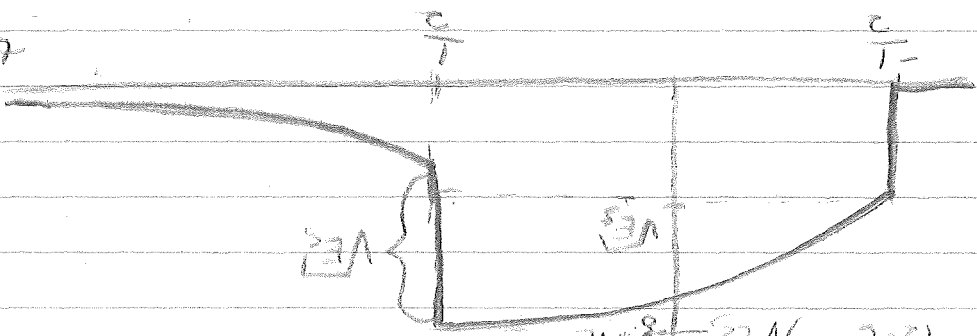
$$\Rightarrow G(f) = \frac{1}{f^3}$$

(POWER)

(POLES IN LEFT)

(UPPER HALF OF f PLANE)

47



$$S(f) = \int_{-\infty}^{\infty} s(x) e^{-j2\pi f x} dx$$

$$= \int_{-1/2}^{1/2} s(x) e^{-j2\pi f x} dx$$

$$= \int_{-1/2}^{-1/4} \sqrt{2} e^{-j2\pi f x} dx + \int_{-1/4}^{1/4} \sqrt{2} e^{-j2\pi f x} dx + \int_{1/4}^{1/2} 0 dx$$

$$= \sqrt{2} \left[\frac{e^{-j2\pi f x}}{-j2\pi f} \right]_{-1/2}^{-1/4} + \sqrt{2} \left[\frac{e^{-j2\pi f x}}{-j2\pi f} \right]_{-1/4}^{1/4}$$

$$= \frac{\sqrt{2}}{-j2\pi f} \left(e^{-j\pi f} - e^{j\pi f} \right) + \frac{\sqrt{2}}{-j2\pi f} \left(e^{-j\pi f} - e^{j\pi f} \right)$$

$$= \frac{\sqrt{2}}{-j2\pi f} \left(2 \cos(\pi f) \right) e^{-j\pi f}$$

$$= \frac{2\sqrt{2} \cos(\pi f) e^{-j\pi f}}{-j2\pi f}$$

FOR $t > \frac{1}{2}$

$$S(f) = \int_{-\infty}^{\infty} s(x) e^{-j2\pi f x} dx = 0$$

FOR $t < -\frac{1}{2}$, $S(f) = 0$

FILTER (SIGNAL TO BE MATCHED)

OUTPUT SIGNAL FROM WHITENING

WHITENING FILTER

$\Rightarrow \delta(t) = \text{IMPULSE RESPONSE FOR}$

$$G(s) = \frac{1 + s + 2\pi}{s + 2\pi}$$

$$= \frac{1 + s + 2\pi}{s + 2\pi}$$

$$= \frac{1 + s + 2\pi}{s + 2\pi}$$

MONDAY

THUS, WE CANNOT BUILD A MATCHED FILTER SAMPLING AT TIME T , CAUSE OF THE INFINITE TAIL, CHOP OFF TAIL IN ABOUT 5 TIME CONSTANTS (5 SEC), WITHOUT TO MUCH LOSS OF OPTIMALITY.

7-5) $s_1(t), s_2(t)$ - TWO LOW-PASS

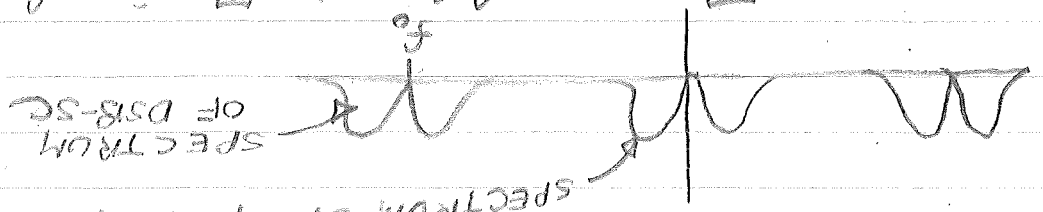
(BASE-BAND) SIGNALS

$$s_1(t) \sqrt{2} \cos 2\pi f_0 t$$

$$s_2(t) \sqrt{2} \sin 2\pi f_0 t$$

SPECTRUM OF s_1 OR s_2

SPECTRUM OF DSB-SC

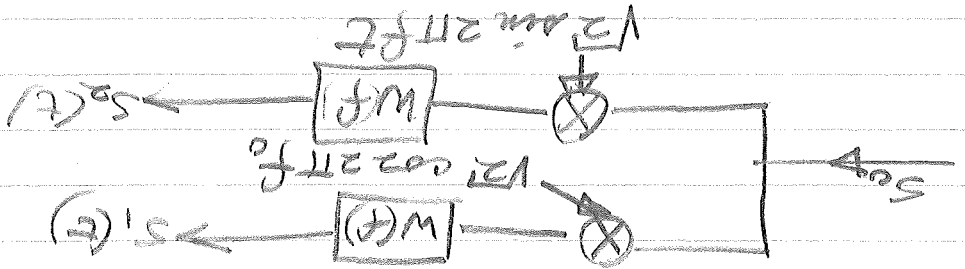


$$s_0(t) = s_1(t) \sqrt{2} \cos 2\pi f_0 t + s_2(t) \sqrt{2} \sin 2\pi f_0 t$$

(QUADRATURE MULTIPLEXING)

IGNORE CHANNEL EFFECTS

HOW DO WE RECOVER $s_1(t)$ & $s_2(t)$



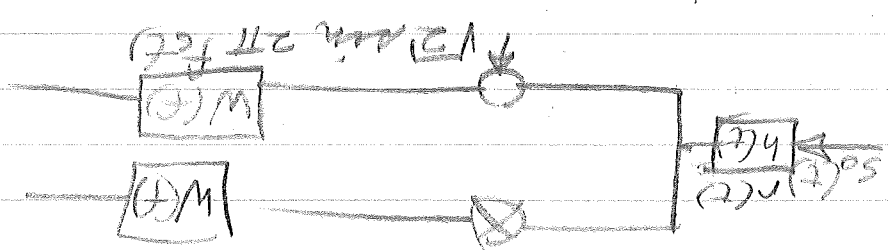
$$\frac{1}{T} \int_{-\infty}^{\infty} H(f) [S_1(f-f_0) + S_1(f+f_0)] df = H(f_0)$$

$$= \frac{1}{T} \int_{-\infty}^{\infty} H(f) [S_1(f-f_0) + S_1(f+f_0)] df$$

$$= \frac{1}{T} \int_{-\infty}^{\infty} H(f) [S_1(f-f_0) + S_1(f+f_0)] df$$

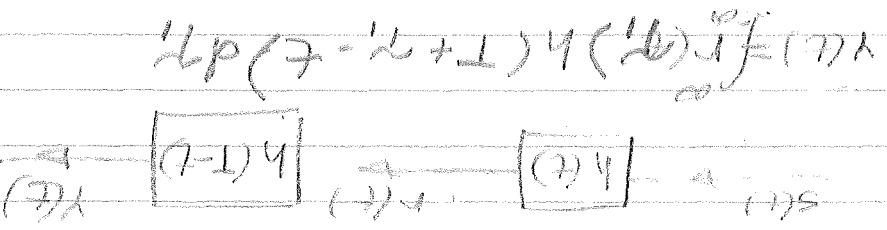
$$= \frac{1}{T} \int_{-\infty}^{\infty} H(f) [S_1(f-f_0) + S_1(f+f_0)] df$$

THE INPUT TO THE LOW-PASS FILTERS
 COS CHANNEL
 $\sqrt{2} \cos 2\pi f_0 t \rightarrow$ SPECTRUM $\frac{1}{T} [R(f-f_0) + R(f+f_0)]$



NOW, IF CHANNEL'S INPUT IS $R(f) = S(f) H(f)$
 NOTHING AT f ORIGIN WITH
 MULTIPLIED BY $\cos 2\pi f_0 t$

FRI.

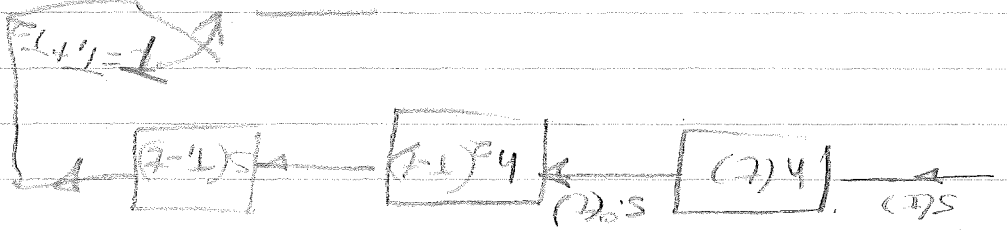


$$y(t) = \int_{-\infty}^{\infty} x(\tau) h(t-\tau) d\tau$$

$$R(f) = S(f) H(f)$$

$$Y(f) = R(f) H(f) = S(f) |H(f)|^2 e^{-j2\pi f T}$$

$$= S(f) |H(f)|^2 e^{-j2\pi f T}$$



SEQUENCE OF INPUT PARAMETERS

COMMUNICATING THE FOLLOWING
 RANDOM VECTOR $\underline{m} = (m_1, m_2, \dots, m_M)$
 EACH m_k IS CONTINUOUS RV.
 PRIOR TO THIS, ALL MESSAGES
 WERE DISCRETE OR FINITE IN

LINEAR MODULATION:

ORTHONORMAL

$$s_m(t) = \sqrt{A} \sum_{k=1}^M m_k \phi_k(t)$$

TRANSMITTER GAIN

OBJECT: ESTIMATE $\underline{m} = (m_1, \dots, m_M)$

INPUT INTO MATCHED FILTER $\frac{A}{T} = \sum m_k \phi_k(t) + \frac{A}{T} h(t)$

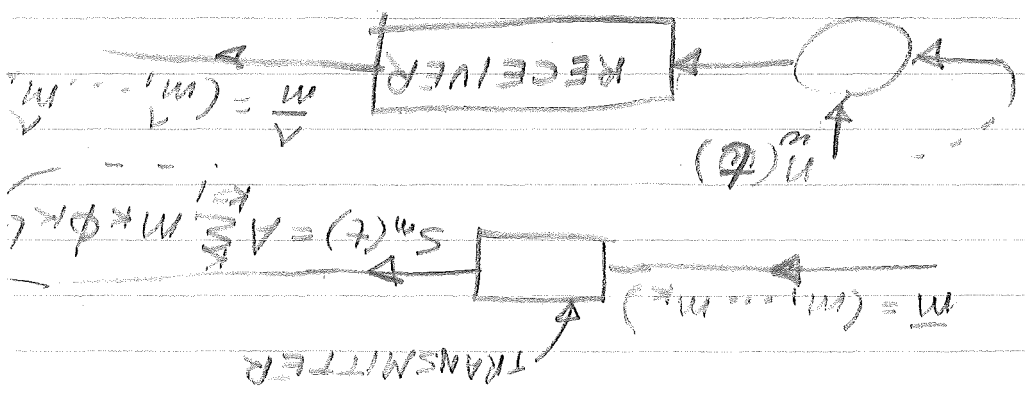
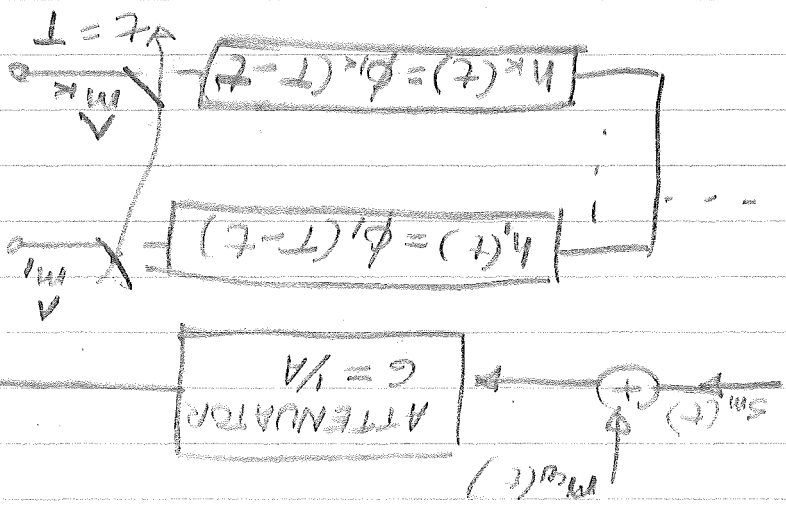
OUTPUT OF FILTER ①

$$= \sum_{k=1}^M m_k \int_{-\infty}^{\infty} \phi_k(t) \phi_k(t+T-t) dt + \int_{-\infty}^{\infty} h(t) \phi_1(t+T-t) dt$$

$$= \sum_{k=1}^M m_k \int_{-\infty}^{\infty} \phi_k(\tau) \phi_k(\tau) d\tau + \int_{-\infty}^{\infty} h(\tau) \phi_1(\tau) d\tau = m_k$$

$$= m_1 + \sum_{k=2}^M m_k = \sum_{k=1}^M m_k = P_{1/A} \Rightarrow P_1 = A m_1 = m_1$$

= RECEIVED 1st COMPONENT



$$\text{ERROR} = \hat{m}_1 - m_1 = \frac{1}{N} \sum_{n=1}^N x_n$$

MEAN SQUARE ERROR

PER COMPONENT

$$= E[|\hat{m}_1 - m_1|^2] = E\left[\frac{1}{N^2} \sum_{n=1}^N x_n^2\right]$$

$$= \frac{2\sigma^2}{N} \Rightarrow \sigma^2 / 2 \text{ IS}$$

SPECTRAL DENSITY OF

THE WHITE GAUSSIAN NOISE

$$\overline{\epsilon^2} = \frac{1}{k} \sum_{k=1}^k E[|\hat{m}_k - m_k|^2]$$

$$= \frac{1}{k} E[(\hat{m}_1 - m_1)^2 + \dots + (\hat{m}_k - m_k)^2]$$

$$= \frac{1}{k} E[|\hat{m} - m|^2]$$

$$= \frac{1}{k} \frac{k \sigma^2}{N \sigma^2} = \frac{2\sigma^2}{N \sigma^2}$$

(AGREES WITH ABOVE)

$$p_m(\alpha) p_r(p/m=\alpha)$$

$$= P_{r,m}(p,\alpha) = P_m(\alpha|r=p) p_r(p)$$

IN ORDER THAT THE A POSTERIORI

PROB. DENSITY $P_m(\alpha|r=p)$

BE MAXIMIZED, WE MUST

BE MAXIMIZED, WE MUST WITH

$$p_r(p)$$

RESPECT TO α

$$\Rightarrow p_m(\alpha) p_r(p/m) \text{ IS MAX}$$

LIKELIHOOD FUNCTION
UPON MAXIMIZING, OUR
LIKELIHOOD FUNCTION, WE
HAVE MAXIMUM LIKELIHOOD
RECEPTION

$$r = n + m$$

$\Rightarrow p_r(p/m = \alpha) = p_r(p - \alpha/m = \alpha)$
NOISE \neq MESSAGE IND.
 $\Rightarrow p_r(p - \alpha) = p_r(p - \alpha)$, WHICH CAN
BE MAXIMIZED.

IN k DIMENSIONS
BECAUSE $n_w(t)$ IS WHITE
GAUSSIAN NOISE, THE
LIKELIHOOD FUNCTION
IN k DIMENSIONS IS

$$p_r(p/m = \alpha) = p_r(p - \alpha/m)$$

$$= \frac{1}{T} (\pi N_0)^{k/2} e^{-1/2 \alpha^2 / N_0}$$

$$= \frac{1}{k} \frac{1}{\sqrt{\pi N_0}} e^{-1/2 \alpha^2 / N_0}$$

(NOTE $r_k = A m_k + n_k$)

THE VECTOR \hat{x} THAT MAXIMIZES THIS FUNCTION (FOR A GIVEN VALUE \hat{y} OF THE RANDOM VECTOR \mathbf{r}) IS $\hat{x} = \hat{y}/A = \hat{y}/(m + n/A) = \hat{y}/m$. THIS IS A LINEAR RECEIVER BECAUSE THE ESTIMATE \hat{x} OF \mathbf{m} IS A LINEAR FUNCTION OF THE RECEIVED VECTOR \hat{y} . RECALL $\hat{y} = \mathbf{m} + \mathbf{n}\mathbf{r}$ WAS ALSO THE RECEIVER IMPLEMENTED BEFORE

MONDAY

7-2 EX)



$$V_c \frac{y_c}{y} = \frac{SL + SC}{SC} = \frac{K_c}{S^2 + W_c^2}$$

SAMPLING THEOREM; OR HOW TO REDUCE CONTINUOUS (ANALOG) DATA TO DISCRETE (DIGITAL)

IF $z(t)$ IS A FINITE ENERGY

WAVEFORM WHOSE FOURIER

TRANSFORM IS IDEALLY

0 FOR $|f| > W_m$, THEN

$$z(t) = \sum_{k=-\infty}^{\infty} z_k \psi_k(t)$$

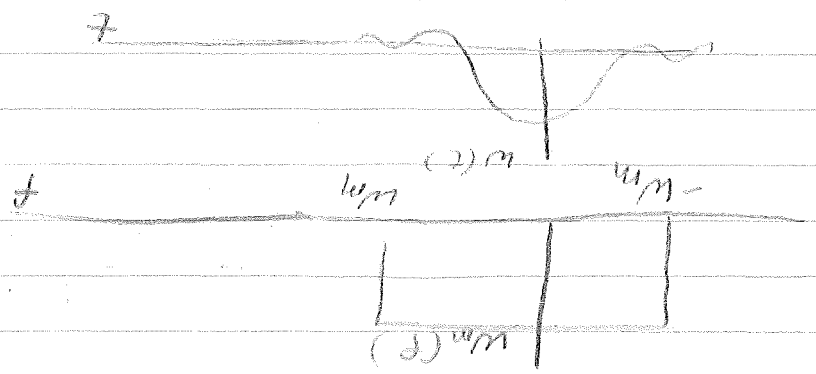
WHERE $z_k = \int_{-\infty}^{\infty} z(t) \psi_k(t) dt$

AND $\psi_k(t) = \psi(t - \frac{k}{2W_m})$

$$\psi(t) = \sqrt{2W_m} \text{ sinc}(2W_m t)$$

OBSERVATIONS:

1) IMPULSE RESPONSE OF L.P. FILTER



2) $\psi_k(t)$ ARE ORTHONORMAL

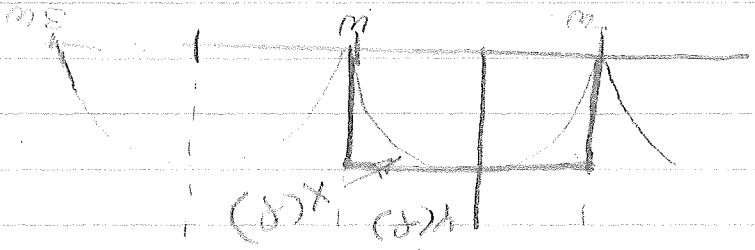
$$\int_{-\infty}^{\infty} \psi_k(t) \psi_p(t) dt = \int_{-\infty}^{\infty} \psi_k(t) \psi_p(t) dt = \delta_{kp}$$

$$= 0 \quad k \neq p$$

$$= 1 \quad k = p$$

$$k = k$$

$$\int_{-\infty}^{\infty} \psi_k(t) \psi_p(t) dt = \delta_{kp}$$



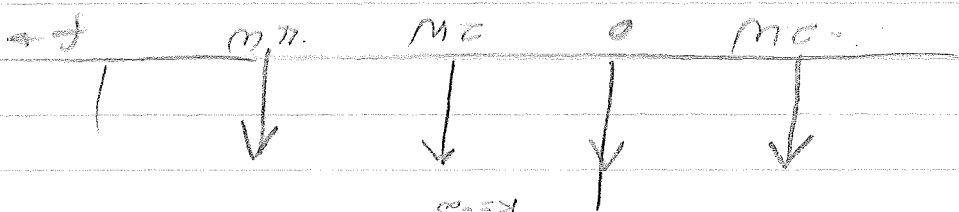
$$Y(f) = \int_{-\infty}^{\infty} X(f) U(f - \beta) df$$

$$= 2W \sum_{k=0}^{\infty} X(f - 2kW)$$

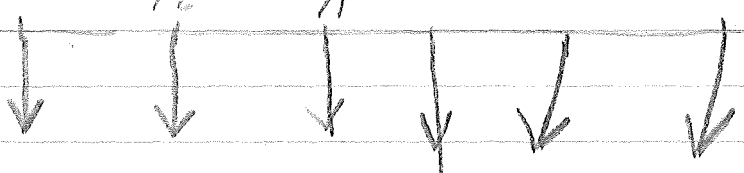
THEN

$$Y(f) = X(f) U(f) = \sum_{k=-\infty}^{\infty} X\left(\frac{f}{2W}\right) \delta(f - 2kW)$$

OUTPUT OF IMPULSE MODULATOR



$$U(f) = \sum_{k=-\infty}^{\infty} \delta(f - 2kW)$$



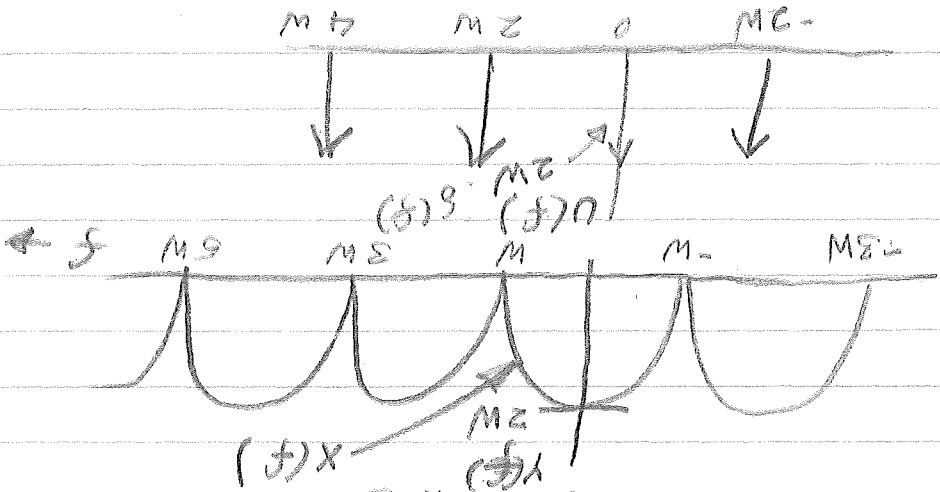
IMPULSE MODULATION $U(f) = \sum_{k=-\infty}^{\infty} \delta(f - 2kW)$

$$Z(f) = \sum_{k=-\infty}^{\infty} K_2 \int_{-\infty}^{\infty} y_k(t) \psi_k(t) dt$$

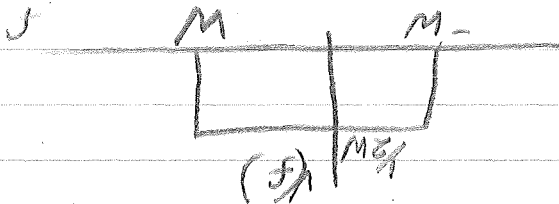
MON: TWO WEEKS FROM TODAY

$$Y(t) = X(t) \sum_{k=-\infty}^{\infty} X\left(\frac{t}{2M}\right) \delta\left(t - \frac{2M}{k}\right)$$

↑
IMPULSE TRAIN



CAN REGAIN THRU FILTER
 $\Rightarrow X(f) = Y(f) V(f)$



OR $X(t) = Y(t) * V(t)$

$$= \int_{-\infty}^{\infty} Y(\tau) V(t - \tau) d\tau$$

$$= \sum_{k=-\infty}^{\infty} X\left(\frac{2M}{k}\right) V\left(t - \frac{2M}{k}\right)$$

$$= \sum_{k=-\infty}^{\infty} X\left(\frac{2M}{k}\right) \underbrace{\sum_{n=-\infty}^{\infty} \delta\left(t - \tau - \frac{2M}{k}\right)}_{\text{INTERPOLATION FUNCTION}}$$

FIG 8-13b

RANDOM WAVE FORM: $m(t) = \sum_{k=1}^K m_k \psi_k(t)$

$$\exists m_k = \int_{-\infty}^{\infty} m(t) \psi_k(t) = \sqrt{\frac{2W_m}{K}} m_k(t)$$

$$\exists m_k = \int_{-\infty}^{\infty} m(t) \psi_k(t) = \sqrt{\frac{2W_m}{K}} m_k(t)$$

COMMUNICATE, AND THEN ESTIMATE THIS DATA

RECEIVER ESTIMATES m_k , AND THEN CONSTRUCTS ESTIMATED WAVEFORM: $\hat{m}(t) = \sum_{k=1}^K \hat{m}_k \psi_k(t)$

(NOTE $\hat{m}(t)$ IS BANDLIMITED)

MAXIMUM LIKELIHOOD

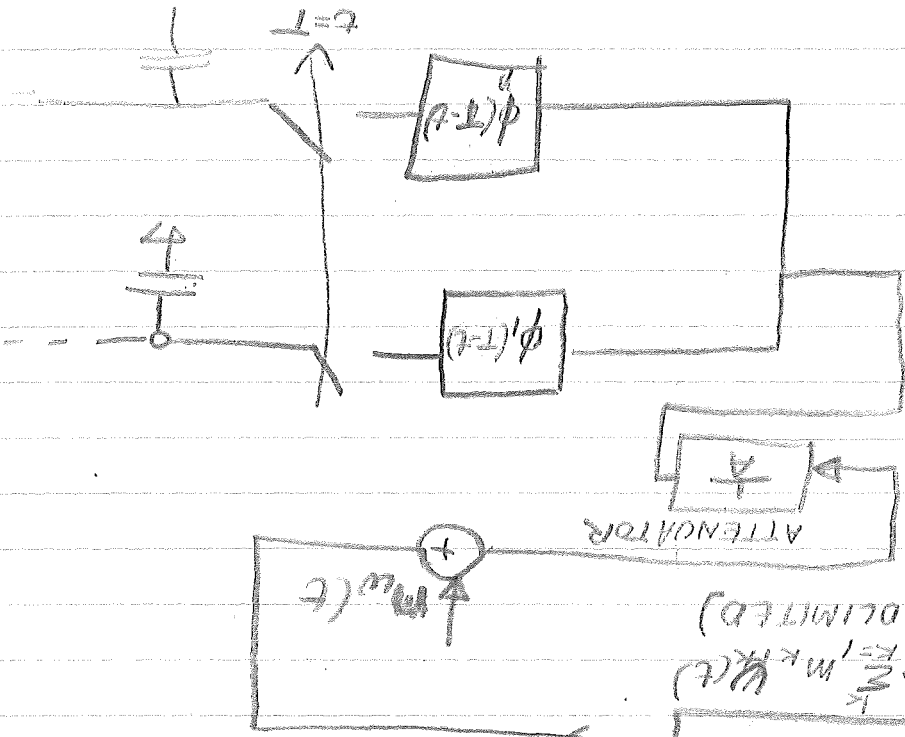
ANOTHER ORTHONORMAL FUNCTION

$$s_m(t) = \sqrt{\frac{2W_m}{K}} \sum_{k=1}^K m_k \phi_k(t)$$

TRANSMITTER

$$m(t) = \sum_{k=1}^K m_k \psi_k(t)$$

(BANDLIMITED)

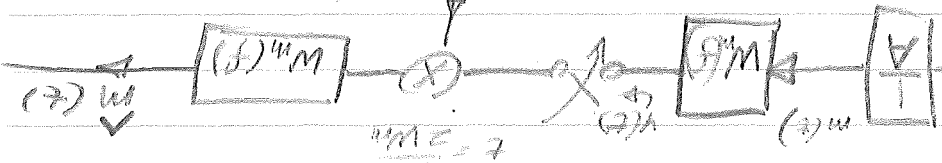


$$\tau \omega, \omega_m = \left(\frac{\omega}{\omega_m} \right) \Rightarrow \tau \omega_m = \omega$$

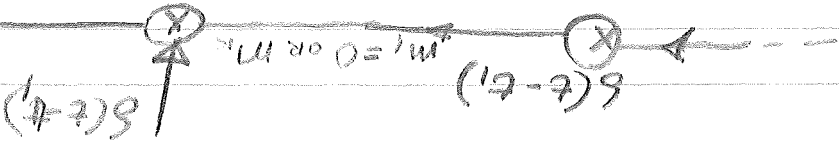
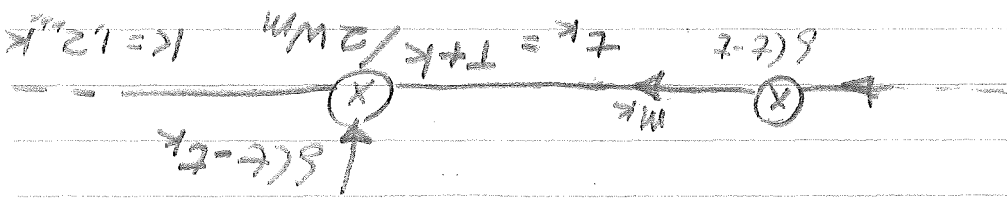
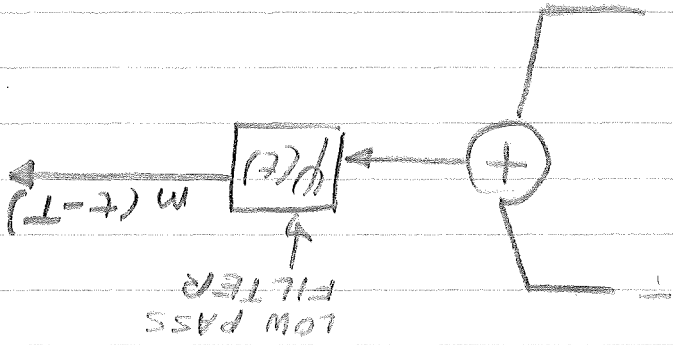
$$\phi(\tau) = \phi(\omega - \tau)$$

$$\Rightarrow \tau \left(\frac{\omega}{\omega_m} \right) = \left(\frac{\omega}{\omega_m} \right) \tau \Rightarrow \tau \omega = \omega$$

$$-k \leq \tau \leq k$$

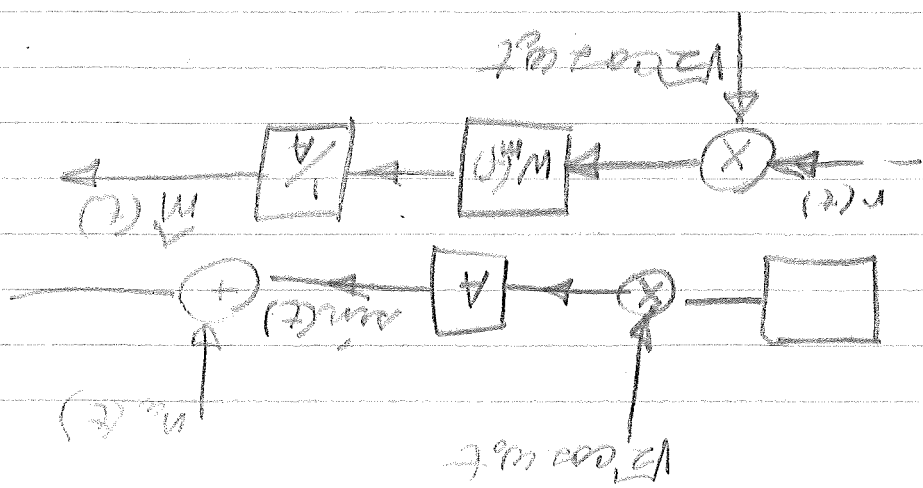
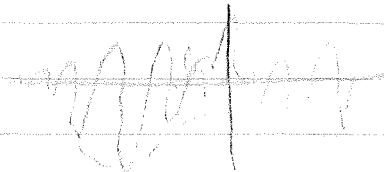


MAY ALSO REPLACE ϕ BY ψ , AND REPLACE BY LP FILTER



DSB WITH CARRIER

MAXIMUM LIKELIHOOD: DSB-SC



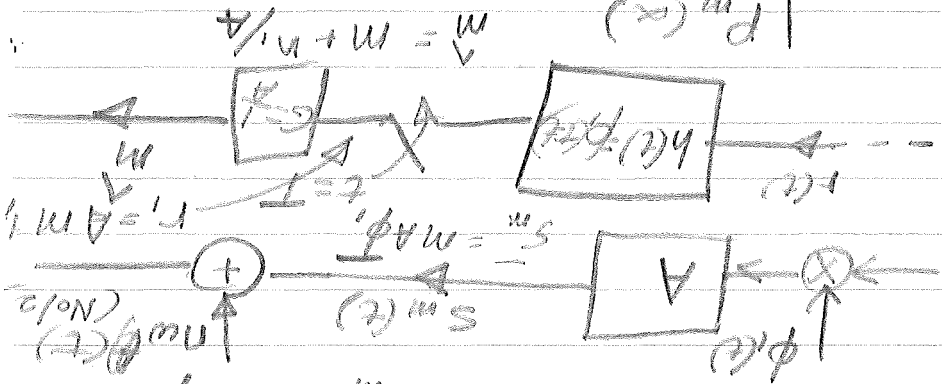
mean $\mu = 0$
 var $\sigma^2 = 2$
 0.1-1-19 (0.21-0.2)
 SKIP SHIT-1100 639-190
 A.L.S. / BUT 116

NON

TWISTED MODULATION:

(NON LINEAR)

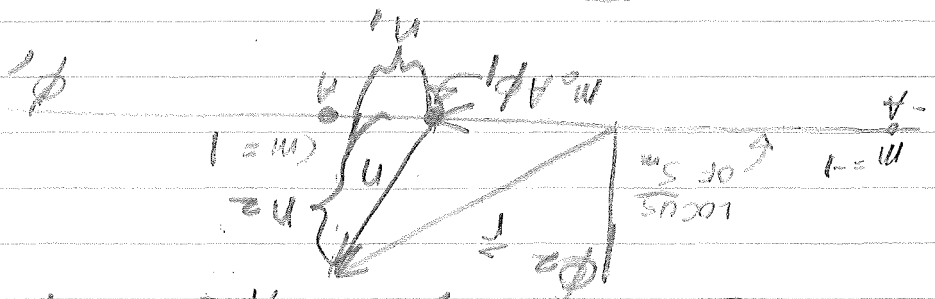
LINEAR MODULATION:



$P_m(\omega)$



$$\epsilon_2 = \frac{(m-m)^2}{(m/2)^2} = \frac{N/2}{N/2}$$



$A = \left| \frac{dS_m}{dM} \right|$ (THE "STRETCH OF THE SIGNAL LOCUS

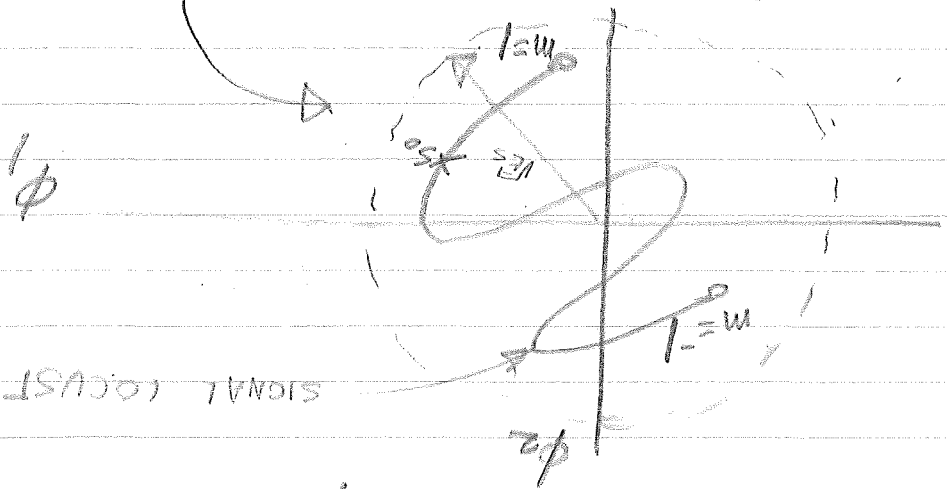
DEFINE STRETCH:

$$\epsilon_2 = \frac{N/2}{N/2}$$

FOR LINEAR MOD, $A=S$

ASSUME: $\left| \frac{d s_m}{d m} \right| = \frac{1}{T}$, A CONSTANT
 INDEPENDENT OF m , TOTAL
 LENGTH OF m , LOCUST.

IF $\int_{-\infty}^{\infty} s_m(t) dt \leq E_s$



$\Rightarrow s_m(t) = a_1(m)\phi_1 + a_2(m)\phi_2$
 FOR LINEAR, MOD, $a_1(m)$ and $a_2(m)$ WOULD BE LINEAR
 FUNCTIONS OF m , FOR
 NON-LINEAR (TWISTED) COMM
 $a_1(m) \neq a_2(m)$ ARE NON LINEAR
 FUNCTIONS OF m

$s_m(t) = a_1(m)\phi_1(t) + a_2(m)\phi_2(t)$
 but $\int_{-\infty}^{\infty} \phi_1(t) dt = \int_{-\infty}^{\infty} \phi_2(t) dt$



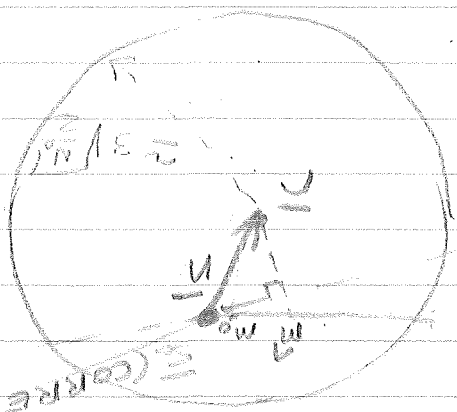
$$S_m^2 = S_0^2 + (m - m_0)^2 S_0^2$$

$$\Rightarrow S_0 = \frac{dS_m}{dm} \quad \left| \begin{array}{l} m = m_0 \\ \text{or } S_m = S_0 \end{array} \right.$$

CONDITIONAL: S_0

$$E[(m - m_0)^2 | m = m_0] = \frac{1}{S_0^2}$$

UNCONDITIONAL $S_0^2 = \frac{1}{N_0/2} = \frac{1}{10/4}$



(CORRESPONDS TO INPUT NO)

$$S_0^2 = \frac{1}{N_0/2}$$

WEAK NOISE SUPPRESSION

$$S = \frac{2}{1}$$

MAXIMUM LIKHOOD RECEIVER DESIGN
FOR ADDITIVE W.G.N.

$$p_m(\alpha|p) = p_r(p|m=w_0) p_m(\alpha)$$

$$= p(p) p_m(\alpha|p)$$

$$\Rightarrow p_m(\alpha|p) = \frac{p_r(p|m=\alpha) p_m(\alpha)}{p_r(p|m=\alpha) p_m(\alpha)}$$

$$p_r(p|m=\alpha) \propto e^{-|p-\alpha|^2/N_0}$$

$$\text{MAXIMIZE } p \cdot s_a - \frac{\gamma}{2} E_s$$

WISH NO MAXIMIZE

$$(p-s_a)(p-s_a) = |p-s_a|^2 = |s_a|^2 + 2p \cdot s_a - \frac{\gamma}{2} E_s$$

NOT $f(\alpha)$

$$p \cdot s_a - \frac{\gamma}{2} E_s = \int_{-\infty}^{\infty} p(t) s_a(t) dt = \frac{\gamma}{2} E_s$$

CORRELATION DETECTION

LINEAR MODULATION:

$$s_a(t) = \alpha A \phi(t)$$

THIS

$$\int_{-\infty}^{\infty} p(t) s_a(t) dt = \frac{\gamma}{2} E_s$$

$$= \alpha A \int_{-\infty}^{\infty} p(t) \phi(t) dt = \frac{\gamma}{2} E_s$$

$$= \alpha A p - \frac{\gamma}{2} \alpha^2 A^2$$

DIFFERENTIATE TO FIND MAX

$$\Rightarrow \frac{d}{d\alpha} = p/A = \alpha + \frac{\gamma}{2} A$$

TRANSMITTED ENERGY $|s_m|^2 = E_s$

MAXIMUM LIKELIHOOD

RECEIVER:

$P_s(p/m=\alpha)$ IS TO BE MAXED

$$\alpha \int_{-\infty}^{\infty} p(r) s_m^*(f) df$$

$$P_m(\alpha/r-p) = \frac{P_s(p)}{P_r(p/m=\alpha)}$$

$$\alpha = \sqrt{E_s} \int_{-\infty}^{\infty} p(r) \phi^*(r-\alpha T_0) dr$$

THIS IS THE OUTPUT OF A

FILTER MATCHED TO $\phi(-t)$

so $h(t) = \phi(-t)$ WHEN INPUT

IS $p(t)$



$$\text{OUTPUT} = \int_{-\infty}^{\infty} p(q) h(t-q) dq$$

$$= \int_{-\infty}^{\infty} p(q) \phi(t-q) dq$$

$$= \int_{-\infty}^{\infty} p(r) \phi(r-\alpha T_0) dr$$

SINCE $\phi(t) = \phi(-t)$ (FOR A LP

FILTER), A MAXIMUM LIKELIHOOD

RECEIVER PASSES $p(t)$ THRU

A LP FILTER $W(f)$, THEN

DETERMINES THE TIME

INSTANT t_0 - $T_0 \leq t_0$

AT WHICH THE OUTPUT

IS MAX, AND SETS $m = \sqrt{E_s}$

FOR PAM = $\frac{N_0}{2E_s}$

$\Rightarrow E_s = \frac{N_0}{2} = \frac{12}{2} \left(\frac{4 \times 10^3}{1} \right) \frac{2E_s}{N_0}$

NOTE: S^2 INDEPENDENT OF m

$S^2 = \frac{E_s}{T_s} (2\pi T_s W)^2$

USING PARSEVAL'S THEM: $S^2 = E_s T_s \int_{-W}^W |f(\omega)|^2 d\omega$

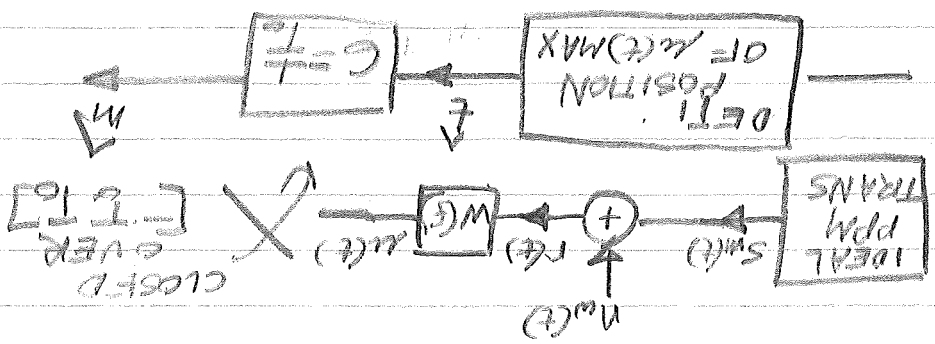
$\phi(t) = \sqrt{2W} \int_{-W}^W e^{j\omega t} d\omega$

$\Rightarrow S^2 = \int_{-E_s T_s}^{E_s T_s} \left[\int_{-\infty}^{\infty} \phi'(t - mT_s) \right]^2 dt$

$S_m(t) = \sqrt{E_s T_s} \phi'(t - mT_s)$

$S_m(t) = \sqrt{E_s T_s} \phi(t - mT_s)$

$S^2 = \int_{-\infty}^{\infty} \left[\frac{E_s}{T_s} S_m(t) \right]^2 dt$



IN SUCCESSION, AND
 LIKELIHOOD RECEIVER

ESTIMATED BY A MAXIMUM
 MK IS TRANSMITTED AND
 WITH P.P.M., EACH MESSAGE,

ASSUME $m_k \leq W_m$

$$m(t) = \sum_{k=-\infty}^{\infty} m_k \phi_k(t)$$

LOW PASS WAVEFORM

WAVEFORM COMM. WITH P.P.M.

$$\Delta f_{PPM} = \frac{1}{B} \left(\frac{1}{2T_s} \right)$$

$$\therefore \frac{\Delta f}{B} = \frac{1}{2T_s} \left(\frac{1}{2T_s} \right)$$

CALLLED EFFECTIVE DIMENSIONALITY
 COMMON. - TO S(S)CTO AND - W(S)CTO
 SAME # OF SAMPLES TO
 $\Rightarrow 4T_s W = \text{TWICE } B.W. \times \text{SIGNAL INTERVAL}$



CONSIDER $4T_s W$; SIGNAL $BW = W$
 SIGNAL INTERVAL $T_s = 2T_0$

FOR LIN MOD.

$$(m_1 + m_2) \phi(t) = m_1 \phi(t) + m_2 \phi(t)$$

$$\frac{\Delta f}{B} = \frac{1}{2T_s}$$

AVE. OUTPUT NOISE PWR

$$= \overline{n^2(t)} = 2W_m S_n(f)$$

$$= 2W_m \int_{-W_m}^{W_m} \frac{N_0}{2} df$$

OR $\overline{n^2(t)} = \frac{12}{12} \frac{N_0 W_m}{2}$

FOR LINEAR MOD: $\overline{n^2(t)} = N_0 W_m / 2$

= STATIONARY GAUSSIAN
 PROCESS WITH SPECTRAL
 DENSITY $S_n(f) = \begin{cases} \frac{N_0}{2} & |f| \leq W_m \\ 0 & \text{ELSEWHERE} \end{cases}$

PRODUCES m_k . THE
 RECEIVER CONSTRUCTS
 $\hat{m}(t) = \sum_{k=0}^{K-1} m_k \psi_k(t)$

$m_k = m_k + n_k$

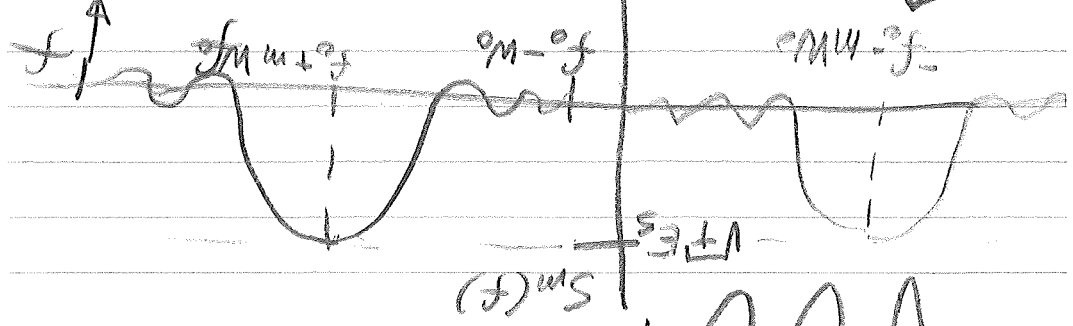
$\Rightarrow \hat{m}(t) = m(t) + n(t)$

$n(t) = \sum_{k=0}^{K-1} n_k \psi_k(t)$

$$s^2 = \frac{3}{5} = \frac{3}{5} = \frac{3}{5}$$

$$\beta = 4TW_0$$

$$f_0 + W_m \quad f_0 - W_m$$



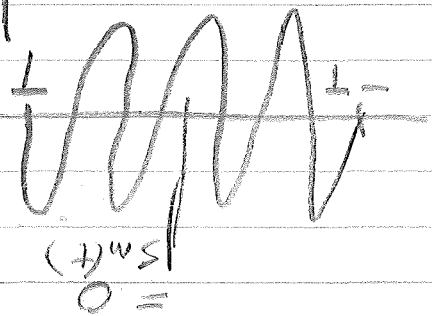
$$f_0 > W_m$$

$$-W_m < f_0$$

OTHERWISE

$$s_m(t) = V_T E_s \phi_m(t)$$

$$\phi_m(t) = \frac{1}{\sqrt{m}} \cos 2\pi(f_0 + W_m t) \dots$$



FREQUENCY POSITION MODULATION

TIME AVAILABLE FOR TRANSMISSION OF EACH MK IS THE SAMPLING INTERVAL $2W_m$. THUS, MAX DEVIATION FOR EACH TRANSMISSION IS $2W_m$. IF WE SET $2f_0 = 1/2W_m$ THEN WE GET $4f_0 W = \beta = W/W_m = \text{B.W. EXPANSION RATIO}$

$$\frac{P^2(t)}{P_s} = \frac{12}{12} \left(\frac{W_m}{W_c} \right)^2 \approx \frac{N_0 W_m}{P_s}$$

MON
FM

$$S_m(t) = A\sqrt{2} \cos 2\pi [f_c t + W \int m(t) dt]$$

INSTANTANEOUS
PHASE

$$f_{INST} = \frac{d}{dt} [f_c t + W \int m(t) dt] = f_c + W m(t)$$

SPECTRUM: LET $m(t) = \cos 2\pi W_m t$

$$W_c = 2\pi f_c \quad W_m = 2\pi W_m$$

$$S_m(t) = A\sqrt{2} \cos \left(W_c t + \frac{W_m}{W_c} \sin W_m t \right)$$

$$B = W_c / W_m$$

$$S_m(t) = A\sqrt{2} \cos(B \sin W_m t) \cos W_c t$$

$$- A\sqrt{2} \sin(B \sin W_m t) \sin W_c t$$

$$J_k(B) = \frac{1}{2\pi} \int_{-\pi}^{\pi} e^{jB \sin t} dt$$

3-19-71

MON 2.12, 2.23, 2.24 COMM PROBS EX 9N 78

(3.4 3.5) 3.4 3.6 3.7 3.8 CORR. REC.

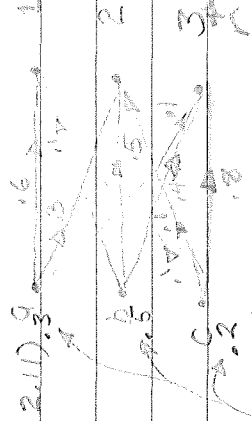
ALL OF CHAPT 4 MATCHED FILTER

SKIP CHAPT 5, 6

CHAPT 7, 2

CHAPT 8; 1, 2, 3, 5

LECTURE



APRIORI PROB = PROB. THAT g, h, c WERE

SENT AFTER HEARING A 1, 2, 3

$P[m_k] =$ APRIORI PROB. OF k^{TH} MESSAGE

$P[r_j | m_k] =$ CONDITIONAL PROB

OF RECEIVING THE j^{TH} r GIVEN

OR CONDITIONED UPON TRANSMITTING

THE k^{TH} MESSAGE

$(P[m_k] P[r_j | m_k]) = P[m_k, r_j] = P[m_k | r_j] P[r_j]$

$P[m_k, r_j] =$ PROB. OF THE "JOINT

EVENT m_k TRANSMITTED AND

r_j IS RECEIVED (APRIORI PROB)

→ BAYES RULE

$$P[m_k | r_j] = \frac{P[m_k, r_j]}{P[r_j]}$$

$$P[m_k | r_j] = \frac{P[m_k, r_j]}{P[r_j]}$$

↑ ↑
FIXED FIXED

WANT VALUE OF m_k TO MAX. $P[m_k | r_j]$

$$P[m_k, r_j] = \frac{P[m_k] P[r_j | m_k]}{P[r_j]}$$

MAXIMIZING \Rightarrow MAXIMIZING

$$P[m_k] P[r_j | m_k]$$

$$P[r_j] = P[r_j, m_1] + P[r_j, m_2] + P[r_j, m_3]$$

$$P[1] = P[1, a] + P[1, b] + P[1, c]$$

$$= (.3)(.6) + (.5)(.1) + (.2)(.1)$$

$$P[2] = P[2, a] + P[2, b] + P[2, c]$$

$$= (.3)(.3) + (.5)(.5) + (.2)(.1)$$

$$= .36$$

$$P[3] = .39$$

$$P[1, a] = .18; \quad P[1, b] = .05 \quad P[1, c] = .02$$

$$P[2, a] = .09 \quad P[2, b] = .25 \quad P[2, c] = .02$$

$$P[3, a] = .03 \quad P[3, b] = .20 \quad P[3, c] = .16$$

RECEIVER DECISION RULE

$$\hat{m}(1) = a \quad (.18)$$

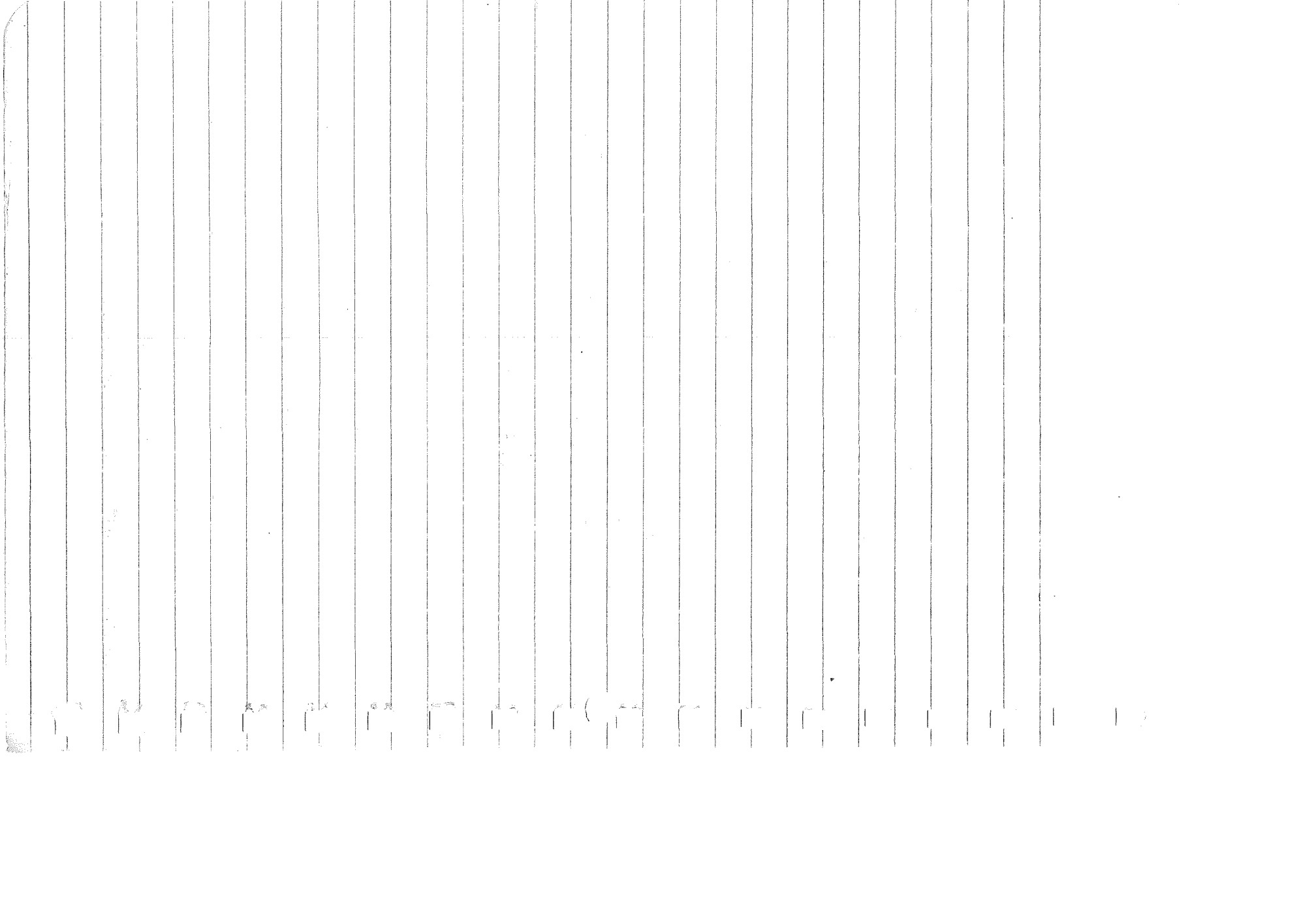
$$\hat{m}(2) = b \quad (.25)$$

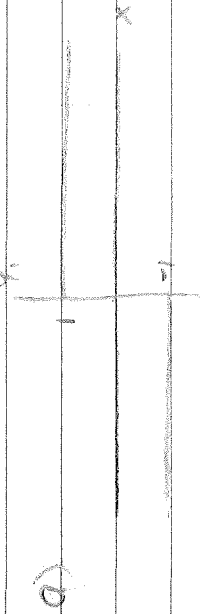
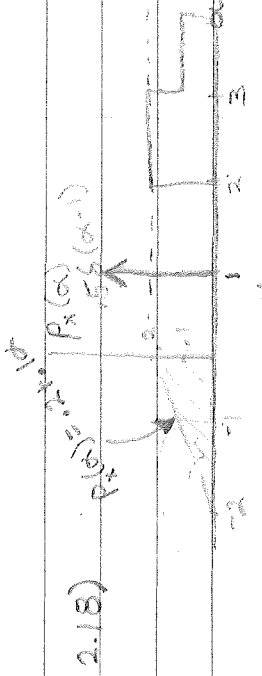
$$\hat{m}(3) = b \quad (.20)$$

$$b) P[c] = .18 + .25 + .20 = .63 \Rightarrow P[E] = .37$$

$$c) b \text{ DOMINATES } \Rightarrow P[E] = .50$$

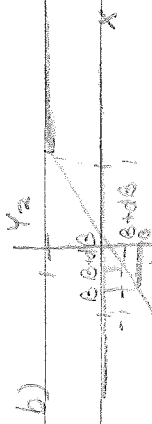
$$\hat{m}(1, 2, 3) = b$$





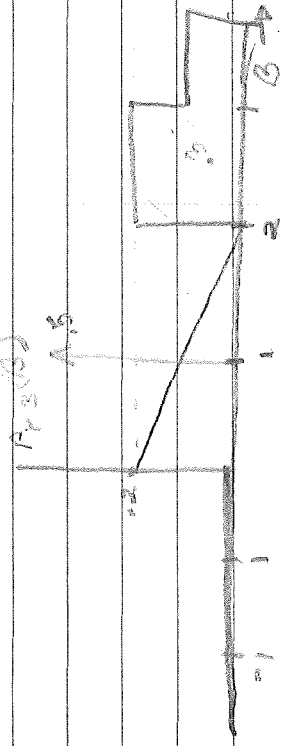
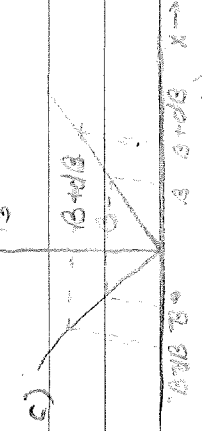
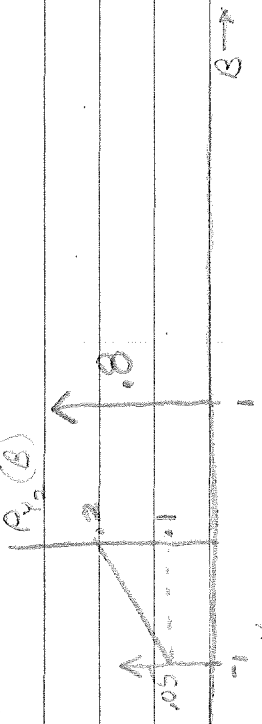
$$P_x(\beta) = 2.5(\beta+1) + 0.5(\beta+1)$$

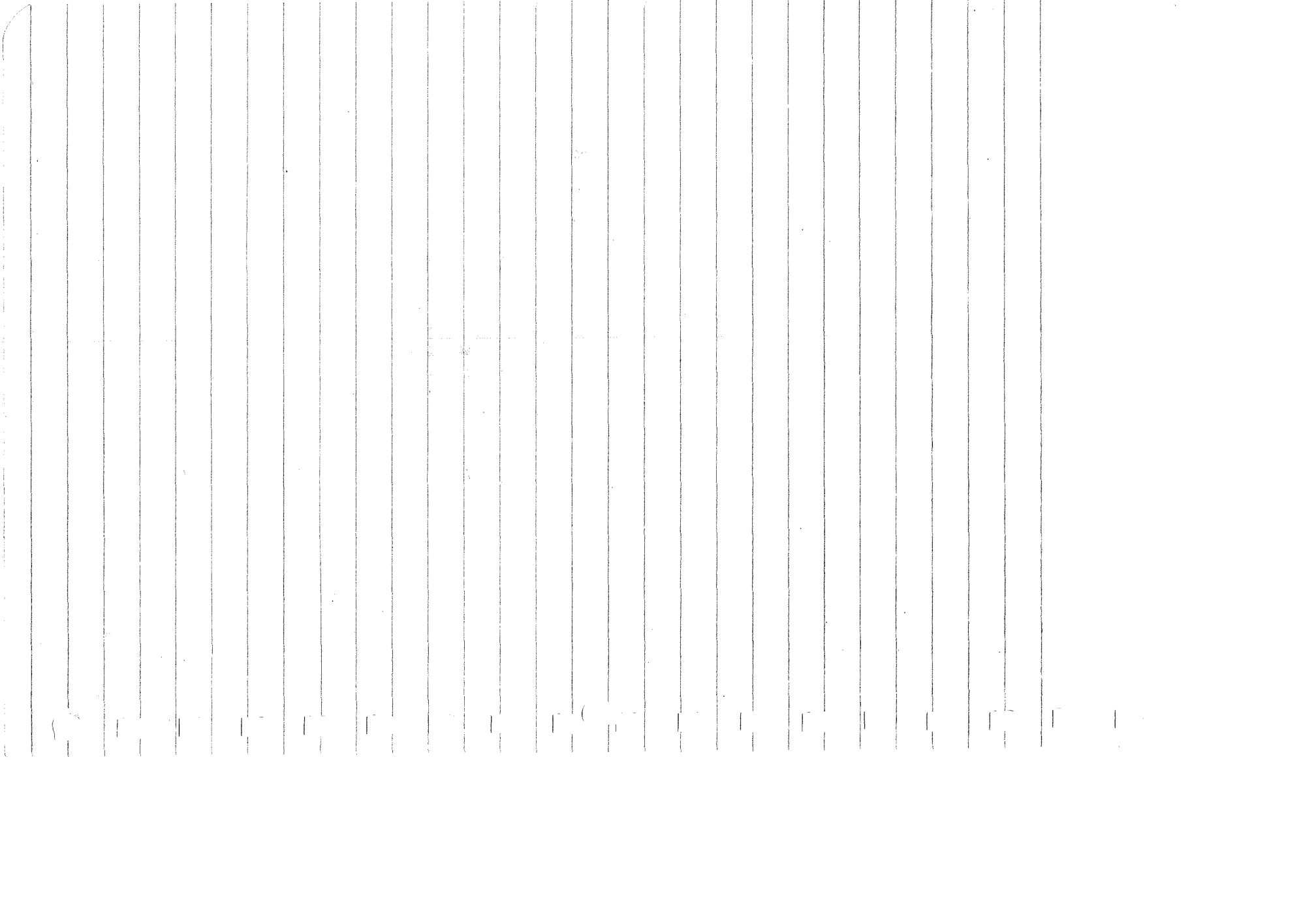
FOR $-1 < \beta < 0$, $P_x(\beta) = 2 + 1/\beta$

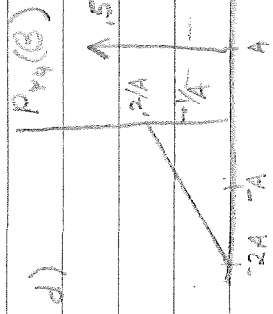


$$P_x(\beta) = 0.5\beta(\beta+1) + 0.5\beta(\beta+1) + 2 + 1/\beta$$

$-1 < \beta < 0$







e) $P_{Y_5}(B) = .56(B-1) + .16(B-2) + .156(B-3)$
 $+ .056(B-4) + .0875(B-4)$
 $+ .16(B+1) + .0128(B+2)$

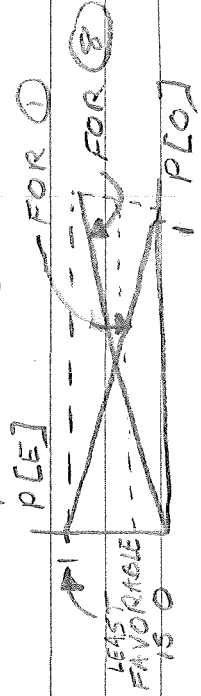
3-23-71

3.12) $(a, b, c) = (0, 0, 0), (0, 0, 1), \dots, (1, 1, 1)$

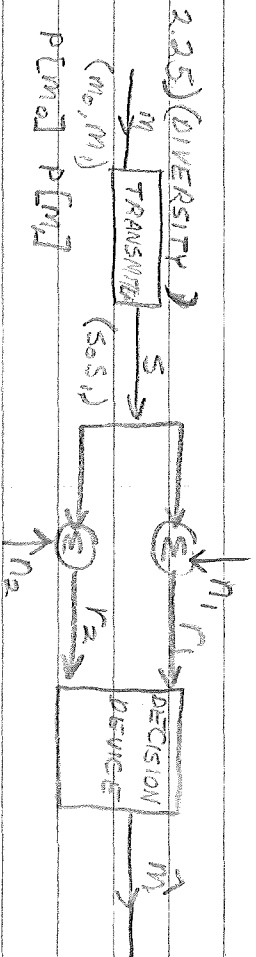
& PROB. OF MAKING CORR. CHOICE

HINT: $(0, 0, 0) \quad P[C] = P[0 \text{ WAS TRANS}]$

$P[E_1] = 1 - P[0]$



$P[E_2] = P[0]$



$S_0 = (-1)^0 \sqrt{E} = \sqrt{E}$ $S_1 = (-1)^1 \sqrt{E} = -\sqrt{E}$

$\exists E = \text{ENERGY} \propto V^2$

$n_1 = s + n_1$ $n_2 = s + n_2$

BAYES MIXED RULE:

$p_r(p|m) P[m] = P[m|r=p] p_r(p)$
 $= p_r(p, m)$ (JOINT DISTRIBUTION OF RANDOM EVENT)

WANT TO MAXIMIZE A' POSTERIORI PROB.

$P[m_i|r=p] = \frac{p_r(p|m_i) P[m_i]}{p_r(p)}$

$P[m_0|r=p] > P[m_1|r=p]$

$\Rightarrow p_r(p|m_0) P[m_0] > p_r(p|m_1) P[m_1]$

$n_0 = s + n \Rightarrow p_r(p|m_i) = ?$

$P[p < n < p + d_p | m = m_i]$

$= P[p < s + n < p + d_p | m_i]$

$= P[p - s_1 < n < p - s_1 + d_p | m = m_i]$

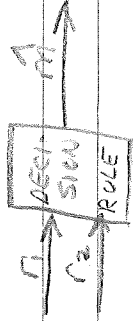
$= p_{n_i}(p - s_1 | m = m_i) dp$

$m_i \text{ IND OF } n \Rightarrow$

$= p_{n_i}(p - s_i) dp$

$\therefore p_r(p|m = m_i) = p_{n_i}(p - s_i)$

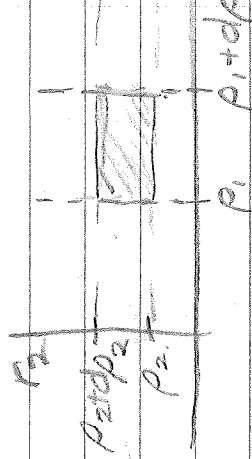
WE MUST EXAMINE THE TWO VARIABLE CASE



$$\text{WANT } P[m_0 | n] = \rho_1, r_2 = \rho_2$$

$$P[m_0 | n] = \rho_1, r_2 = \rho_2 > P[m_1 | n] = \rho_1, r_2 = \rho_2$$

$$\Rightarrow P_{r_1, r_2}(\rho_1, \rho_2 | m_0) > P_{r_1, r_2}(\rho_1, \rho_2 | m_1)$$



BY ANALOGY

$$P_{r_1, r_2}(\rho_1, \rho_2 | m_i) = P_{n_1, n_2}(\rho_1 - s_1, \rho_2 - s_2 | m_i)$$

(n_1, n_2) INDEPENDENT FROM m_i

$$= P_{n_1}(\rho_1 - s_1) P_{n_2}(\rho_2 - s_2)$$

MEAN = s^2

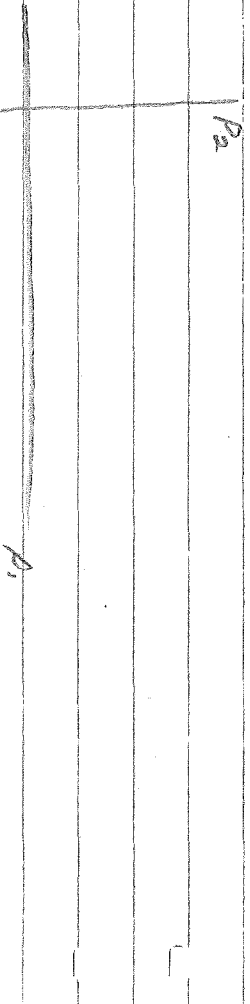
$$P_{n_1}(\rho_1 - s_1) = \frac{1}{\sqrt{2\pi}\sigma_1} e^{-\frac{(\rho_1 - s_1)^2}{2\sigma_1^2}}$$

$$P_{n_2}(\rho_2 - s_2) = \frac{1}{\sqrt{2\pi}\sigma_2} e^{-\frac{(\rho_2 - s_2)^2}{2\sigma_2^2}}$$

$$P_{r_1, r_2}(\rho_1, \rho_2 | m_0) = \frac{P[m_0]}{2\pi\sigma_1\sigma_2} e^{-\left(\frac{(\rho_1 - s_1)^2}{2\sigma_1^2} + \frac{(\rho_2 - s_2)^2}{2\sigma_2^2}\right)}$$

$$P_{r_1, r_2}(\rho_1, \rho_2 | m_1) = \frac{P[m_1]}{2\pi\sigma_1\sigma_2} e^{-\left(\frac{(\rho_1 - s_1)^2}{2\sigma_1^2} + \frac{(\rho_2 - s_2)^2}{2\sigma_2^2}\right)}$$

②



Let $p_1 = p_2 =$

$$P_{m_2}(p_1, p_2 | m_2) P(m_2) = \frac{P(m_2)}{2\pi\sigma^2} e^{-\frac{1}{2\sigma^2} [(p_1 - s_1)^2 + (p_2 - s_1)^2]}$$

$$P_{m_1}(p_1, p_2 | m_1) P(m_1) = \frac{P(m_1)}{2\pi\sigma^2} e^{-\frac{1}{2\sigma^2} [(p_1 - s_1)^2 + (p_2 - s_1)^2]}$$

ALL THAT IS NEEDED IS EXPONENTS

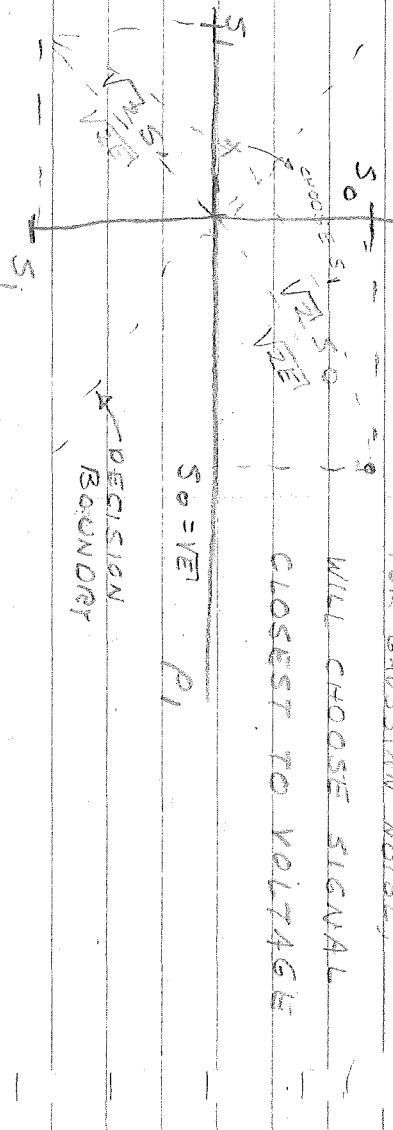
$$(p_1 - s_0)^2 + (p_2 - s_0)^2 > (p_1 - s_1)^2 + (p_2 - s_1)^2$$

$$P[m_0] = P[m_1] \Rightarrow s_0 = -s_1$$

FOR GAUSSIAN NOISE,

WILL CHOOSE SIGNAL

CLOSEST TO VOLTAGE



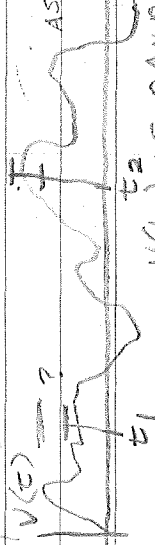
THE FARTHER APART THE POINTS,
THE BETTER THE DECISION

3-27-71

CHAPT. 3

RANDOM PROCESS:

SAMPLE FUNCTION



$$P_{X(t)}(\alpha, t_1)$$

SINGLE VAR = $V(t_1)$

$$P_{X(t_1), X(t_2)}(\alpha_1, \beta_2)$$

\vdots

$$P_{X(t_1), \dots, X(t_n)}(\alpha_1, \dots, \alpha_n)$$

IF EACH IS GAUSSIAN & IS GAUSSIAN

IF P IS DEPENDENT ONLY ON Δt ,

SYSTEM IS STATIONARY

NEED ONLY \bar{X} & \bar{X} TO DEFINE

GAUSSIAN PRODUCT

READ: 3.1, 3.2, 3.4, 3.5

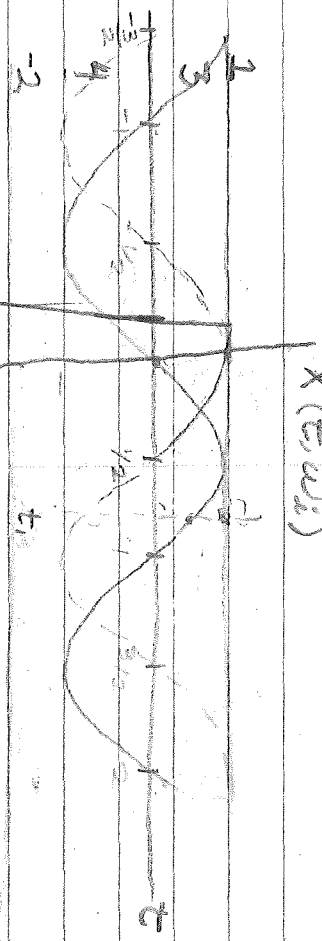
③

3.1

$$X(\omega, t) = 1 \quad X(\omega_3 t) = \sin \pi t$$

$$X(\omega_2 t) = -2 \quad X(\omega_4 t) = \cos \pi t$$

$$X(t, \omega_1)$$



a) $P[\omega_1] = 1/4$ V_i

$$P_{X(t_1)}(\alpha) = \frac{1}{4} \delta(\alpha-1) + \frac{1}{4} \delta(\alpha+2)$$

$$+ \frac{1}{4} \delta(\alpha - \sin \pi t) + \frac{1}{4} \delta(\alpha - \cos \pi t)$$

$P_{X(t_1)}(\alpha)$ CHANGES WITH TIME \Rightarrow NOT STATIONARY

b) $\bar{X}(t) = \int_{-\infty}^{\infty} \alpha P_{X(t)}(\alpha) d\alpha$

$$= \frac{1}{4} (1 - 2 + \sin \pi t + \cos \pi t)$$

$$\overline{X(t_1) X(t_2)} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \alpha \beta P_{X(t_1) X(t_2)}(d\alpha d\beta)$$

$$= R(t_1, t_2) = \text{CORRELATION FUNC.}$$

TO CALCULATE: $P_{X(t_1) X(t_2)}(\alpha, \beta)$

$$= P_{\bar{X}(t)}(\alpha) = P_{X(t_1)}(\alpha) P_{X(t_2)}(\beta / X(t_1) = \alpha]$$

WHAT IS $P_{X(t_2)}(\beta / X(t_1) = \alpha)$?

LET $t_1 = t_2$, THEN ONLY VALUES OF α ARE $-1, -2, \pm 1, 0, 1$

THEN, IF $\alpha = 1$, $P_{X(t_2)}(\beta / X(t_1) = 1)$

$$= \delta(\beta - 1) \quad (\text{MOST STAY ON SAME FUNCTION})$$

THEN, IF $\alpha = -2$, $P_{X(t_2)}(\beta / X(t_1) = -2)$

$$= \delta(\beta + 2)$$

THEN, IF $\alpha = 1, 0, -1$, $P_{X(t_2)}(\beta / X(t_1) = 1, 0, -1)$

$$= \delta(\beta - \sin \pi t_1)$$

THEN, IF $\alpha = \pm 707$, $P_x(t_2)$, $(B/x(t_1) = \pm 707)$
 $= \delta(B - \cos \pi t_2)$

$$\Rightarrow \overline{x(t_1)x(t_2)} = \overline{x(\frac{\pi}{4})x(-\frac{\pi}{4})}$$

$$= \int_{-\infty}^{\infty} \alpha \cdot B \cdot \frac{1}{4} [\delta(\alpha-1) + \delta(\alpha+2) + \delta(\alpha+707) + \delta(\alpha-707)]$$

$$P[B/x(-\frac{\pi}{4}) = \alpha] d\alpha dB$$

$$= \int_{-\infty}^{\infty} [B \cdot \frac{1}{4} [P_x(t_2) (B/x(-\frac{\pi}{4}) = 1)$$

$$\rightarrow 2P_x(t_2) (B/x(-\frac{\pi}{4}) = -2)$$

$$- 707 P_x(t_2) (B/x(-\frac{\pi}{4}) = \pm 707)]$$

$$+ \int_{-\infty}^{\infty} [B \cdot \frac{1}{4} [P_x(t_2) (B/x(-\frac{\pi}{4}) = 707)] dB]$$

$$= \int_{-\infty}^{\infty} [B \cdot \frac{1}{4} [\delta(B-1) - 2\delta(B+2)$$

$$- 707\delta(B - \sin \pi t_2 + 707\delta(B - \cos \pi t_2)] dB$$

$$\therefore \overline{x(t_1)x(t_2)} = \frac{1}{4} + 1 - \frac{707}{4} \sin \pi t_2$$

$$+ \frac{707}{4} \cos \pi t_2 = \frac{5}{4} + \frac{707}{4} (\cos \pi t_2 - \sin \pi t_2)$$

FOR $t_1 = -1/4$

CAN'T PUT AS $f(t_2 - t_1) \Rightarrow$ NOT SECOND ORDER STATIONARY

c)

$$\frac{1}{\alpha} \int_{-\infty}^{\infty} \frac{1}{B} P_{AB} = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} P_x(-t) P_x(t) (\alpha) P_x(t) dt dB$$

$$= \int_{-\infty}^{\infty} \frac{1}{4} [P_x(-t) = \alpha] dt dB$$

$$= \int_{-\infty}^{\infty} \frac{1}{4} [\delta(\alpha-1)\delta(B-1) + \delta(\alpha+2)\delta(B+2)$$

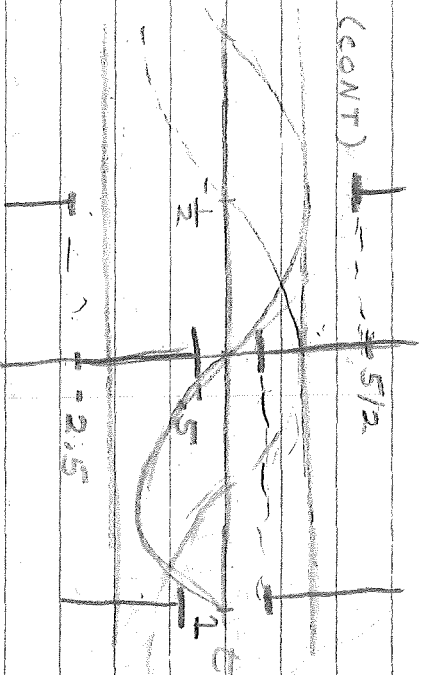
$$+ \delta(\alpha+707)\delta(B-707) + \delta(\alpha-707)\delta(B-707)] dB d\alpha$$

$$\therefore P = \frac{1}{2}$$

(CONT.)

11

c) (cont)



$$P = \frac{2}{3} = \frac{8}{12}$$

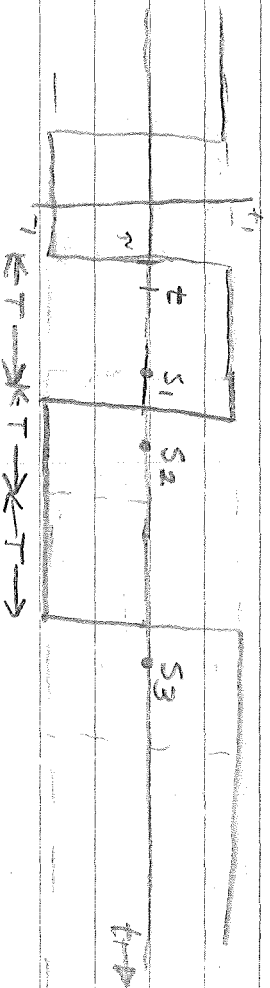
5-2-7)

010 3-9, 3-10

3-12)

R.V.

$$X(t) = \sum_{j=-\infty}^{\infty} w_j \mu_j(t - jT - \tau)$$



W_j THE VALUE OF X(t) IN THE
jTH INTERVAL, IS IND. OF w_j

THE VALUE OF X(t) IN jTH INTERVAL

∴ WHEN |t - s_j| > T, THE

CORRELATION FUNCTION

$$R_x(t, s_3) = X(t)X(s_3) = \frac{1}{2} (1-1-1+1) = 0$$

PRODUCT OF ALL POSSIBLE

PAIRS OF VALUES OF X(t) AND X(s_j)

WHEN t AND s ARE IN SAME INTERVAL

EX) LET $s = s_1$

$$\Rightarrow X(t) = X(s_1) = \frac{t}{T}$$

$$\therefore \frac{X(t)X(s_1)}{X(t)X(s_1)} = R_X(t, s_1) = 1$$

$\therefore X(t)X(s) = 1 = P[t \text{ \& } s \text{ ARE IN SAME INTERVAL}]$

$+ 0 \cdot P[t \text{ \& } s \text{ ARE NOT IN SAME INTERVAL}]$

$$= P[t \text{ \& } s \text{ ARE IN SAME INTERVAL}]$$

FROM THE FIGURE, $t \text{ \& } s$ WILL LIE

IN THE SAME T SEC. INTERVAL IFF

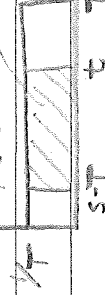
$s - T < \tau < t$. HOLDS FOR

$s > t$ (FOR EX., IN THE FIGURE)

$$P[s - T < \tau < t] = (t - s + T) \cdot \frac{1}{T} = 1 - \frac{s - t}{T}$$

$P_{\tau}(\alpha)$

$$= 1 - \frac{u}{T} \quad (u = s - t)$$



FOR $s < t$

LET $s < t$, THEN $s \text{ \& } t$ BELONGS TO

THE SAME INTERVAL IFF

$t - T < \tau < s$

$$\Rightarrow P[t - T < \tau < s] = 1 + \frac{u}{T} \quad (u = s - t)$$

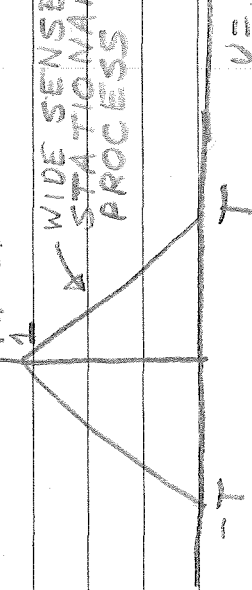
$$\therefore R_X(t, s) = R_X(s - t) = 1 + \frac{u}{T} \quad u < 0$$

$$= 1 - \frac{u}{T} \quad u > 0$$

$$= 0 \quad |u| > T$$

$R_X(u)$

WIDE SENSE
STATIONARY
PROCESS



$u = s - t$

13

AMBIGUITY FUNCTIONS

$$x(t)$$

$$x_p(t) = x(t+n)$$

DEFINE A SIGNAL SPACE

$$\{x(t), y(t), z(t), \dots, g(t)\}$$

PLUS A METRIC OR 'DISTANCE'

BETWEEN SIGNALS

$$d_{\text{DISTANCE}}(x, y) = \int_{-\infty}^{\infty} |x(t) - y(t)|^2 dt$$

$$d(x, x_p) = \int_{-\infty}^{\infty} |x(t) - x_p(t)|^2 dt$$

$$= \int_{-\infty}^{\infty} [x(t) - x(t+n)]^2 dt$$

$$= \int_{-\infty}^{\infty} [x(t) - x(t+n)] dt$$

$$= \int_{-\infty}^{\infty} [x(t)x(t) + x(t+n)x(t+n)] dt$$

$$- \int_{-\infty}^{\infty} [x(t)x(t+n) + x(t+n)x(t)] dt$$

$$(R_x(t) = \int_{-\infty}^{\infty} x(t)x(t+n) dt)$$

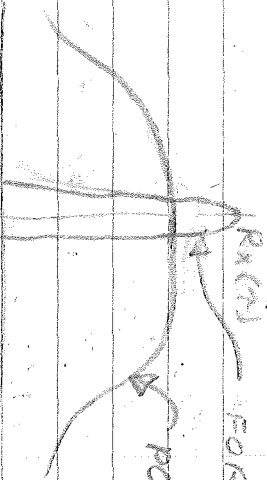
$$\Rightarrow d(x, x_p) = R_x(0) + R_x(0) - R_x(n) - R_x(n)$$

$$= 2(R_x(0) - R_x(n))$$

$R_x(n)$

FOR LITTLE AMBIGUITY

poor



5-10-71

4.1) $\sum_{i=1}^n r = S + 0$

MUST MAXIMIZE: $P[m_i] p_0(\rho/\bar{s} = \bar{s})$; $i=0,1$

FOR $i=k, \Rightarrow \hat{m} = M_k$

NOW, $P[m_i] = 1/2$ FOR $i=0,1$

IE $P[m_i]$ IS INDEPENDENT OF i .

HENCE, CHOOSE $\hat{m} = M_k$ IF

$P(\bar{\rho}/s = s_i)$ IS MAX FOR $i=k$.

$$\bar{r} = n \begin{bmatrix} 1 \\ 1 \end{bmatrix} + S \text{ OR } r_{2i} = n + S r_i$$

FORGET VECTOR NATURE: CAPTS

GIVEN p_n , WHAT IS $P_0(\rho/s = s_i)$

$$n = r - S$$

$$P(\rho/s = s_i) = p_n(\rho - s_i / s = s_i)$$

$$= p_n(\rho - s_i) \text{ (IS STATISTICALLY INDEPENDENT)}$$

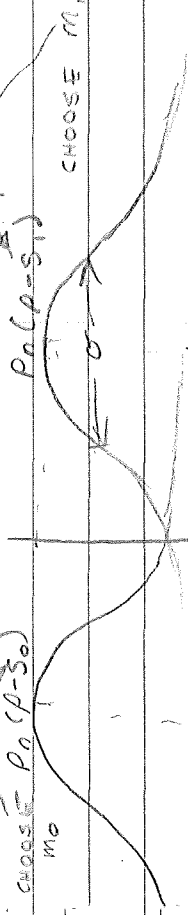
BECAUSE NOISE IS 0-MEAN GAUSSIAN

$$\Rightarrow P_0(\rho - s_i) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left(-\frac{1}{2\sigma^2}(\rho - s_i)^2\right)$$

$$\Rightarrow P_0(\rho - s_0) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left(-\frac{1}{2\sigma^2}(\rho - s_0)^2\right)$$

$$P_0(\rho - s_1) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left(-\frac{1}{2\sigma^2}(\rho - s_1)^2\right)$$

CHOOSE $P_0(\rho - s_0)$



$$P[C/m_0] = \frac{1}{\sqrt{2\pi}\sigma} \int_{-\infty}^{\infty} \exp\left(-\frac{1}{2\sigma^2}(\rho - s_0)^2\right) d\rho$$

$$= \frac{1}{\sqrt{2\pi}\sigma} \int_{-\infty}^{\infty} \exp\left(-\frac{1}{2\sigma^2}(\rho - s_0)^2\right) d\rho$$

(CONST)

(15)

$$P[C/m_0] = \frac{1}{2} + \frac{1}{\sqrt{\pi}} \sigma \int_0^{\frac{b}{2\sigma}} \exp\left(-\frac{b^2}{2\sigma^2} d^2\right) d\delta$$

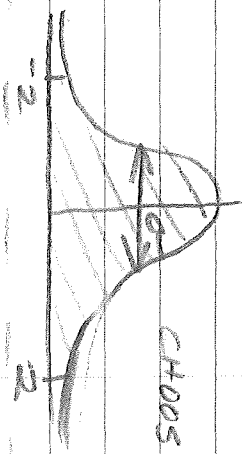
$$P[C/m_1] = \frac{1}{2} + \frac{1}{\sqrt{\pi}} \sigma \int_0^{\frac{b}{2\sigma}} \exp\left(-\frac{b^2}{2\sigma^2} d^2\right) d\delta$$

$$\Rightarrow P[C] = P[C/m_0] + P[C/m_1] = P[M_i]$$

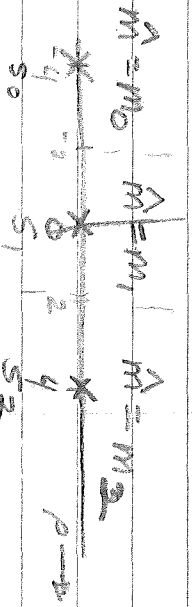
$$P[E] = 0.1 \Rightarrow P[C] = 0.9$$

$$\Rightarrow 0.9 = \frac{1}{2} + \frac{1}{\sqrt{\pi}} \sigma \int_0^{\frac{b}{2\sigma}} \exp\left(-\frac{b^2}{2\sigma^2} d^2\right) d\delta$$

$$\sigma = 0.98 \sqrt{2\pi} \sigma \int_0^{\frac{b}{2\sigma}} \exp\left(-\frac{b^2}{2\sigma^2} d^2\right) d\delta$$



CHOOSE $\sigma \Rightarrow \int_0^{\frac{b}{2\sigma}} \exp\left(-\frac{b^2}{2\sigma^2} d^2\right) d\delta$
OF WHOLE THINGS



FOR OPTIMUM RECEIVER WITH

$$P[M_i] = \frac{1}{2} \forall i$$

$$P[E] = 1 - \frac{1}{2} [P[C/m_0] + P[C/m_1] + P[C/m_2]]$$

INVESTIGATE

$$P_r(p-s_0) = \sqrt{\frac{2\pi}{\sigma^2}} \sigma \exp\left(-\frac{1}{2\sigma^2} (p+q)^2\right) = P_r(p/s=s_0)$$

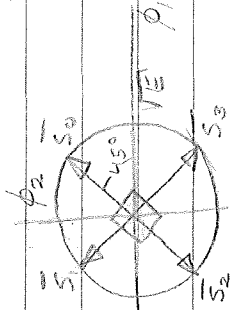
$$P_r(p-s_1) = \sqrt{\frac{2\pi}{\sigma^2}} \sigma \exp\left(-\frac{1}{2\sigma^2} p^2\right) = P_r(p/s=s_1)$$

$$P_r(p-s_2) = \sqrt{\frac{2\pi}{\sigma^2}} \sigma \exp\left(-\frac{1}{2\sigma^2} (p-q)^2\right) = P_r(p/s=s_2)$$

b) $P_0(p-s) = \sqrt{\frac{2\pi}{\sigma^2}} \sigma \exp\left(-\frac{1}{2\sigma^2} (p-s)^2\right)$
 \Rightarrow SHIFTED TO RIGHT TONE UNIT

(NO CHANGE IN $P[E]$)

4-2)



$\phi_1 \neq \phi_2$ ARE ORTHOGONAL $\int_{-\infty}^{\infty} \phi_1 \phi_2 = 0$
 $\int_{-\infty}^{\infty} \phi_1^2 dt = \int_{-\infty}^{\infty} \phi_2^2 dt = \text{ENERGY}$
 IF $E=1$, $\phi_1 \neq \phi_2$ ARE ORTHONORMAL

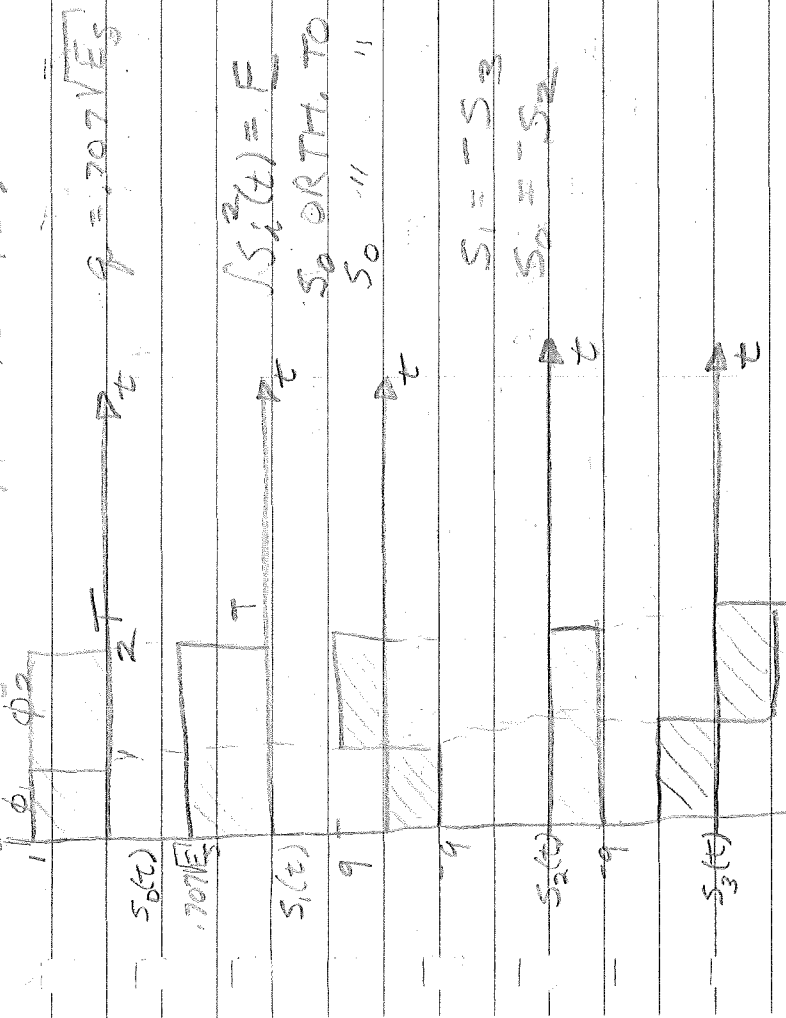
ENERGY = $E S$

$S_0 = \sqrt{E} (\cos \phi_1 + \cos \phi_2)$

$S_1 = \sqrt{E} (-\cos \phi_1 + \cos \phi_2)$

$S_2 = \sqrt{E} (\sin \phi_1 - \sin \phi_2)$

$S_3 = \sqrt{E} (\sin \phi_1 + \sin \phi_2)$



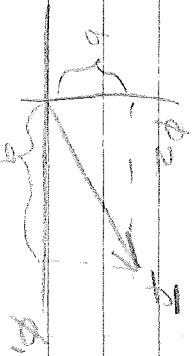
$S_0^2(t) = E$
 S_0 ORTH. TO S_1
 S_0 " " S_2
 S_0 " " S_3

$S_1 = -S_3$
 $S_2 = -S_0$

$$f(t) \Rightarrow \bar{f}$$

$$\bar{f}_1 = \phi_1(t), \bar{f}_2 = \phi_2(t) = \phi_2 \text{ ORTHONORMAL}$$

$$f = a\bar{f}_1 + b\bar{f}_2$$

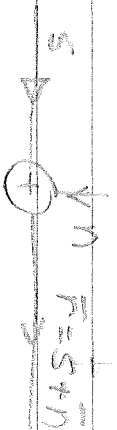
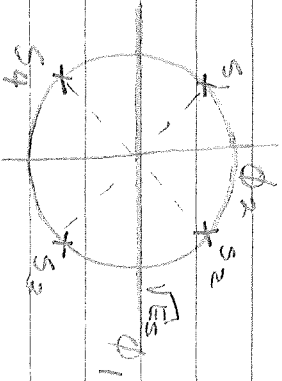


$$a = \bar{f}_1 \cdot f = \int_{-\infty}^{\infty} \phi_1(t) f(t) dt$$

$$b = \bar{f}_2 \cdot f = \int_{-\infty}^{\infty} \phi_2(t) f(t) dt$$

4-71

4-2)



$$\bar{n} = \begin{bmatrix} n_1 \\ n_2 \end{bmatrix}, p_n(n_1, n_2) = \frac{1}{\sqrt{2\pi} \sigma} e^{-\frac{(n_1, n_2)}{2\sigma^2}}$$

$$p_n(n_1, n_2) = \frac{1}{N\sigma^2} e^{-\frac{(n_1^2 + n_2^2)}{2\sigma^2}}$$

$$= \frac{1}{\sqrt{2\pi} \sigma} e^{-\frac{n_1^2}{2\sigma^2}} \frac{1}{\sqrt{2\pi} \sigma} e^{-\frac{n_2^2}{2\sigma^2}}$$

$$= p_n(n_1) p_n(n_2)$$

WE CAN DEFINE 2 ORTHONORMAL TIME FUNCTIONS, $\phi_1(t), \phi_2(t)$, THEN THE SIGNALS MAY BE

WRITTEN:

$$\begin{cases} s_0(t) = \sqrt{E_s} (\sqrt{2} \phi_1(t) + \sqrt{2} \phi_2(t)) \\ s_1(t) = \sqrt{E_s} (\sqrt{2} \phi_1(t) - \sqrt{2} \phi_2(t)) \\ s_2(t) = -s_0(t) \end{cases}$$

$$s_3(t) = -s_1(t)$$

$$s_0 = \begin{bmatrix} \sqrt{E_s} \\ \sqrt{E_s} \\ \sqrt{E_s} \\ \sqrt{E_s} \end{bmatrix}, s_1 = \begin{bmatrix} \sqrt{E_s} \\ \sqrt{E_s} \\ -\sqrt{E_s} \\ -\sqrt{E_s} \end{bmatrix}, s_2 = \begin{bmatrix} -\sqrt{E_s} \\ -\sqrt{E_s} \\ \sqrt{E_s} \\ \sqrt{E_s} \end{bmatrix}, s_3 = \begin{bmatrix} -\sqrt{E_s} \\ \sqrt{E_s} \\ -\sqrt{E_s} \\ \sqrt{E_s} \end{bmatrix}$$

HOW DO WE MAKE $A(t)$ TO A VECTOR

$$\begin{cases} n_1 = \int_{-\infty}^{\infty} n_1(t) \phi_1(t) dt \\ n_2 = \int_{-\infty}^{\infty} n_2(t) \phi_2(t) dt \end{cases} \text{ PROJECTIONS}$$

(ϕ_1, ϕ_2 ORTHONORMAL)

n_1 AND n_2 ARE GAUSSIAN R.V.

$$P[m_i] = P[m_j] \quad i, j = 0, 1, 2, 3$$

MUST MAXIMIZE APOSTERIORI PROBABILITY:

$$P[m_i] p_n(\bar{r} | s = s_i); i.e$$

$\hat{m}(0) = m_i$ WHEN

$$P[m_i] p_n(\bar{r} | s = s_i) > P[m_j] p_n(\bar{r} | s = s_j) \forall j$$

BECAUSE, $P[m_i] = 1/4$, WE HAVE

MAXIMUM LIKELIHOOD SITUATION

AND THE DECISION FUNC. BECOMES:

$$p_n(\bar{r} | s = s_i)$$

$$\text{NOW } P_r(\bar{r} | s = s_k) = p_n(\bar{r} - s_k)$$

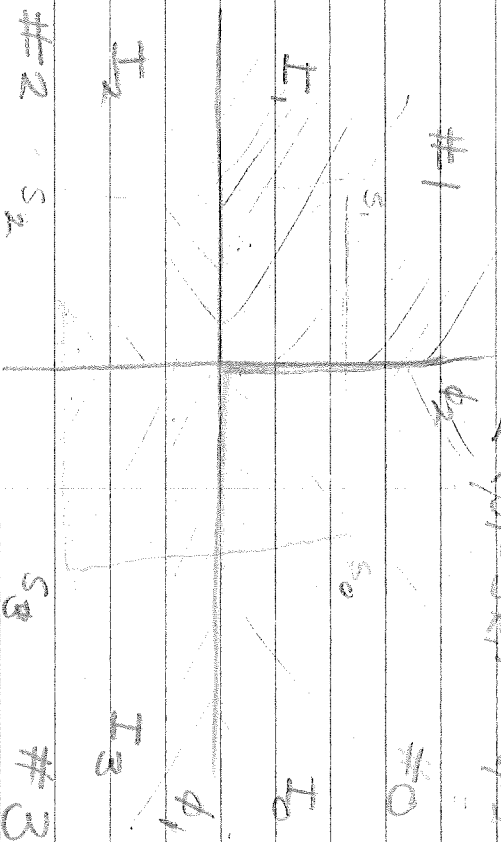
$$= \frac{1}{\pi N_0} e^{-\frac{[(\bar{r} - s_k)^2 + (\bar{r} - s_k)^2]}{N_0}}$$

$$\text{AND } \frac{1}{N_0} e^{-\left[(\rho_1 - s_{k1})^2 + (\rho_2 - s_{k2})^2 \right] / N_0}$$

$$> \frac{1}{N_0} e^{-\left[(\rho_1 - s_{k1})^2 + (\rho_2 - s_{k2})^2 \right] / N_0} \quad \text{Krus}$$

$$|E| = (\rho_1 - s_{k1})^2 + (\rho_2 - s_{k2})^2$$

$$\leftarrow (\rho_1 - s_{k1})^2 + (\rho_2 - s_{k2})^2$$



$$P[C/m_2] = P[I_1 | m_2]$$

$$= \iint p_{\rho}(s) ds$$

FOR

EXAMPLE

$$P[C/m_2] = \int_0^{\infty} \int_0^{\infty} \frac{1}{N_0} e^{-\left[(\rho_1 - s_{k1})^2 + (\rho_2 - s_{k2})^2 \right] / N_0}$$

$$= \int_0^{\infty} \int_0^{\infty} \frac{1}{N_0} e^{-\left[(\rho_1 - \sqrt{s})^2 + (\rho_2 - \sqrt{s})^2 \right] / N_0} \rho_1 \rho_2$$

$$= \left(\frac{1}{N_0} \right)^2 \int_0^{\infty} \int_0^{\infty} e^{-\left[(\rho_1 - \sqrt{s})^2 + (\rho_2 - \sqrt{s})^2 \right] / N_0} d\rho_1 d\rho_2$$

$$= \left[\frac{1}{N_0} \right]^2 \int_0^{\infty} e^{-\left[(\rho_1 - \sqrt{s})^2 + (\rho_2 - \sqrt{s})^2 \right] / N_0} d\rho_2$$

$$= Q_2 \left(-\sqrt{\frac{N_0}{2}} \right)$$

$$\Rightarrow Q_2 \left(-\sqrt{\frac{N_0}{2}} \right) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{-t^2/2} dt$$

$$Q_2 = \left(\frac{1}{\sqrt{2\pi}} \right) \int_{-\infty}^{\infty} e^{-t^2/2} dt$$

VECTOR LENGTHS AND ENERGY

$$\Rightarrow P[c/m_0] = Q^2 \left(\sqrt{\frac{E_s}{N_0}} \right)$$

$$\therefore P[c/m_0] = \dots \Rightarrow \lambda = 0, 1, 2, 3$$

$$\Rightarrow P[c] = Q^2 \left(\sqrt{\frac{E_s}{N_0}} \right)$$

$\frac{E_s}{N_0}$ = SIGNAL TO NOISE RATIO



DEFINE AN ORTHONORMAL SET

$$\phi_1(t) = \frac{1}{\sqrt{4}} x(t)$$

$$\phi_2(t) = \frac{1}{\sqrt{4}} y(t)$$

THEN $\int_{-\infty}^{\infty} \phi_1(t) \phi_2(t) dt = 0$

$$\int_{-\infty}^{\infty} \phi_i^2(t) dt = 1 \quad i = 1, 2$$

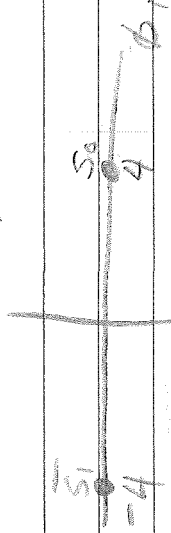
SPECTRAL DENSITY OF NOISE:

$$S(f) = \frac{N_0}{2} = 4 \quad \text{WATT-CYCLES}^{-1} \text{ HERTZ}^{-1}$$

$$\Rightarrow N_0 = 8$$

$$a) \text{ LET } S_0(t) = 4\phi_1(t) \Rightarrow \bar{S}_0 = 4\phi_1$$

$$S_1(t) = -4\phi_1(t) \Rightarrow \bar{S}_1 = -4\phi_1$$



$$P[m_0] = P[m_1] = \frac{1}{2}$$

$$\therefore \hat{m}(p) = m_0 \quad |F| =$$

$$p_n(p-s_0) \rightarrow p_n(p-s_i)$$

IN THE FIRST PROBLEM,

ALL VECTORS ARE ONE DIMENSIONAL.

BY DEFINITION:

$$\hat{n} = n = \int_{-\infty}^{\infty} n_w(t) \phi_1(t) dt \quad (11)$$

$$E[\hat{n}] = \int_{-\infty}^{\infty} E[n_w(t)] \phi_1(t) dt = 0$$

$$n^2 = \int_{-\infty}^{\infty} n_w(t) \phi_1(t) dt \int_{-\infty}^{\infty} n_w(t_2) \phi_1(t_2) dt_2$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} n_w(t) n_w(t_2) \phi_1(t) \phi_1(t_2) dt_1 dt_2$$

$$E[n^2] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} E[n_w(t) n_w(t_2)] \phi_1(t) \phi_1(t_2) dt_1 dt_2$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \delta(t_1 - t_2) \phi_1(t) \phi_1(t_2) dt_1 dt_2$$

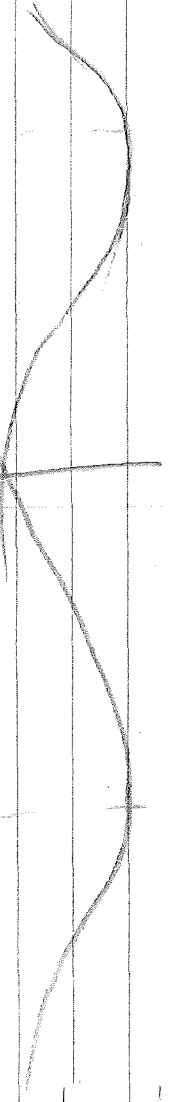
$$= \frac{N_0}{2} \int_{-\infty}^{\infty} \phi_1(t) \phi_1(t) dt = \frac{N_0}{2}$$

$$E[n^2] = 0^2 \quad (\text{FOR } 0 \text{ MEAN}) = N_0/2$$

$$\therefore p_n(\bar{p}-s_0) = \frac{1}{\sqrt{2\pi N_0}} e^{-\frac{(p-s_0)^2}{2N_0}}$$

$$= \frac{1}{\sqrt{2\pi N_0}} e^{-\frac{(p-s)^2}{2N_0}} = \frac{1}{\sqrt{2\pi N_0}} e^{-\frac{(p-s)^2}{2}}$$

$$= \frac{1}{\sqrt{2\pi N_0}} e^{-\frac{(p-s)^2}{2N_0}} = \frac{1}{\sqrt{2\pi N_0}} e^{-\frac{(p-s)^2}{2}}$$



$$s_0 = 4$$

$$I_1$$

$$s_0$$

$$s_0 = 4$$

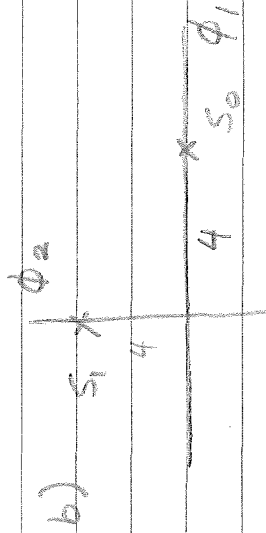
$$P[C/m_0] = \int_0^{\infty} \frac{1}{\sqrt{2\pi}} e^{-\frac{e^{-s_0 t}}{2}} dp$$

$$\text{LET } \phi = \frac{e^{-s_0 t}}{2}, \quad d\phi = -\frac{1}{2} dp$$

$$\Rightarrow P[C/m_0] = \frac{1}{\sqrt{2\pi}} \int_{-\frac{1}{2}}^{\infty} e^{-\frac{1}{2}\phi} d\phi = Q(-2)$$

$$P[C/m_1] = P[C/m_0] = Q(-2)$$

$$\Rightarrow P[C] = Q(-2)$$



$$s_0 = [4, 0], \quad s_1 = [0, 4]$$

$$\bar{n} = [n_1, n_2]$$

$$n_1 = \int_{-\infty}^{\infty} n_w(t) \phi_1(t) dt$$

$$n_2 = \int_{-\infty}^{\infty} n_w(t) \phi_2(t) dt$$

$$E[n_1] = E[n_2] = 0$$

$$E[n_1^2] = E[n_2^2] = N_0/2$$

$$E[n_1 n_2] = \int_0^T E[n_w(t) n_w(t_2)] \phi_1(t) \phi_2(t_2) dt dt_2 \\ = \frac{N_0}{2} \int \phi_1(t) \phi_2(t) dt = 0$$

\therefore NOISE COMPONENTS INDEPENDENT

FOR THE PROJECTIONS ONTO

TWO ORTHOGONAL FUNCS, $\phi_1(t), \phi_2(t)$

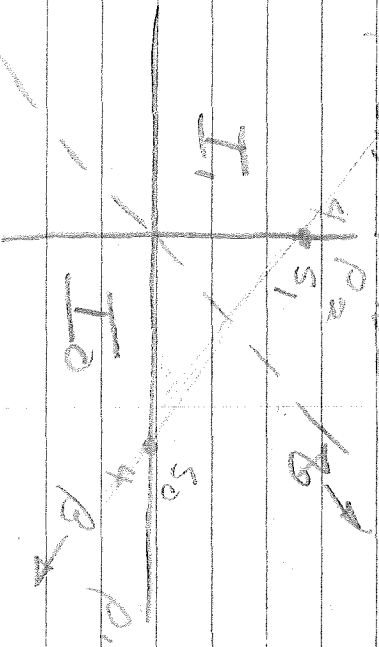
$$\therefore p_n(\alpha) = \frac{1}{2\pi} e^{-(\alpha^2 + \alpha^2)/2 N_0/2}$$

(CONT)

(23)

$$p_n(p-s_0) = \frac{1}{2\pi N_0} e^{-\left[\frac{(p_1-4)^2 + p_2^2}{2N_0/2}\right]}$$

$$p_n(p-s_0) = \frac{1}{\sqrt{N_0}} e^{-\left[\frac{(p_1^2 + (p_2-4)^2)}{N_0}\right]}$$



$$P[C/m_0] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d p_1 \frac{1}{\sqrt{N_0}} e^{-\left[\frac{(p_1-4)^2 + p_2^2}{N_0}\right]}$$

$$\text{LET } \beta = p_1 - 4$$

$$P[C/m_0] = \int_{-\infty}^{\infty} d p_2 \int_{-\infty}^{\infty} d \beta \frac{1}{\sqrt{N_0}} e^{-\left[\frac{\beta^2 + p_2^2}{N_0}\right]}$$

$$\text{LET } \alpha = \frac{\beta}{\sqrt{N_0}} \quad (\beta = p_2)$$

$$\beta = \sqrt{N_0} (\alpha + p_2)$$

THEN

$$P[C/m_0] = \int_{-\infty}^{\infty} d \beta \int_{-\infty}^{\infty} d \alpha \frac{1}{\sqrt{N_0}} e^{-(\alpha^2 + (p_2-1)/N_0)}$$

$$= \frac{1}{\sqrt{N_0}} \int_{-\infty}^{\infty} d \alpha e^{-\alpha^2} = Q(-\sqrt{2})$$

$$P[C/m_0] = Q(-\sqrt{2})$$

$$\Rightarrow P[C] = Q[-\sqrt{2}] < Q[-2]$$

5-13-71

RECEIVER IMPLEMENTATION

M-MESSAGE, $i = 0, \dots, M-1$

N-DIMENSIONS $f = 1, \dots, N$

RECEIVER CALCULATES:

$$\vec{r} = (r_1, \dots, r_N)$$

$$r_f = \int_{-\infty}^{\infty} r(t) \phi_j(c) dt$$

= PROJECTION OF $r(t)$ ONTO $\phi_j(c)$

DECISION FUNCTION

$$|r \cdot \vec{s}_i|^2 = N_0 \ln P[m_i]$$

$$\text{FOR W.G.N, } s_{if} = \frac{N_0}{2} c_f; \sigma^2 = \frac{N_0}{2}$$

$\hat{m} = \text{MK IF DECISION FUNCTION}$

IS MINIMUM FOR $i = k$

$$\text{NOW } |r \cdot \vec{s}_k|^2 = \sum_{f=1}^N (r_f - s_{kf})^2 = |r|^2 - 2r \cdot \vec{s}_k + |s_k|^2$$

$$\Rightarrow \vec{r} \cdot \vec{s}_k = \frac{1}{2} |r \cdot \vec{s}_k|$$

HENCE, BECAUSE OF THE (-) SIGN

BEFORE $\vec{r} \cdot \vec{s}_k$, MUST MAXIMIZE

$\vec{r} \cdot \vec{s}_k$ IN ORDER TO MINIMIZE

$$|r \cdot \vec{s}_k|^2$$

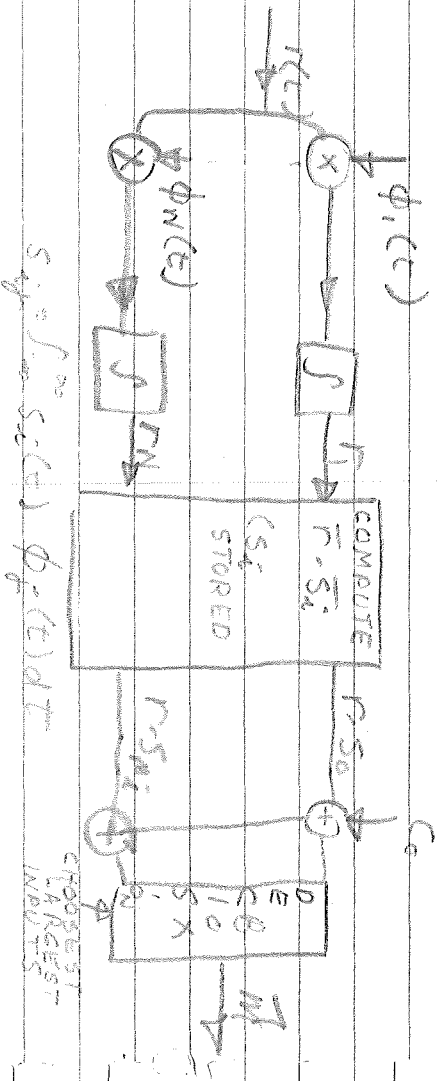
REALLY WE MUST MAXIMIZE

$$r \cdot \vec{s}_k + c_k = \frac{1}{2} (N_0 \ln P[m_i]) - |s_k|^2$$

$$i = 0, \dots, M-1$$

CORRELATION RECEIVER COMPUTES THE (CROSS) CORRELATION FUNCTION $\bar{r} \cdot \bar{s}_i$, EITHER ANALOGICALLY OR DIGITALLY

NOTE $\bar{r} \cdot \bar{s}_i = \int_{-\infty}^{\infty} r(t) s_i(t) dt$
 OR $r_i = \int_{-\infty}^{\infty} r(t) \phi_i(t) dt$



MATCHED FILTERS (Pg 236)



WE WANT TO GENERATE

THE COMPONENTS, $r_i(t) = \int_{-\infty}^{\infty} r(\alpha) h(t-\alpha) d\alpha$

$r_i = \int_{-\infty}^{\infty} r(\alpha) \phi_i(\alpha) d\alpha$

CONSIDER;

$h(t) = \phi_i(T-t); T = N$

$r_i(t) = \int_{-\infty}^{\infty} r(\alpha) \phi_i(T-t-\alpha) d\alpha$

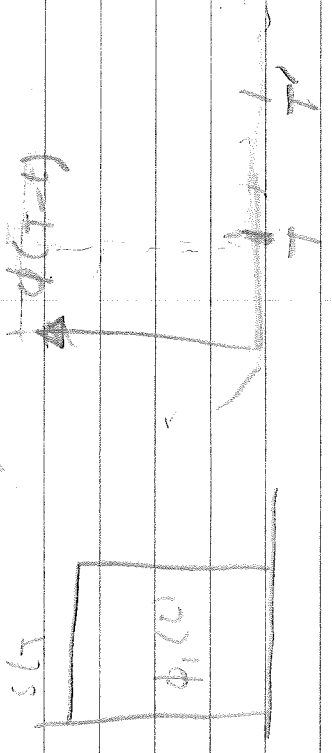
$$= \int_{-\infty}^{\infty} r(\alpha) \phi_i(T + \alpha - t) d\alpha$$

SAMPLE AT $t=0$ AND $N=0$

$$y_i(t) = \int_{-\infty}^{\infty} r(\alpha) \phi_i(\alpha) d\alpha$$

$h(t)$ MUST BE CAUSE

$h(t) = 0$; SUPER IMPULSE



FOR CAUSALITY ON $\phi(T-t)$, WE

~~FORGET THAT~~, WE FORGIVE THAT

EACH BASIS FUNC. VANISH

IDENTICALLY OUTSIDE SOME

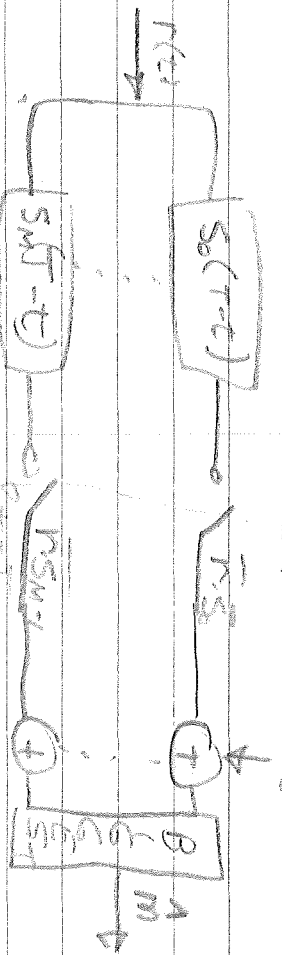
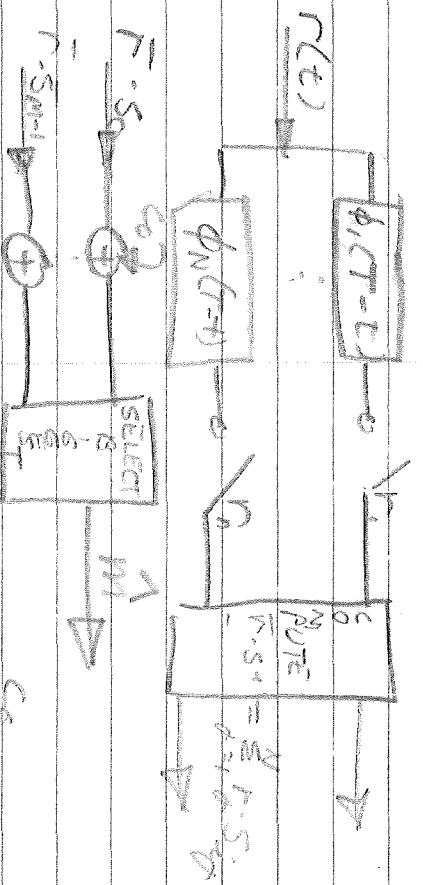
FINITE INTERVALS

CAN MATCH DIRECTLY TO $S_c(T)$

$$U(t) = \int_{-\infty}^{\infty} R(\alpha) S_c(T - (t-\alpha)) d\alpha$$

$$= \int_{-\infty}^{\infty} R(\alpha) S_c(T + \alpha - t) d\alpha$$

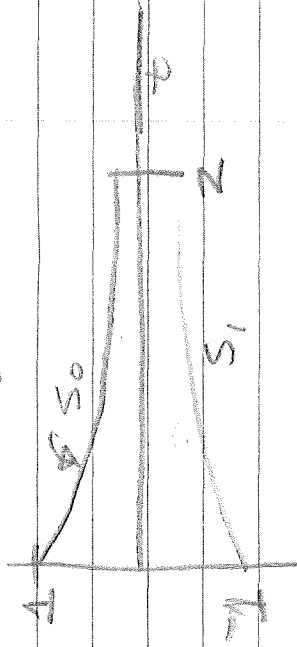
$$\therefore U(T) = \int_{-\infty}^{\infty} R(\alpha) S_c(\alpha) d\alpha$$



MATCHING DIRECTLY TO SIGNAL

4-15)

$$s_0 = e^{-t} \mu(t); \quad s_1(t) = e^{-t} \mu(t)$$



ASSUMING $S_N(f) = N_0/2$

$$P[E] = Q \left[\frac{d}{\sqrt{2N_0}} \right] \Rightarrow d = \frac{\text{DISTANCE BETWEEN SIGNALS}}{\sqrt{E}}$$

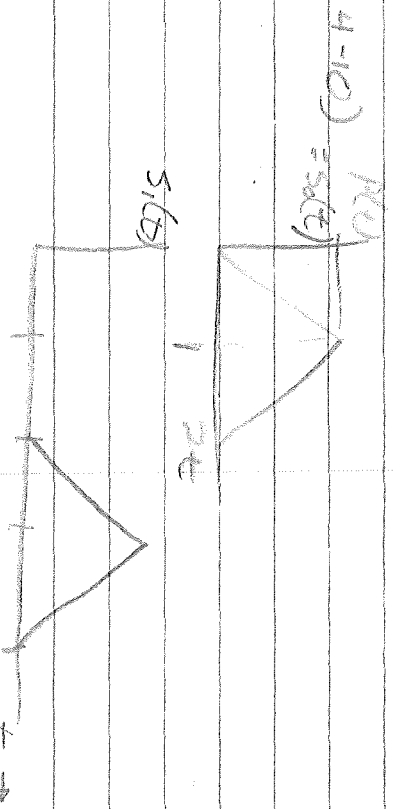
$$\frac{s_0}{s_0}$$

$$E_s = \int_0^{\infty} e^{-2t} dt = \frac{1}{2}$$

$$\Rightarrow d = 2\sqrt{E_s}$$

$$\therefore P[E] = Q \left[\frac{2\sqrt{E_s}}{\sqrt{2N_0}} \right] = Q \left[\sqrt{\frac{2E_s}{N_0}} \right]$$

$$E_s (\text{REALLY}) = \int_0^{\infty} e^{-2t} dt = \frac{1}{2} (1 - e^{-4})$$



a) AN OPTIMUM RECEIVER
 SELECTS m_0 AFTER
 RECEIVING $r(t)$

$$\int_{-\infty}^{\infty} r(t) s_0(t) dt \int_{-\infty}^{\infty} r(t) s_1(t) dt$$

SINCE THE ENERGY OF
 $s_0(t)$ = ENERGY IN $s_1(t)$
 AND BOTH ARE EQUALLY
 PROBABLE

($C_0 = C_1$, HENCE, IGNORE)

b) FOR EQUALLY LIKELY BINARY

MESSAGES'

$$P[E] = Q \left[\frac{d}{\sqrt{2N_0}} \right]$$

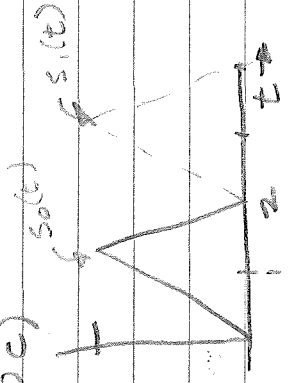
WHERE $d^2 = |s_0 - s_1|^2$

$$= \int_{-\infty}^{\infty} [s_0(t) - s_1(t)]^2 dt = \frac{16}{3}$$

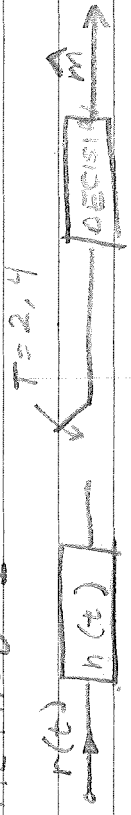
$$\Rightarrow P[E] = Q \left[\frac{4}{\sqrt{0.17}} \right] \approx 10^{-9}$$

4-17-71

4-10c)



C) METHOD 1

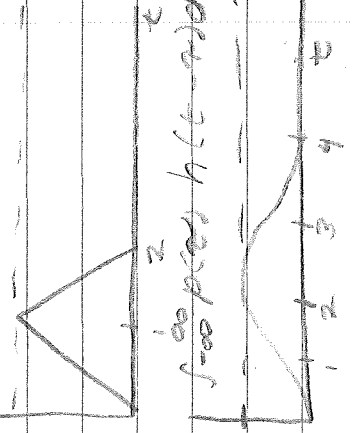


THE SAMPLE AT $T=2$ IS

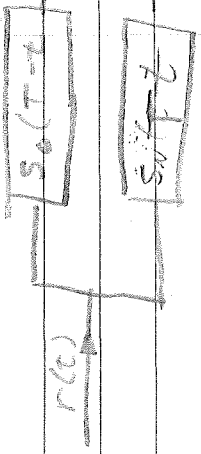
$$\int_{-\infty}^{\infty} r(t) s_0(t) dt$$

THAT AT $T=4$ IS $\int_{-\infty}^{\infty} r(t) s_1(t) dt$

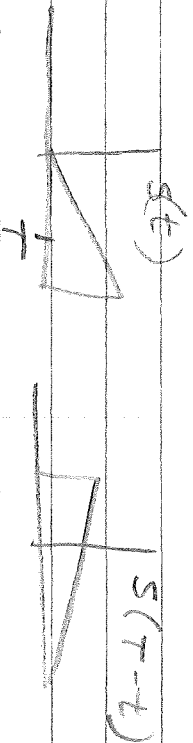
$$h(t) = s_0(2-t)$$



MATSH FILTER



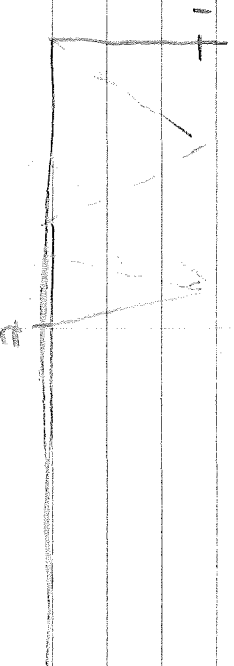
(31)



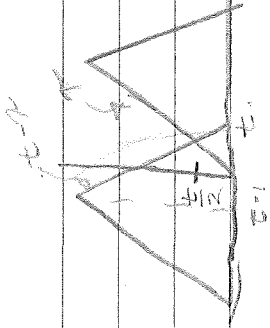
(conv)

$$\begin{aligned}
 & \int_{-\infty}^{\infty} r(\alpha) h(t-\alpha) d\alpha = e(t) \\
 & = \int_{-\infty}^{\infty} r(\alpha) s_0(t-\alpha) d\alpha \\
 & = \int_{-\infty}^{\infty} r(\alpha) s_0(t-\alpha) d\alpha \\
 & v(2) = \int_{-\infty}^{\infty} r(\alpha) s_0(\alpha) d\alpha \\
 & v(4) = \int_{-\infty}^{\infty} r(\alpha) s_0(\alpha-2) d\alpha \\
 & = \int_{-\infty}^{\infty} r(\alpha) s_0(\alpha) d\alpha
 \end{aligned}$$

$$\begin{aligned}
 & \int_{-\infty}^{\infty} p(r) s_0(t-r) dr \\
 \Rightarrow & \int_{-\infty}^{\infty} p(r) h(t-r) dr = \int_{-\infty}^{\infty} p(r) s_0(2-t+r) dr \\
 & = \int_{-\infty}^{\infty} s_0(r) s_0(2-t+r) dr \\
 & = \int_{-\infty}^{\infty} s_0(r) s_0(t-r) dr
 \end{aligned}$$



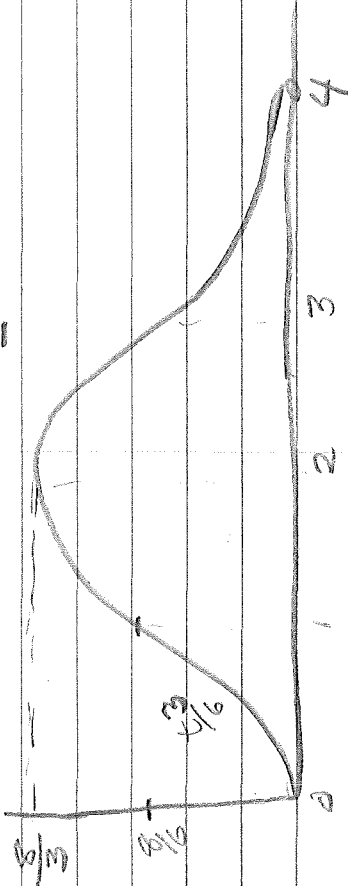
$t < 0 \Rightarrow * = 0$



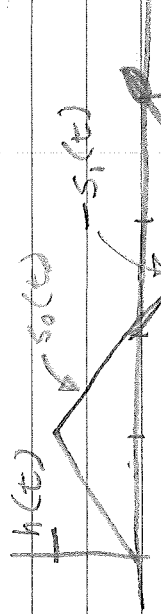
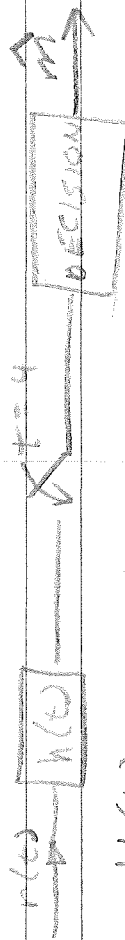
$$\int_0^3 P(t) dt = \frac{t^3}{3} + \frac{t^3}{2} = \frac{t^3}{6} \quad 0 < t < 1$$



$$\int_0^{t-1} P(t-2) + \int_{t-1}^t P(t) dt = \int_0^t P(t-2) dt$$



FOR METHOD II



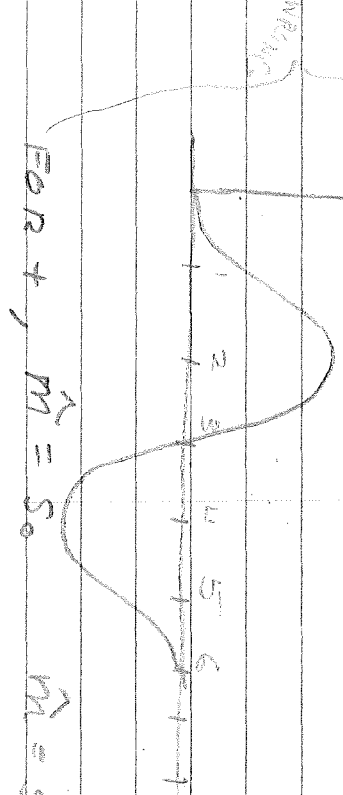
$$h(t) = s_0(t) - s_1(t)$$

(cont)

$$\int_{-\infty}^{\infty} r(t) h(t-\tau) d\tau$$

$$= \int_{-\infty}^{\infty} r(\tau) [s_0(t) - s_1(t)] d\tau$$

$$\int_{-\infty}^{\infty} p(\tau) h(t-\tau) d\tau$$



FOR $t > 4$, $\hat{m} = s_0$ $\hat{m} = s_1$ FOR $t < 3$

$$h(t) = s_0(4-t) - s_0(t-4)$$

$$\int_{-\infty}^{\infty} r(\tau) [s_0(4+\tau-t) - s_0(4-\tau-t)] d\tau$$

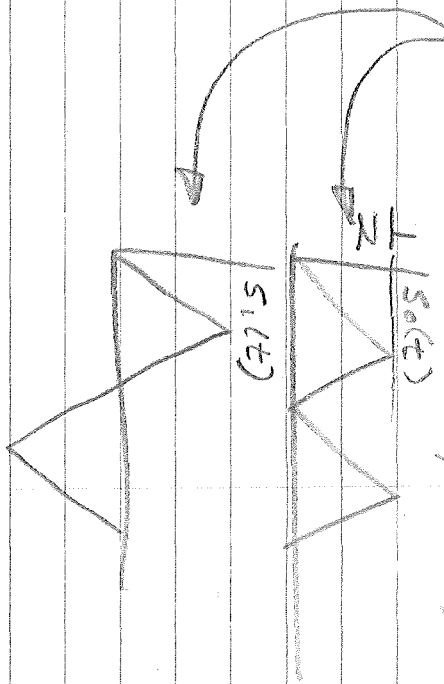
(RIGHT GRAPH)

d) SAME ERROR PROB

$$s_0(t) = \frac{1}{2} [p(t) + p(t-2)]$$

SMALL ERROR (ENTIPITA)

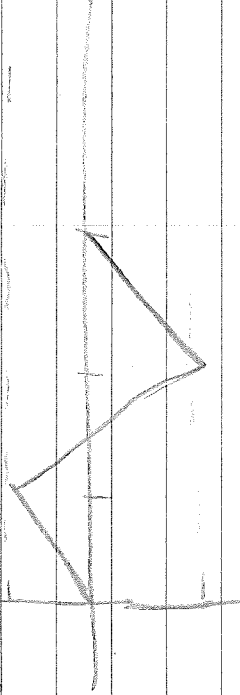
$$s_1(t) = p(t), \quad s_0(t) = p(t)$$



e) FOR $S_0(t) = p(t)$

$S_1(t) = p(t-1)$

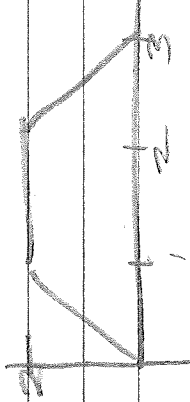
$S_0(t) - S_1(t)$



$$d^2 = \int_{-\infty}^{\infty} [S_0(t) - S_1(t)]^2 dt$$

$$= 2 \int_0^1 (2-x)^2 dx + 2 \int_1^2 (4-x)^2 dx = 4$$

$$P[E] = \sigma \left[\frac{1}{\sqrt{105}} \right]$$



FOR $S_0(t) = p(t)$, $S_1(t) = p(t-1)$

$d^2 = \int_{-\infty}^{\infty} [S_0(t) - S_1(t)]^2 dt = \frac{20}{3}$

$P[E] = \sigma \left[\sqrt{\frac{5}{3(105)}} \right] \approx 4 \times 10^{-9}$

4-21-71

$$\int_{-\infty}^{\infty} f(t) g(t) dt = \int_{-\infty}^{\infty} F(\omega) G(\omega) d\omega$$

$$\begin{aligned} \rho^2 &= \int_{-\infty}^{\infty} [s(t) - s_0(t)]^2 dt \\ &= \int_{-\infty}^{\infty} e^{j\omega t} S(\omega) \cdot 0 \cdot S_0(\omega) + S_0(\omega) + S_0^*(\omega) d\omega \end{aligned}$$

FOR REAL TIME FUNCTIONS:

$$S_0(-\omega) = S_0^*(\omega)$$

CHAPT. 7 : FIRST 2 SECTIONS

COMPLEX CONVOLUTION

$$\mathcal{F}\{g(t)h(t)\} = \int_{-\infty}^{\infty} G(\omega) H^*(\omega - \beta) d\beta$$

$$\mathcal{F}\{f^*(t)\} = \mathcal{F}\{G^*(\omega)\}$$

$$\mathcal{F}\{h(t)\} = \mathcal{F}\{H(\omega)\}$$

$$\mathcal{F}\{g(t)h(t)\} = \int_{-\infty}^{\infty} e^{-j\omega t} g(t)h(t) dt$$

$$\begin{aligned} &= \int_{-\infty}^{\infty} e^{j\omega t} dt \int_{-\infty}^{\infty} G(\omega') e^{-j\omega' t} d\omega' \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} H(\omega - \omega') e^{j\omega t} d\omega' d\omega \end{aligned}$$

$$\begin{aligned} &= \int_{-\infty}^{\infty} G(\omega') H(\omega - \omega') d\omega' \\ &= \int_{-\infty}^{\infty} G(\omega') H(\omega - \omega') d\omega' \end{aligned}$$

$$\int_{-\infty}^{\infty} e^{-j\omega t} dt = \delta(\omega)$$

$$\Rightarrow \mathcal{F}\{g(t)h(t)\} = \int H(\omega) G(\omega) d\omega$$

$$\begin{aligned} &= \int_{-\infty}^{\infty} G(\omega - \omega') H(\omega - \omega') d\omega' \\ &= \int_{-\infty}^{\infty} G(\omega') H(\omega - \omega') d\omega' \end{aligned}$$

FRI 4-25-71

$$7-4) \quad n(t) = R_c(t) \sqrt{2} \cos \omega_0 t + N_s(t) \sqrt{2} \sin \omega_0 t$$

$$n(t) n(t-\tau) = [N_c(t) \sqrt{2} \cos \omega_0 t + N_s(t) \sqrt{2} \sin \omega_0 t] [N_c(t-\tau) \sqrt{2} \cos \omega_0(t-\tau) + N_s(t-\tau) \sqrt{2} \sin \omega_0(t-\tau)]$$

$$= N_c(t) N_c(t-\tau) 2 \cos \omega_0 t \cos \omega_0(t-\tau) -$$

$$+ N_s(t) N_s(t-\tau) 2 \sin \omega_0 t \sin \omega_0(t-\tau) -$$

$$+ N_s(t) N_c(t-\tau) 2 \sin \omega_0 t \cos \omega_0(t-\tau) -$$

$$+ N_c(t) N_s(t-\tau) 2 \cos \omega_0 t \sin \omega_0(t-\tau)$$

$$= R_c(\tau) [\cos \omega_0 \tau + \cos(2\omega_0 \tau - \omega_0 \tau)]$$

$$+ R_s(\tau) [\cos \omega_0 \tau - \cos(2\omega_0 \tau - \omega_0 \tau)]$$

$$+ R_c(\tau) [\sin(2\omega_0 \tau - \omega_0 \tau) + \sin \omega_0 \tau]$$

$$+ R_s(\tau) [\sin(2\omega_0 \tau - \omega_0 \tau) - \sin \omega_0 \tau]$$

WANT 2 MAKE FUNCTION OF τ

$$n(t) n(t-\tau) = \cos \omega_0 \tau [R_c(\tau) + R_s(\tau)]$$

$$+ \cos(2\omega_0 \tau - \omega_0 \tau) [R_c(\tau) - R_s(\tau)]$$

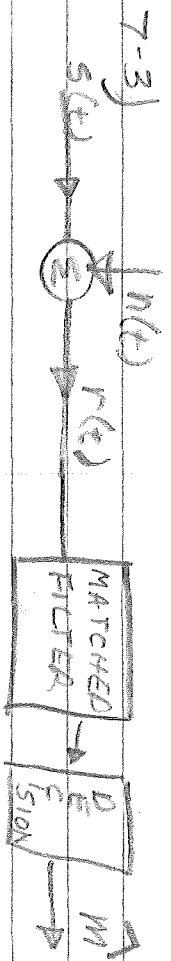
$$+ \sin \omega_0 \tau [R_s(\tau) - R_c(\tau)]$$

$$+ \sin(2\omega_0 \tau - \omega_0 \tau) [R_s(\tau) + R_c(\tau)]$$

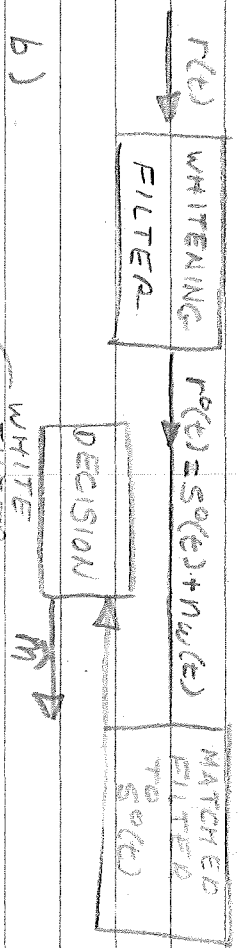
WIDE SENSE STATIONARY SUFFICIENT:

$$R_c(\tau) = R_s(\tau)$$

$$R_s(\tau) = -R_c(\tau)$$

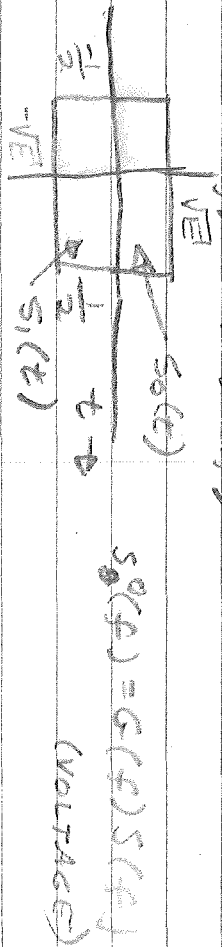


WISH TO PASS $r(t)$ THRU WHITENING FILTER



$s(t) + n(t) = r(t)$ $r'(t) = s'(t) + n_w(t) + s_0(t)$

$S^0(f) = G(f)S(f)$



WANNNA FINDA $G(f)$

$S_w(f) = \frac{N_0}{2}$

$S_n(f) = \frac{N_0}{2} \frac{f^2+1}{f^2+4}$

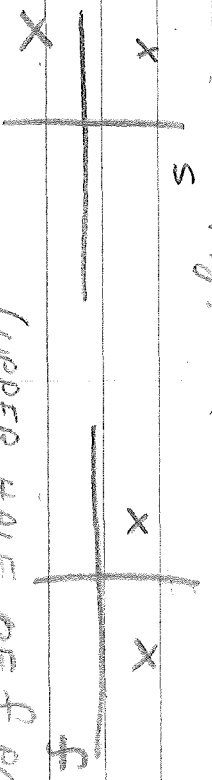
$S_w(f) = |G(f)|^2 S_n(f)$ (POWER)

$\Rightarrow \frac{N_0}{2} = G(f)G^*(f) \frac{N_0}{2} \frac{f^2+1}{f^2+4}$

$\Rightarrow G(f)G^*(f) \frac{f^2+1}{f^2+4} = 1$

$\Rightarrow G(f)G^*(f) = \frac{f^2+4}{f^2+1}$

$\therefore G(f) = \frac{2+f^2}{1+f^2}$ (POLES IN LEFT)



(UPPER HALF OF f PLANE)

$$s = j\pi 2f$$

$$G(s) = \frac{4\pi + j2\pi f}{2\pi + j2\pi f} = \frac{4\pi + s}{2\pi + s}$$

$$s + 2\pi \frac{1 + \frac{3s}{2\pi}}{s + 4\pi} = 1 + \frac{2\pi}{s + 2\pi}$$

$$\frac{s + 2\pi}{2\pi}$$

$\Rightarrow g(t) = \text{IMPULSE RESPONSE FOR } g$

WHITENING FILTER

$$g(t) = \mathcal{L}^{-1}[G(s)] = \delta(t) + 2\pi e^{-2\pi t}$$

OUTPUT SIGNAL FROM WHITENING

FILTER (SIGNAL TO BE MATCHED)

$$s^0(t) = \int_{-\infty}^{\infty} s(\alpha) g(t-\alpha) d\alpha$$

$$= \pm \sqrt{E_s} \int_{-\frac{1}{2}}^{\frac{1}{2}} [\delta(t-\alpha) + e^{-2\pi\alpha}] \mu_{-1}(t-\alpha) d\alpha$$

FOR $t < -\frac{1}{2}$, $s^0(t) = 0$

FOR $-\frac{1}{2} < t < \frac{1}{2}$

$$s^0(t) = \pm \sqrt{E_s} (1 + e^{-t}) \int_{-\frac{1}{2}}^t e^{2\alpha} d\alpha$$

$$= \pm \sqrt{E_s} [2 - e^{-(t+\frac{1}{2})}]$$

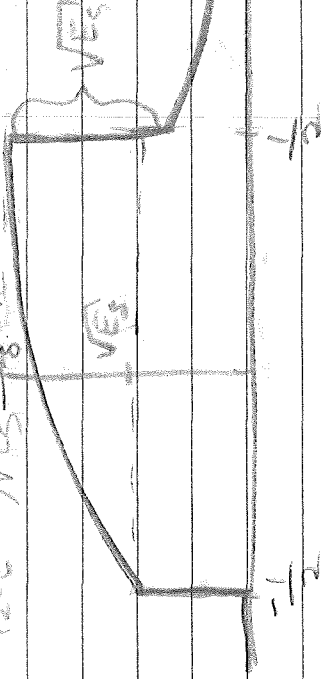
FOR $t > \frac{1}{2}$

$$s^0(t) = \pm \sqrt{E_s} [e^{-t} - \frac{1}{2} e^{-s}] d\alpha]$$

$$= \pm \sqrt{E_s} (e^{-t/2} - e^{-t/2}) e^{2t}$$

$$= \pm \sqrt{E_s} 2 \sinh(\frac{t}{2}) e^{-t}$$

$$(2 \cdot e^{-t/2}) \sqrt{E_s} \frac{e^{t/2}}{2}$$



THUS, WE CANNOT BUILD A
 MATCHED FILTER SAMPLING
 AT TIME T , CAUSE OF THE
 INFINITE TAIL,
 CHOP OFF TAIL IN ABOUT
 5 TIME CONSTANTS (5 τ_{sec})
 WITHOUT TO MUCH LOSS OF
 OPTIMALITY

MONDAY

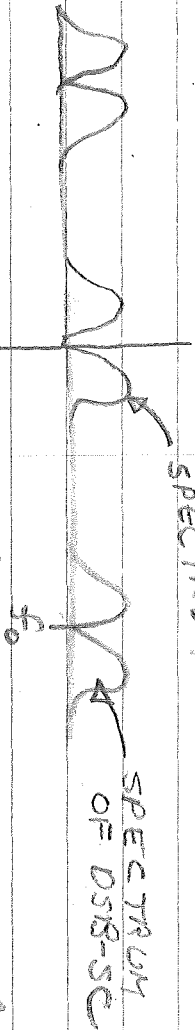
7-5) $s_1(t)$, $s_2(t)$ - TWO LOW-PASS

(BASE-BAND) SIGNALS

$$s_1(t) = \sqrt{2} \cos 2\pi f_0 t$$

$$s_2(t) = \sqrt{2} \sin 2\pi f_0 t$$

SPECTRUM OF s_1 OR s_2

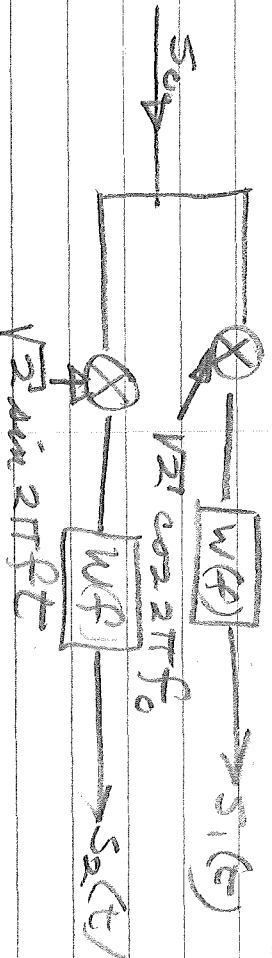


$$s_0(t) = s_1(t) \sqrt{2} \cos 2\pi f_0 t + s_2(t) \sqrt{2} \sin 2\pi f_0 t$$

(QUADRATURE MULTIPLEXING)

IGNORE CHANNEL EFFECTS

HOW DO WE RECOVER $s_1(t) + s_2(t)$



PROOF

SPECTRUM OF $S_0(t)$:

$$S_0(f) = \sqrt{2\pi} [S_1(f-f_0) + S_2(f+f_0)]$$
$$= \int_{-\infty}^{\infty} S_2(f-f_0) + \int_{-\infty}^{\infty} S_2(f+f_0)$$

$$\int_{-\infty}^{\infty} S_1(t) \cos(2\pi f_0 t) dt$$
$$= \int_{-\infty}^{\infty} S_1(t) (e^{-j2\pi f_0 t} + e^{-j2\pi f_0 t})$$
$$= \frac{1}{2} \int_{-\infty}^{\infty} S_1(t) \delta(f+f_0-\phi) d\phi$$
$$+ \frac{1}{2} \int_{-\infty}^{\infty} S_1(t) \delta(f+f_0-\phi) d\phi$$

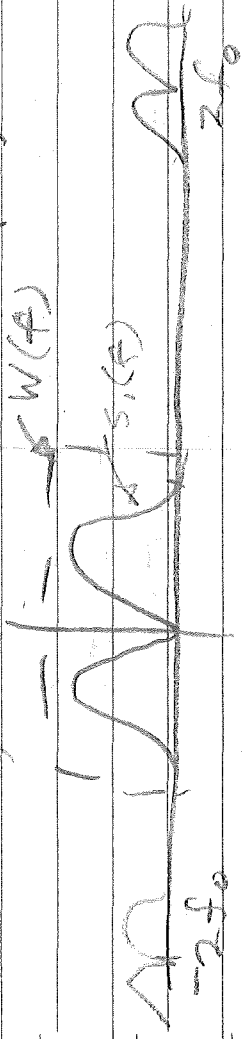
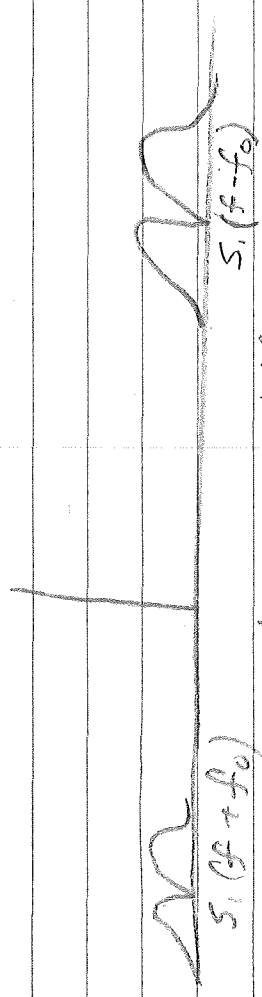
(COMPLEX CONVOLUTION)

$$\int_{-\infty}^{\infty} (e^{j2\pi f_0 t}) \int_{-\infty}^{\infty} S_1(t) e^{-j2\pi(f-f_0)t} dt = S(f-f_0)$$
$$\Rightarrow \int_{-\infty}^{\infty} \{S_1(t) \cos(2\pi f_0 t)\}$$

$$= \frac{1}{2} (S_1(f-f_0) + S_1(f+f_0))$$

SHIFT TO RIGHT R-SHIFT

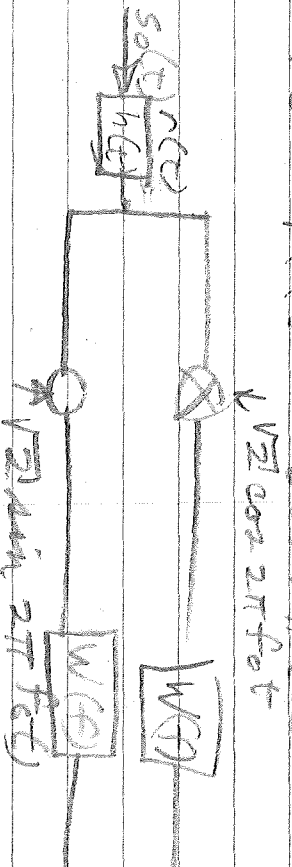
$$\therefore S_0(f) = \sqrt{2\pi} [S_1(f-f_0) + S_1(f+f_0)]$$
$$= \int_{-\infty}^{\infty} S_2(f-f_0) + \int_{-\infty}^{\infty} S_2(f+f_0)$$



$$-j S_0(f-f_0) + j S_0(f) \\ = -j S_0(f) + j S_0(f+f_0)$$

NOTHING AT f ORIGIN WHEN
MULTIPLIED BY $\cos 2\pi f_0 t$

NOW, IF CHANNEL'S IMPULSE
IS $R(f) = S_0(f) H(f)$



THE INPUT TO THE LOW-PASS FILTERS

COS CHANNEL

$\sqrt{2} \cos 2\pi f_0 t \rightarrow$ SPECT $\sqrt{2} [R(f-f_0) + R(f+f_0)]$

$$= \sqrt{2} S_0(f-f_0) H(f+f_0) + S_0(f+f_0) H(f-f_0)$$

$$= \frac{1}{2} [H(f-f_0) [S_1(f-f_0) + S_1(f)] \\ - j S_0(f-f_0) + j S_0(f)] \\ + H(f-f_0) [S_1(f) + S_1(f+f_0)] \\ - j S_0(f) + j S_0(f+f_0)]$$

SIN CHANNEL

$$\frac{1}{\sqrt{2}} [R(f-f_0) - R(f+f_0)]$$

$$= \frac{1}{\sqrt{2}} [S_0(f-f_0) H(f-f_0)]$$

$$= \frac{1}{\sqrt{2}} [S_0(f+f_0) H(f+f_0)]$$

$$= \frac{1}{\sqrt{2}} \{ H(f-f_0) [S_1(f-2f_0)]$$

$$+ S_1(f) - S_2(f-2f_0) + S_2(f) \}$$

$$- H(f+f_0) [S_1(f) + S_1(f+2f_0)]$$

$$- S_1(f) + S_2(f+2f_0) \}$$

OUTPUT ONLY CONTAINS $S_A(f)$

\Rightarrow OUTPUT OF COS CHANNEL

$$\frac{1}{\sqrt{2}} \{ S_1(f) \} [H(f-f_0) + H(f+f_0)]$$

$$+ \frac{1}{\sqrt{2}} [S_2(f) H(f-f_0) + H(f+f_0)]$$

$$0 \leq f \leq W$$

\Rightarrow OUTPUT OF SIN CHANNEL

$$\frac{1}{\sqrt{2}} [S_1(f)] [H(f-f_0) - H(f+f_0)]$$

$$+ \frac{1}{\sqrt{2}} [S_2(f) H(f-f_0) - H(f+f_0)]$$

$$0 \leq f \leq W$$

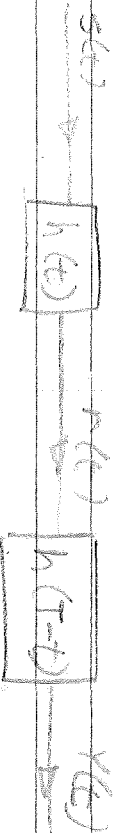
FOR $0 \leq f \leq W$

$$H(f-f_0) = H^*(f+f_0)$$

$$H(\omega) = H^*(-\omega)$$

$$\Rightarrow H^*(f_0-f) = H(f+f_0)$$

FRI.

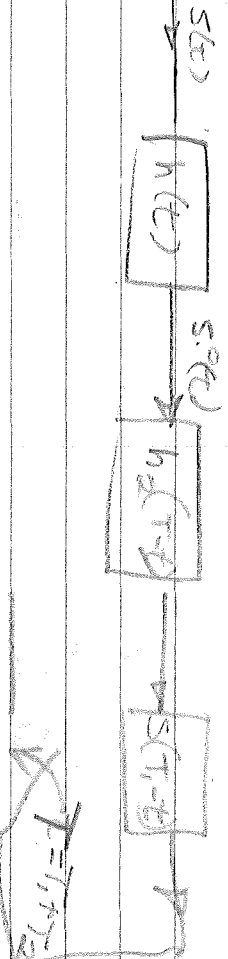


$$y(t) = \int_{-\infty}^{\infty} h(t + \tau - T) x(\tau) d\tau$$

$$R(f) = S(f) H(f)$$

$$Y(f) = R(f) H^*(f) e^{-j2\pi fT}$$

$$= S(f) |H(f)|^2 e^{-j2\pi fT}$$



SEQUENCE OF INPUT PARAMETERS

COMMUNICATING THE FOLLOWING

RANDOM VECTOR $\vec{m} = (m_1, m_2, \dots, m_M)$

EACH m_i IS CONTINUOUS RV.

PRIOR TO THIS, ALL MESSAGES

WERE DISCRETE OR FINITE INT

LINEAR MODULATION,

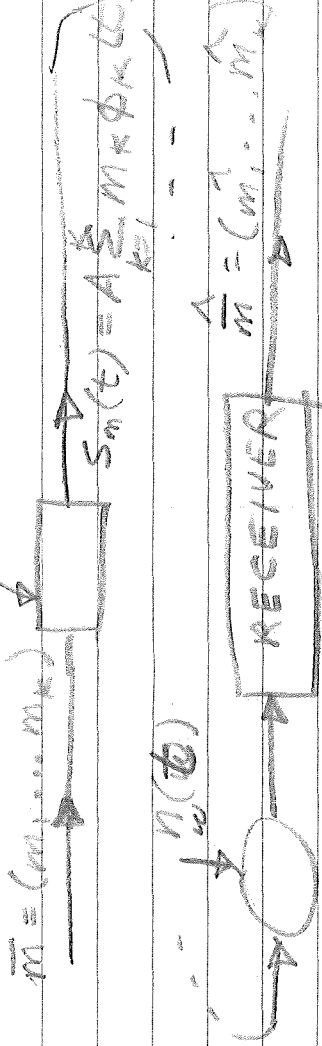
ORTHONORMAL

$$S_m(t) = \sum_{k=1}^M m_k \phi_k(t)$$

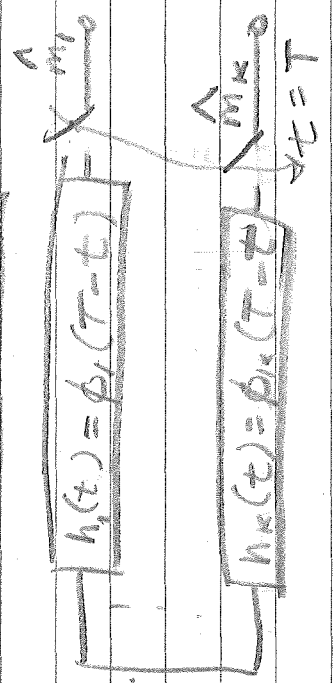
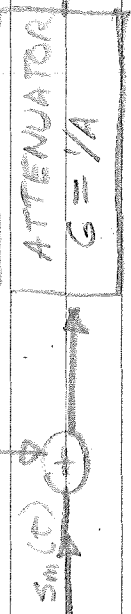
TRANSMITTER GAIN

OBJECT: ESTIMATE $\hat{\vec{m}} = (\hat{m}_1, \dots, \hat{m}_M)$

TRANSMITTER



$m_{k0}(t)$



INPUT INTO MATCHED FILTER

$$\frac{r(t)}{A} = \sum m_k \phi_k(t) + n(t) \frac{1}{A}$$

OUTPUT OF FILTER ①

$$= \sum_k m_k \int_{-\infty}^{\infty} \phi_k(t) \phi_k(t) dt + \int_{-\infty}^{\infty} n(t) \phi_1(t) dt$$

$$= \sum_k m_k \int_{-\infty}^{\infty} \phi_k(t) \phi_k(t) dt + \int_{-\infty}^{\infty} n(t) \phi_1(t) dt$$

$$= m_1 + \int_{-\infty}^{\infty} n(t) \phi_1(t) dt = \hat{m}_1$$

$$= m_1 + \int_{-\infty}^{\infty} n(t) \phi_1(t) dt = \hat{m}_1$$

= RECEIVED 1ST COMPONENT

ERROR = $\hat{m}_1 - m_1 = \frac{1}{N} \sum_{k=1}^N$
 MEAN SQUARE ERROR

PER COMPONENT
 $= E [| \hat{m}_1 - m_1 |^2] = E [\frac{1}{N^2} \sum_{k=1}^N m_k^2]$
 $= \frac{1}{N^2} N \sigma^2 \Rightarrow \sigma^2 / N$ IS

SPECTRAL DENSITY OF
 THE WHITE GAUSSIAN NOISE

$$E [\sum_{k=1}^N W_k E [| \hat{m}_k - m_k |^2]]$$

$$= \frac{1}{N} E [(m_1 - m_1)^2 + \dots + (m_k - m_k)^2]$$

$$= \frac{1}{N} E [| \hat{m}_1 - m_1 |^2]$$

$$= \frac{1}{N} \frac{K N \sigma^2}{2 A^2} = \frac{\sigma^2}{2 A^2}$$

(AGREES WITH ABOVE)

$$p_m(\alpha) p_r(p/m=\alpha)$$

$$= P_{YM}(p, \alpha) = P_m(\alpha | r=p) p_r(p)$$

IN ORDER THAT THE A POSTERIORI
 PROB. DENSITY $p_m(\alpha | r=p)$

BE MAXIMIZED, WE MUST

$$\frac{p_m(\alpha) p_r(p/m=\alpha)}{p_r(p)}$$

RESPECT TO α

$\Rightarrow p_m(\alpha) p_n(\rho/m)$ IS MAX

LIKELIHOOD FUNCTION
UPON MAXIMIZING OUR
LIKELIHOOD FUNCTION, WE
HAVE MAXIMUM LIKELIHOOD
RECEPTION

$$r = n + m$$

$\Rightarrow p_r(\rho/m = \alpha) = p_n(\rho - \alpha | m = \alpha)$
NOISE & MESSAGE IN-
 $\Rightarrow = p_n(\rho - \alpha)$, WHICH CAN
BE MAXIMIZED,

IN K DIMENSIONS
BECAUSE $n_w(t)$ IS WHITE
GAUSSIAN NOISE, THE
LIKELIHOOD FUNCTION
IN K DIMENSIONS IS

$$p_r(\rho/m = \bar{a}) = p_n(\rho - \bar{a} | A)$$

$$= (\pi N_0)^{-K/2} e^{-|\rho - \bar{a} |^2 / N_0}$$

$$= \prod_{k=1}^K \frac{1}{\sqrt{\pi N_0}} e^{-(\rho_k - \alpha_k A)^2 / N_0}$$

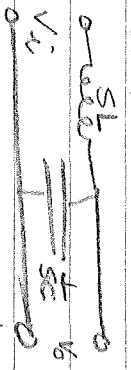
(NOTE $\rho_k = A m_k + n_k$)

THE VECTOR \vec{r} THAT MAXIMIZES THIS FUNCTION (FOR A GIVEN VALUE ρ OF THE RANDOM VECTOR \vec{r}) IS $\vec{r} = \rho \vec{A} = \vec{m} + \vec{v} \vec{A} = \frac{\vec{A}}{m}$

THIS IS A LINEAR RECEIVER BECAUSE THE ESTIMATE \hat{m} OF m IS A LINEAR FUNCTION OF THE LINEAR RECEIVED VECTOR \vec{r} . RECALL $\vec{m} = \vec{m} + \vec{v} \vec{A}$ WAS IMPLEMENTED BEFORE

MONDAY

7-2 (ex)



$$V_0 = \frac{S_L}{S_L + S_C} = \frac{V_c}{S^2 + \omega_0^2}$$

- SAMPLING THEOREM: OR HOW TO
 REDUCE CONTINUOUS (ANALOG)
 DATA TO DISCRETE (DIGITAL)

IF $x(t)$ IS A FINITE ENERGY
 WAVEFORM WHOSE FOURIER
 TRANSFORM IS IDEENTICALLY

0 FOR $|f| \geq W_m$, THEN

$$Z(\omega) = \sum_{k=-\infty}^{\infty} Z_k \psi_k(\omega)$$

WHERE $Z_k = \int_{-\infty}^{\infty} x(t) \psi_k(t) dt$

AND $\psi_k(t) = \psi(t - \frac{k}{2W_m})$

$$\psi(t) = \sqrt{2W_m} \text{sinc}(2W_m t)$$

OBSERVATIONS:

1) IMPULSE RESPONSE OF L.P.F. FILTER



t

2) $\{\psi_k(t)\}$ ARE ORTHONORMAL

$$\int_{-\infty}^{\infty} \psi_k(t) \psi_l(t) dt = \int_{-\infty}^{\infty} \psi_k(t) \psi_l(t) dt = \delta_{kl}$$

$$= 0 \quad l \neq k$$

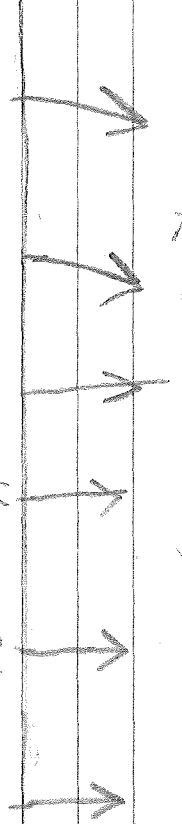
$$= 1 \quad l = k$$

$$= \delta_{kl}$$

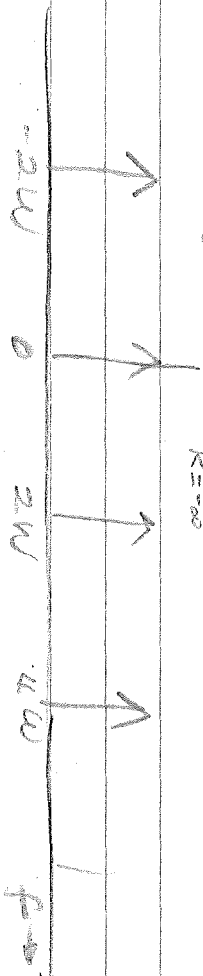
$$z(t) = \sum_{k=-\infty}^{\infty} k a \int_{-\infty}^{\infty} y_k(t) \psi_k(t) dt$$

IMPULSE MODULATOR

$$v(t) = \sum_k \delta(t - \frac{kT}{2}) = \int_{-\infty}^{\infty} U(f) e^{j2\pi f t} df$$



$$\mathcal{F}\{v(t)\} = \sum_{k=-\infty}^{\infty} \delta(f - \frac{k}{2T})$$



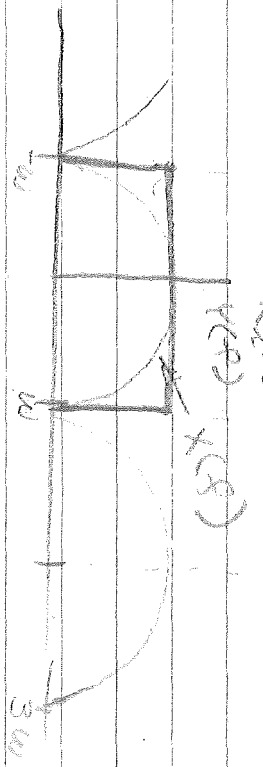
OUTPUT OF IMPULSE MODULATOR

$$v(t) = x(t)v(t) = \sum_{k=-\infty}^{\infty} x(\frac{kT}{2}) \delta(t - \frac{kT}{2})$$

THEN

$$V(f) = \int_{-\infty}^{\infty} x(\frac{kT}{2}) v(f - \frac{k}{2T}) dk$$

$$= 2W \sum_{k=-\infty}^{\infty} x(f - \frac{k}{2T})$$

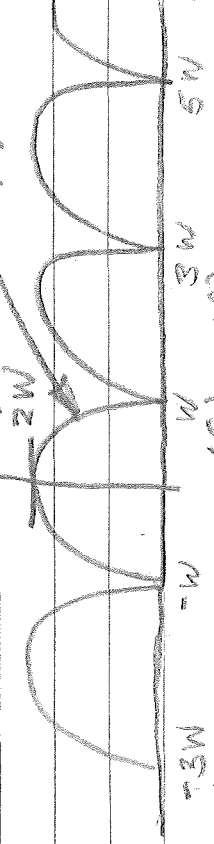


MON / TWO WEEKS FROM TODAY

IMPULSE TRAIN

$$y(t) = x(t) u(t) = \sum_{k=-\infty}^{\infty} x\left(\frac{k}{2W}\right) \delta\left(t - \frac{k}{2W}\right)$$

$y(f)$



$u(f) \delta(f)$



CAN REGAIN THRU FILTER

$$\Rightarrow x(f) = y(f) v(f)$$

$y(f)$



$$\text{OR } x(t) = y(t) * v(t)$$

$$= \int_{-\infty}^{\infty} y(\tau) v(t - \tau) d\tau$$

$$= \int_{-\infty}^{\infty} \sum_{k=-\infty}^{\infty} x\left(\frac{k}{2W}\right) \delta\left(t - \frac{k}{2W}\right) v(t - \tau) d\tau$$

$$= \sum_{k=-\infty}^{\infty} x\left(\frac{k}{2W}\right) v\left(t - \frac{k}{2W}\right)$$

INTERPOLATION FUNCTION

$$= \sum_{k=-\infty}^{\infty} x\left(\frac{k}{2W}\right) \frac{\text{SINC} \left(\frac{k}{2W} \left(t - \frac{k}{2W} \right) \right)}{2W v\left(t - \frac{k}{2W}\right)}$$

FIG 8-13b

RANDOM WAVE FORM: $m(t)$ BANDLIMITED

$$\Rightarrow m(t) = \sum_{k=1}^K m_k \psi_k(t)$$

$$\Rightarrow m_k = \int_{-\infty}^{\infty} m(t) \psi_k(t) = \frac{1}{\sqrt{2W_m}} \int_{-\infty}^{\infty} m(t) \left(\frac{K}{2W_m}\right)$$

COMMUNICATE, AND THEN ESTIMATE THIS DATA

RECEIVER ESTIMATES \hat{m}_k , AND

THEN CONSTRUCTS ESTIMATED

WAVEFORM: $\hat{m}(t) = \sum_{k=1}^K \hat{m}_k \psi_k(t)$

(NOTE $\hat{m}(t)$ IS BANDLIMITED)

MAXIMUM LIKHOOD

ANOTHER
OPTIONAL
FUNCTION

TRANSMITTER

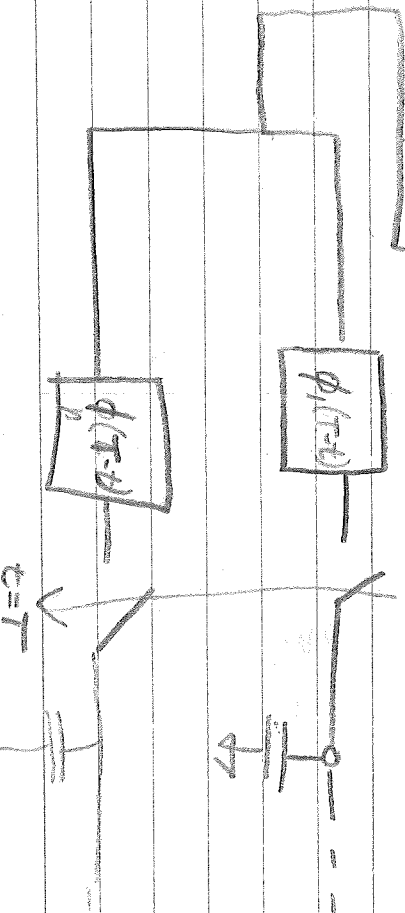
$$s_m(t) = A \sum_{k=1}^K m_k \phi_k(t)$$

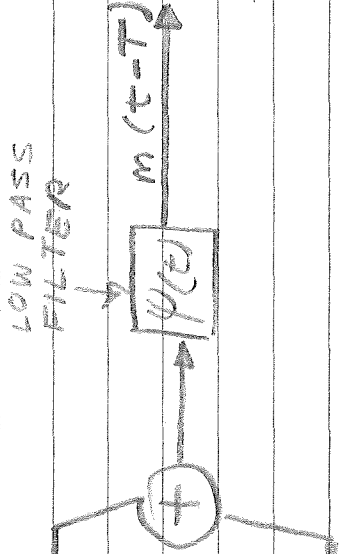
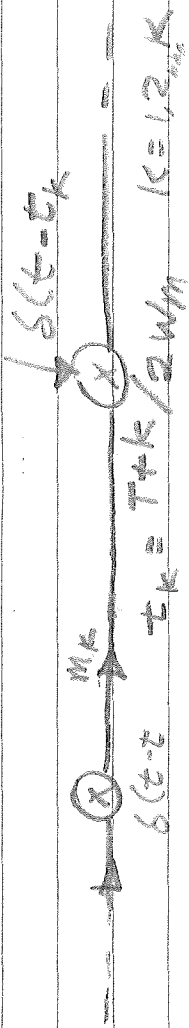
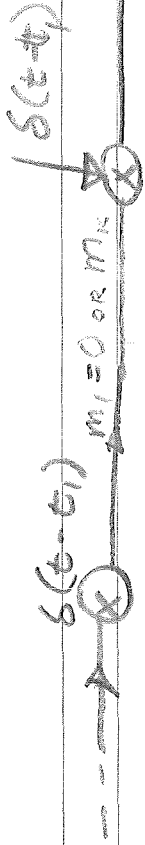
$$m(t) = \sum_{k=1}^K m_k \psi_k(t)$$

(BANDLIMITED)

AMPLIFIER

$\int m_k(t)$





MAY ALSO REPLACE ϕ BY ψ , AND REPLACE BY LP FILTER



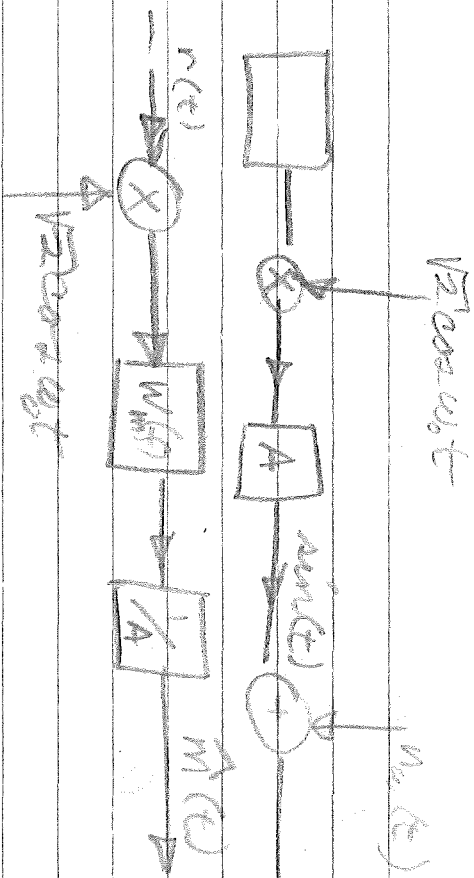
$$-\frac{\pi}{2} \leq \omega \leq \frac{\pi}{2} \quad \sum_{k=-\infty}^{\infty} \frac{1}{2W_m} \delta\left(t - \frac{k}{2W_m}\right)$$

$$y(t) = \int_{-\infty}^{\infty} m(\tau) \cdot \sqrt{2W_m} \psi(t-\tau) d\tau$$

$$\Rightarrow y\left(\frac{t}{2W_m}\right) = \sqrt{2W_m} \sum_{k=-\infty}^{\infty} \psi\left(\frac{t}{2W_m} - \frac{k}{2W_m}\right) \psi\left(\frac{t}{2W_m} - \tau\right) d\tau$$

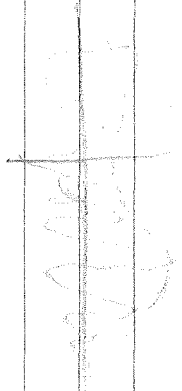
$$\psi(t) = \psi(-t)$$

$$\Rightarrow y\left(\frac{t}{2W_m}\right) = \sqrt{2W_m} m_c$$



MAXIMUM LIKELIHOOD: DSB-SC.

DSB WITH CARRIER



NEAN 3-2 QUIZ

AM-1-19 0-21-627

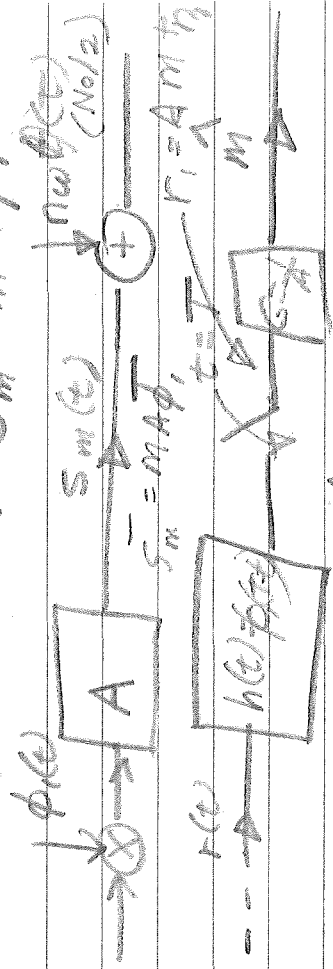
AND SCHEDULE 639-142

1.6.8.8. 639-142

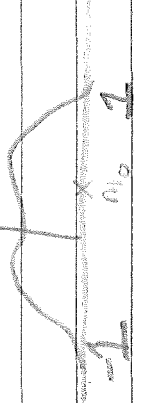
MDM

TWISTED MODULATION:
(NON LINEAR)

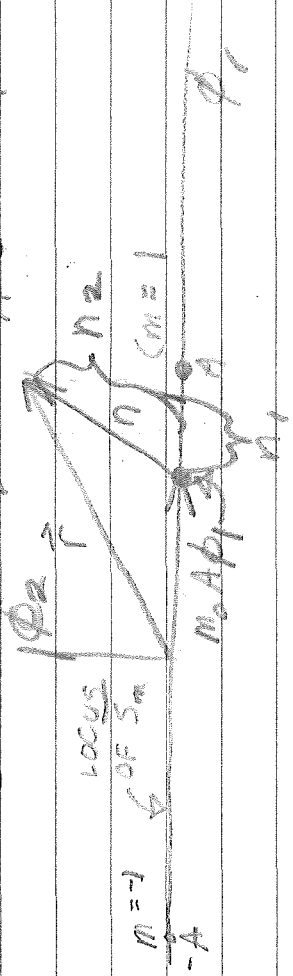
LINEAR MODULATION: $S_m = mA\phi$



$P_m(\omega) \hat{m} = m + n/A$

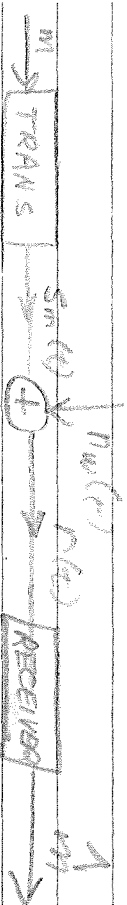


$$E^2 = (\hat{m} - m)^2 = \left(\frac{A^2}{A^2} \right) = \frac{N_0/2}{A^2}$$



$A = \left| \frac{dS_m}{dm} \right|$ (THE STRETCH OF THE SIGNAL LOCUS)

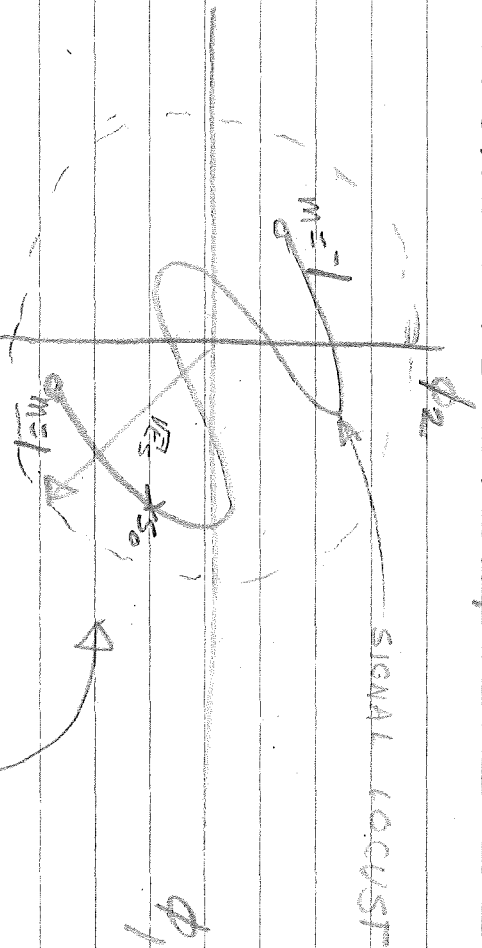
DEFINE STRETCH: $E^2 = \frac{N_0/2}{S^2}$
 $S \triangleq \left| \frac{dS_m}{dm} \right|$ FOR LINEAR MOD. $A = S$



$$s_m(t) = a_1(m) \phi_1(t) + a_2(m) \phi_2(t)$$

$$s_{rx} = \int_{-\infty}^{\infty} d_1(t) \phi_1(t) dt + \int_{-\infty}^{\infty} d_2(t) \phi_2(t) dt$$

$\Rightarrow s_m(t) = a_1(m) \phi_1 + a_2(m) \phi_2$
 FOR LINEAR MOD, $a_1(m)$ and $a_2(m)$ WOULD BE LINEAR FUNCTIONS OF m , FOR NON-LINEAR (TWISTED) COMM $a_1(m) \neq a_2(m)$ ARE NON LINEAR FUNCTIONS OF m



$$\text{IF } \int_{-\infty}^{\infty} s_m(t) dt \leq E_s$$

ASSUME: $\left| \frac{d s_m}{d m} \right| = \frac{1}{2}$, A CONSTANT,

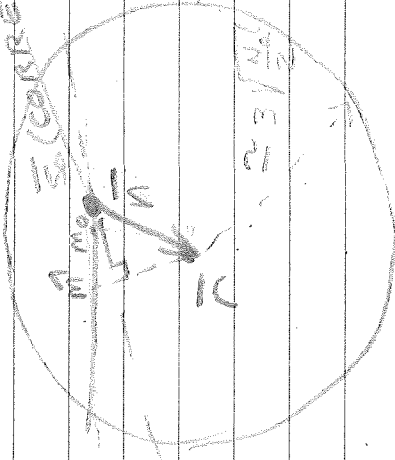
INDEPENDENT OF m ,
 $L = \text{TOTAL LENGTH OF } m \text{ LOCUST,}$

$$S = \frac{L}{2}$$

WEAK NOISE SUPPRESSION

$$\frac{E^2}{S^2} = \frac{N_0 L^2}{S^2}$$

RESPONDS TO INPUT NOISE

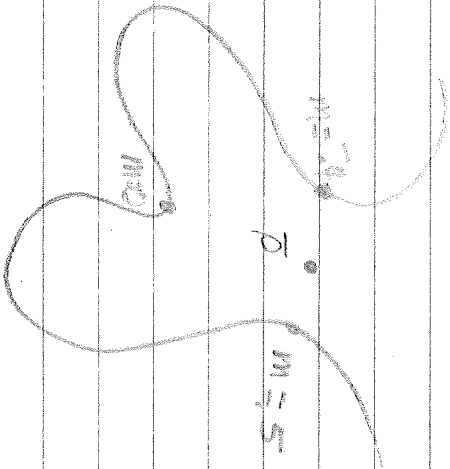
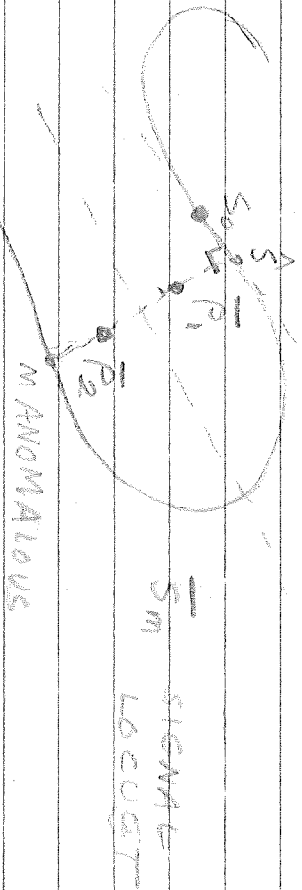


$$S_m \approx S_0 + (m - m_0) S_0$$

$$S_0 = \frac{dS_m}{dm} \Big|_{m=m_0} \quad \text{OR} \quad S_m = m_0$$

CONDITIONAL $\frac{E^2}{S^2} \Big|_{m=m_0} = \frac{N_0 L^2}{S_0^2}$

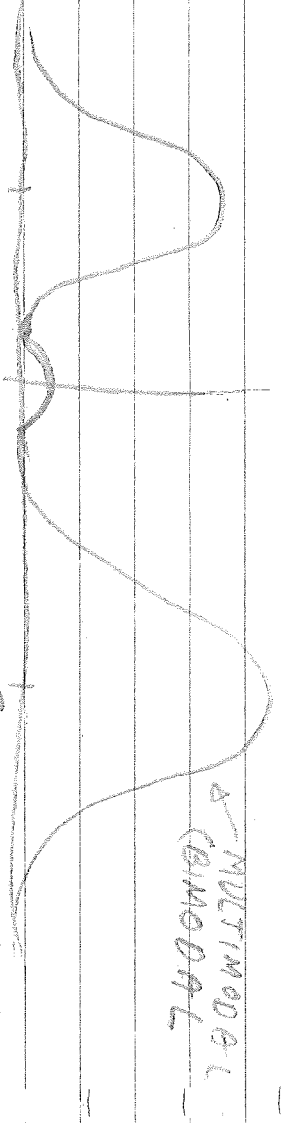
UNCONDITIONAL $\frac{E^2}{S^2} = \frac{N_0 L^2}{S^2} = \frac{L^2}{4}$



$P_m(\alpha | \bar{r} = \bar{p})$ APOSTERIORIA

MULTIMODAL (BIMODAL)

$$E[m | \bar{r} = \bar{p}] = \int_{-\infty}^{\infty} \alpha p_m(\alpha | \bar{r} = \bar{p}) d\alpha$$



- MAXIMUM LIKHOOD RECEIVER DESIGN

FOR ADDITIVE W.G.N.

$$p_{m,r}(\alpha, r) = p_r(r|m = m_0) p_m(\alpha)$$

$$= p(r|\alpha) p_m(\alpha | r = r)$$

$$\Rightarrow p_m(\alpha | r = r) = \frac{p_r(r|m = \alpha) p_m(\alpha)}{p_r(r)}$$

$$p_r(r|m = \alpha) \propto e^{-\frac{1}{2} \rho - S/\sigma^2} / N_0$$

$$\text{MAXIMIZE } \rho \cdot S_\alpha - \frac{1}{2} E_\alpha$$

WISH NO MAXIMIZE

$$(\bar{\rho} - S_\alpha)(\bar{\rho} - S_\alpha) = \bar{\rho}^2 - \underbrace{(\bar{\rho} S_\alpha)}_{\substack{\text{not } f(\alpha) \\ E_\alpha}} + 2\bar{\rho} \cdot S_\alpha$$

$$\rho \cdot S_\alpha - \frac{1}{2} E_\alpha = \int_{-\infty}^{\infty} \rho(t) S_\alpha(t) dt = \frac{1}{2} E_\alpha$$

CORRELATION DETECTION

LINEAR MODULATION:

$$s_\alpha(t) = \alpha A \phi(t)$$

$$\begin{aligned} \text{THUS } \int_{-\infty}^{\infty} \rho(t) S_\alpha(t) dt &= \frac{1}{2} E_\alpha \\ &= \alpha A \int_{-\infty}^{\infty} \rho(t) \phi(t) dt = \frac{1}{2} E_\alpha \\ &= \alpha A \rho - \frac{1}{2} \alpha^2 A^2 \end{aligned}$$

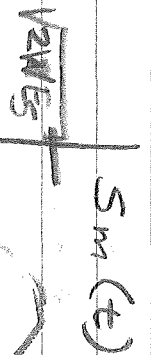
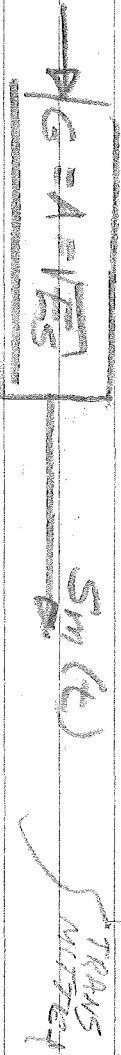
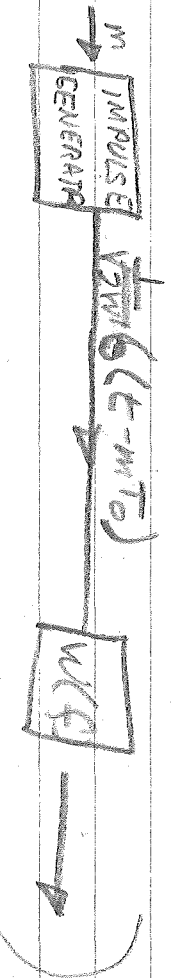
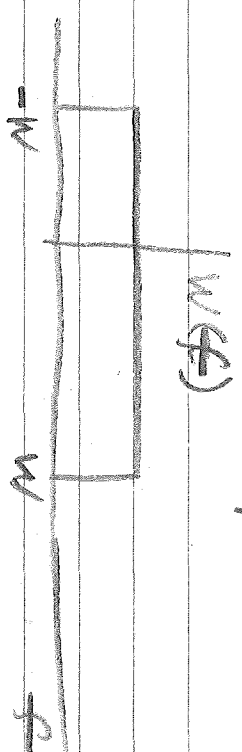
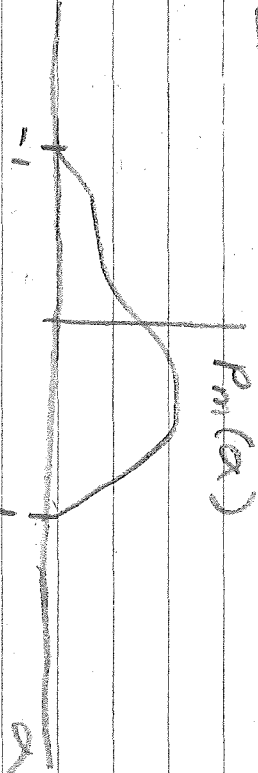
DIFFERENTIATE TO FIND MAX

$$\Rightarrow \alpha = \rho / A = \alpha + \frac{1}{A}$$

MDN

PULSE POSITION MODULATION

$$\left[\frac{c}{2} = \frac{N_0/2}{S_{\Sigma}} = \left(\frac{N_0/2}{\frac{N_0/2}{\sqrt{E_s}}} \right) \text{ FOR LINEAR MODULATION} \right]$$



$$S_m(t) = \sqrt{E_s} \cos(2\pi f_c(t - t_0) + \phi(t))$$

$$\phi(t) = \sqrt{2W} \cos(2\pi Wt) - W < t < W$$

- TRANSMITTED ENERGY $|s_m|^2 = E_s$
MAXIMUM LIKELIHOOD

RECEIVER:

$P_r(p_r | p_m = \alpha)$ IS TO BE MAXED

$$\alpha \int_{-\infty}^{\infty} p_r(t) s_m(\phi) dt$$

$$P_r(p_r | p_m = \alpha)$$

$$\alpha \sqrt{E_s} \int_{-\infty}^{\infty} p_r(t) \phi(t - \alpha T_0) dt$$

THIS IS THE OUTPUT OF A

FILTER MATCHED TO $\phi(-t)$

ie $h(t) = \phi(-t)$ WHEN INPUT

IS $p(t)$

$$p(t) \xrightarrow{h(t)} h(t)$$

$$\text{OUTPUT} = \int_{-\infty}^{\infty} p(\tau) h(t - \tau) d\tau$$

$$= \int_{-\infty}^{\infty} p(\tau) \phi(\tau - t) d\tau$$

$$= \int_{-\infty}^{\infty} p(\tau) \phi(\tau - \alpha T_0) d\tau$$

SINCE $\phi(t) = \phi(-t)$ (FOR A LP

FILTER), A MAXIMUM LIKELIHOOD

RECEIVER PASSES $p(t)$ THRU

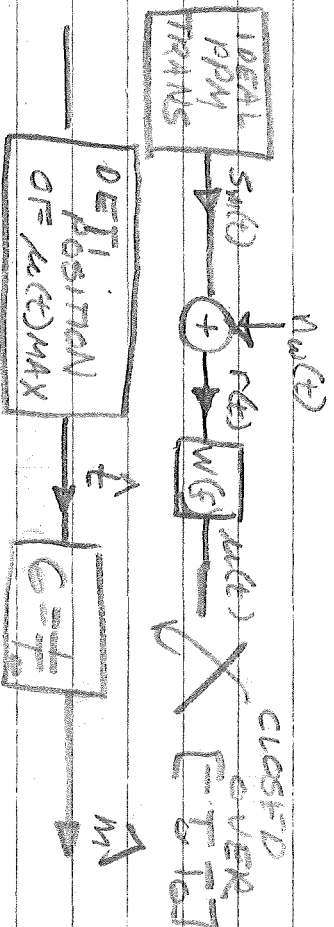
A LP FILTER $w(f)$, THEN

DETERMINES THE TIME

INSTANT, T , $-T_0 \leq t \leq T_0$

AT WHICH THE OUTPUT T

IS MAX, AND SETS $\hat{m} = T/T_0$



$$s_m(t) = \int_{-\infty}^{\infty} \left[\frac{B}{s_m} s_m(t) \right]^2 dt$$

$$s_m(t) = \sqrt{E_s} \phi(t - mT_0)$$

$$\frac{s_m(t)}{s_m} = -\sqrt{E_s} T_0 \phi'(t - mT_0)$$

$$\Rightarrow s^2 = -\sqrt{E_s} T_0 \int_{-\infty}^{\infty} [\phi'(t - mT_0)]^2 dt$$

$$\phi(t) = \sqrt{2W} \frac{\sin 2\pi W t}{2\pi W t}$$

USING PARSEVAL'S THEM:

$$s^2 = E_s T_0^2 \int_{-\infty}^{\infty} \frac{1}{2W} \phi^2 df$$

$$s^2 = \frac{E_s}{3} (2\pi T_0 W)^2$$

NOTE: s^2 INDEPENDENT OF m

$$\Rightarrow \frac{E_s}{3} = \frac{N_0 f^2}{s^2} = \frac{1^2}{4T_0^2} \left(\frac{1}{4T_0 W} \right)^2 \frac{N_0}{2E_s}$$

$$\text{FOR PAM} = \frac{N_0}{2E_s}$$

m

FOR LIN MOD.

$$(M_1 + M_2) \phi(t) = m_1 \phi(t) + m_2 \phi(t)$$
$$\sum z = N_0 / 2E_s$$

CONSIDER $4T_0W$; SIGNAL BW = W

SIGNAL INTERVAL $T_s = 2T_0$

~~mod~~

$\Rightarrow 4T_0W =$ TWICE BW, X SIGNAL INTERVAL
SAME # FROM OF SAMPLES TO

COMMUN. $-T_0 < s(t) < T_0$ AND $-W < f < W$
CALLED EFFECTIVE DIMENSIONALITY

$$\therefore \sum z = \frac{1}{\pi^2} \frac{1}{B_s} \left(\frac{N_0}{2E_s} \right)$$

WAVEFORM COMM. WITH P.P.M.

LOW PASS WAVEFORM

$$m(t) = \sum_{k=-\infty}^{\infty} m_k \phi_k(t) \cdot |f| \leq W_m$$

ASSUME $|m_k| \leq 1 \forall k$

WITH P.P.M., EACH MESSAGE,
 m_k IS TRANSMITTED AND
LIKELIHOOD RECEIVED
IN SUCCESSION, AND

PRODUCES \hat{m}_k , THE

RECEIVER CONSTRAINTS

$$\hat{m}(t) = \sum_{k=-\infty}^{\infty} m_k \psi_k(t)$$

$$\hat{m}_k = m_k + n_k$$

$$\Rightarrow \hat{m}(t) = m(t) + n(t)$$

$$n(t) = \sum_{k=-\infty}^{\infty} n_k \psi_k(t)$$

= STATIONARY GAUSSIAN

PROCESS WITH SPECTRAL

DENSITY

$$S_n(f) = \begin{cases} \frac{1}{2} N_0 W_m & |f| \leq W_m \\ 0 & \text{ELSEWHERE} \end{cases}$$

Avg. OUTPUT NOISE PWR

$$= N^2(t) = 2 W_m S_n(f)$$

$$= 2 W_m \frac{N_0 W_m}{2}$$

$$\text{OR } N^2(t) = \frac{1}{2} N_0 \frac{N_0 W_m}{2}$$

FOR LINEAR MOD:

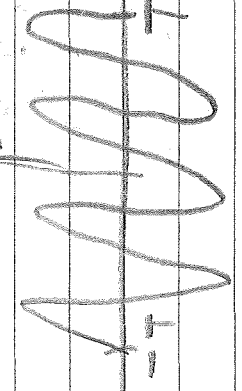
$$N^2(t) = N_0 W_m / E_s$$

- TIME AVAILABLE FOR TRANSMISSION OF EACH MK IS THE SAMPLING INTERVAL $2W_m$. THUS, MAX ALLOWABLE POSITION DEVIATION FOR EACH TRANSMISSION IS $2T_0 \leq \frac{1}{2W_m}$. IF WE SET $2T_0 = \frac{1}{2W_m}$, THEN WE GET $4T_0 W = 1 = W/W_m = \text{B.W. EXPANSION RATIO}$

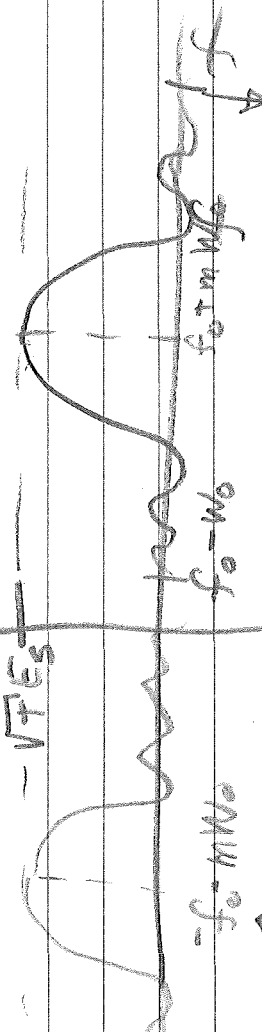
FREQUENCY POSITION MODULATION

$s_m(t) = \sqrt{E_s} \phi_m(t)$
 $\phi_m(t) = \frac{1}{\sqrt{T}} \cos 2\pi(f_0 + W_m t) \cdot T \text{ etc}$
 $= 0$ OTHERWISE

$f_0 > W_0$
 $-1 \leq m \leq 1$



$s_m(f)$



$f = f_0 + m W_0$
 $m = \frac{f - f_0}{W_0}$
 $k = \frac{f - f_0}{W_0} \quad f_0 + W_m$
 $\beta = 4\pi W_0 T$
 $S^2 = \frac{E_s}{3} (2\pi T W_0)^2$

$$n \frac{2(t)}{2} = \frac{1^2}{\pi^2} \left(\frac{v_m}{w_0} \right)^2 \frac{N_0 w_m}{E_s}$$

MON

FEM

$$S_m(t) = A\sqrt{2} \cos 2\pi \left[f_0 t + w_m \int m(t) dt \right]$$

INSTANTANEOUS
PHASE

$$f_{INST} = \frac{df}{dt} \left[f_0 t + w_m \int m(t) dt \right]$$

$$= f_0 + w_m m(t)$$

SPECTRUM: LET $m(t) = \cos 2\pi w_m t$

$$w_0 = 2\pi f_0 \quad w_m = 2\pi w_m$$

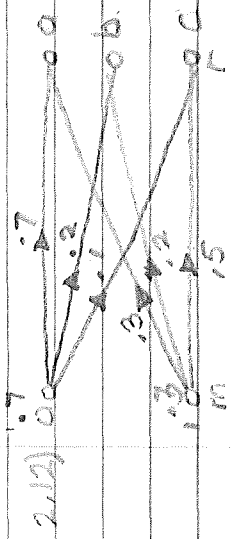
$$S_m(t) = A\sqrt{2} \cos \left(w_0 t + \frac{w_m}{w_m} \sin w_m t \right)$$

$$B = w_1 / w_m$$

$$S_m(t) = A\sqrt{2} \left[\cos(B \sin w_m t) \cos w_0 t \right. \\ \left. - \sin(B \sin w_m t) \sin w_0 t \right]$$

$$J_k(B) = \frac{1}{\pi} \int_{-\pi}^{\pi} e^{i k t}$$

30/30



$a) P[0,0] = .49 \quad P[1,0] = .09$
 $P[0,b] = .14 \quad P[1,b] = .06$
 $P[0,c] = .07 \quad P[1,c] = .15$
 $\hat{m}(a) = 0 \quad (.49)$
 $\hat{m}(b) = 8 \quad (.14)$
 $\hat{m}(c) = 1 \quad (.15)$

$P[C] = .78 \Rightarrow P[E] = .22$

$b) P[0,0,0] = C = P(0) \quad P(E_0) = 1 - P[0]$
 $3) P[0,0,1] = C = (.7)P[0] + (.2)P[0] + (.5)P[1]$
 $= (.9)P[0] + (.5)[1 - P[0]]$
 $= .4P[0] + .5$

$P[E] = 1 - P[C] = .5 - .4P[0]$

$3) P[0,1,0] \Rightarrow P[C] = (.8)P[0] + (.2)[1 - P[0]] = .2 + .6P[0]$

$P(E) = 1 - P[C] = .8 - .6P[0]$

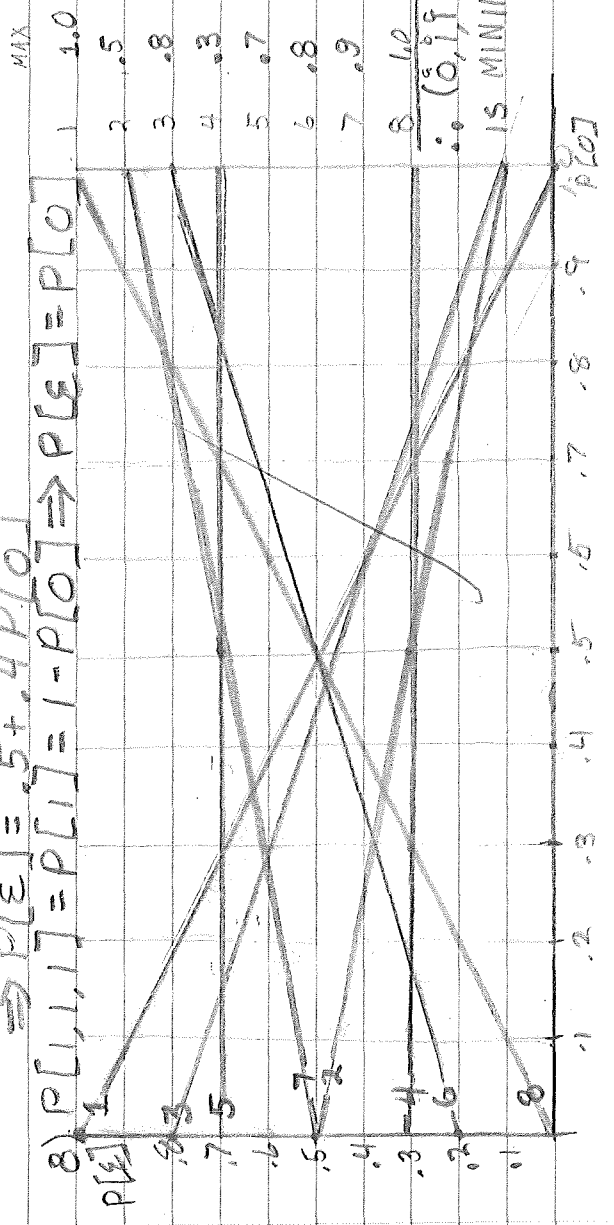
$4) P[0,1,1] = (.7)P[0] + (.7)[1 - P[0]] = .7 \Rightarrow P[E] = .3$

$5) P[1,0,0] = (.3)[1 - P[0]] + .3P[0] = .3 \Rightarrow P[E] = .7$

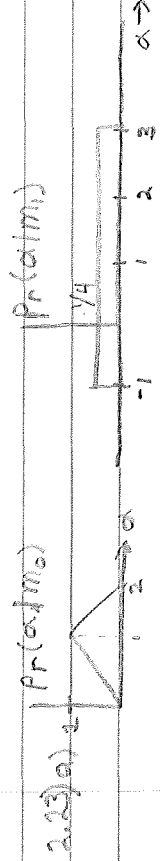
$6) P[1,0,1] = (.8)[1 - P[0]] + .2P[0] = .8 - .6P[0]$
 $\Rightarrow P[E] = .2 + .6P[0]$

$7) P[1,1,0] = (.5)(1 - P[0]) + .1P[0] = .5 - .4P[0]$
 $\Rightarrow P[E] = .5 + .4P[0]$

$8) P[1,1,1] = P[1] = 1 - P[0] \Rightarrow P[E] = P[0]$



$\therefore (0.19, 0.19)$
IS MINIMAX

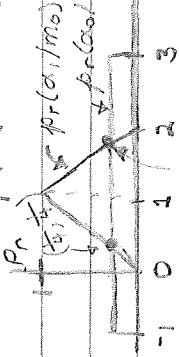


$P[m_0] = P[m_1]$

WHEN $\hat{m}(\alpha) = m_0$

IFF $p_r(\alpha/m_0)P[m_0] > p_r(\alpha/m_1)P[m_1]$

OR $p_r(\alpha/m_0) > p_r(\alpha/m_1)$

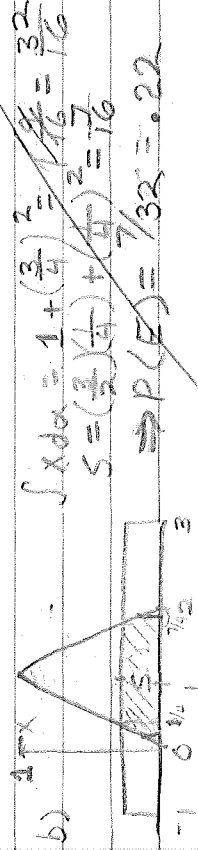


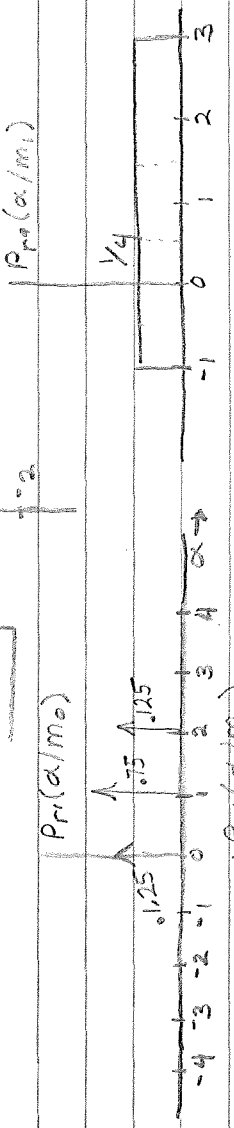
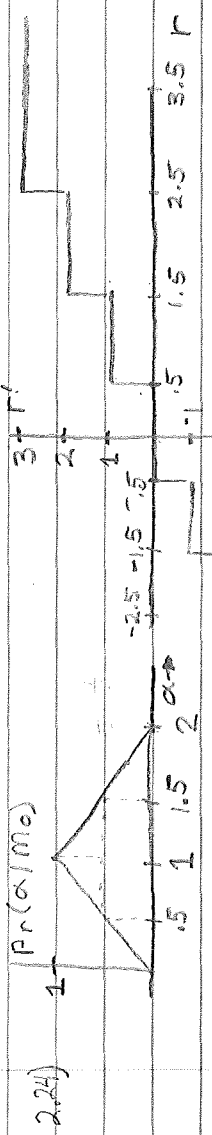
$p_r(\alpha/m_0) > p_r(\alpha/m_1)$ FOR $\frac{1}{4} < \alpha < \frac{3}{4}$
 $p_r(\alpha/m_1) > p_r(\alpha/m_0)$ FOR $-\frac{1}{4} < \alpha < \frac{1}{4}$, $\frac{3}{4} < \alpha < 3$

$(\frac{3}{4}, \frac{1}{4})$

$\therefore \hat{m}(\alpha) = m_0 \quad \frac{1}{4} < \alpha < \frac{3}{4}$

$\hat{m}(\alpha) = m_1 \quad -\frac{1}{4} < \alpha < \frac{1}{4}, \frac{3}{4} < \alpha < 3$





$$\begin{aligned}
 P(m_0) &= P(m_1) \Rightarrow P(m_0) = P(m_1) = .5 \\
 P(-2, m_0) &= 0 & P(-2, m_1) &= 0 \\
 P(-1, m_0) &= 0 & P(-1, m_1) &= (.125)(.5) = .0625 \\
 P(0, m_0) &= (.125)(.5) = .0625 & P(0, m_1) &= (.25)(.5) = .125 \\
 P(1, m_0) &= (.75)(.5) = .375 & P(1, m_1) &= (.25)(.5) = .125 \\
 P(2, m_0) &= (.125)(.5) = (.0625) & P(2, m_1) &= (.125)(.5) = .0625 \\
 P(3, m_0) &= 0 & P(3, m_1) &= (.125)(.5) = .0625 \\
 \hat{m}(-2) &= m_0 \text{ or } m_1 & & .0625 \\
 \hat{m}(-1) &= m_1 & & .1250 \\
 \hat{m}(0) &= m_1 & & .3750 \\
 \hat{m}(1) &= m_0 & & .1250 \\
 \hat{m}(2) &= m_1 & & .0625 \\
 \hat{m}(3) &= m_1 & & .0625 \\
 & & & \underline{.7500} \Rightarrow P[A] = .25
 \end{aligned}$$

BOB MARKS

$$\frac{30}{40}$$

$$3-4) R_i(\tau) = \overline{N_i(t) N_i(t-\tau)} = \frac{4\alpha\beta \pi^2 \tau}{4\pi^2 \tau^2} ; i=1,2$$

$$R_{12}(\tau) = \overline{N_1(t) N_2(t-\tau)} = \frac{4\alpha\beta \pi^2 \tau}{2\pi^2 \tau^2}$$

$$X_1 = N_1(t) |_{t=0}$$

$$X_2 = N_1(t) |_{t=1}$$

$$X_3 = N_2(t) |_{t=0}$$

$$(X_1, X_2) : R_1(\tau) |_{\tau=1} = 0$$

$$(X_1, X_2) : R_{12}(\tau) |_{\tau=0} = 1/2$$

$$(X_2, X_3) : R_{12}(\tau) |_{\tau=1} = 0$$

$\Rightarrow X_2$ INDEPENDENT OF X_1 AND X_3

$$\rho_{13} = 1/2 ; \sigma_1 = \sigma_3 = 1$$

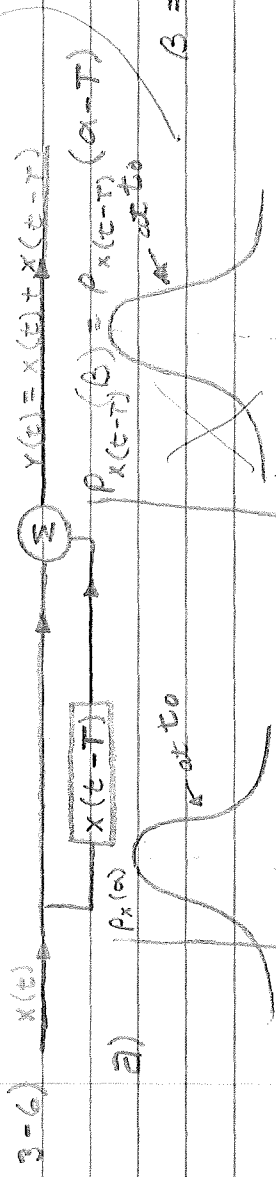
$$\Rightarrow P_{X_1, X_3}(\alpha, \beta) = \frac{1}{2\pi\sqrt{3/4}} \exp\left[-\frac{\alpha^2 - \alpha\beta + \beta^2}{2(3/4)}\right]$$

$$P_{X_2}(\gamma) = \frac{1}{\sqrt{2\pi}} \exp\left[-\frac{\gamma^2}{2}\right]$$

$$P_{X_1, X_2, X_3}(\alpha, \gamma, \beta) = (P_{X_1, X_3}(\alpha, \beta) P_{X_2}(\gamma))$$

$$= \left(\frac{1}{\sqrt{6}\pi^{3/2}} \exp\left[-\frac{\alpha^2 - \alpha\beta + \beta^2}{(1.5)} - \frac{\gamma^2}{2}\right] \right)$$

derivatives do not depend on time.



Sum of two Gaussian r.v.'s is Gaussian.

$$P_Y(\alpha) = \frac{1}{2} (P_{X(t)}(\alpha) + P_{X(t-T)}(\alpha))$$

$\Rightarrow P_Y(\alpha)$ NOT GAUSSIAN (GAUSSIAN IFF $m_X(t) = m_X$ OR $T=0$)

$$d_X(t,s) = E[(X(t) - m_X(t))(X(s) - m_X(s))]$$

$$m_Y(t) = \int_{-\infty}^{\infty} m(X) h(t-T) dF + m_X(t)$$

$$h(t) = \delta(t-T)$$

$$\Rightarrow m_Y(t) = m_X(t) + m_X(t-T)$$

$$d_Y(t,s) = E[(Y(t) - m_Y(t))(Y(s) - m_Y(s))]$$

$$\Rightarrow d_Y(t,s) = E[(X(t) + X(t-T) - m_X(t) - m_X(t-T))(X(s) + X(s-T) - m_X(s) - m_X(s-T))]$$

c) STATIONARITY $\Rightarrow m_X(t) = m_X$; $X(t) = X(t+T)$

$$\Rightarrow d_Y(t,s) = E[(X(t) + X(t-T) - 2m_X)(X(s) + X(s-T) - 2m_X)]$$

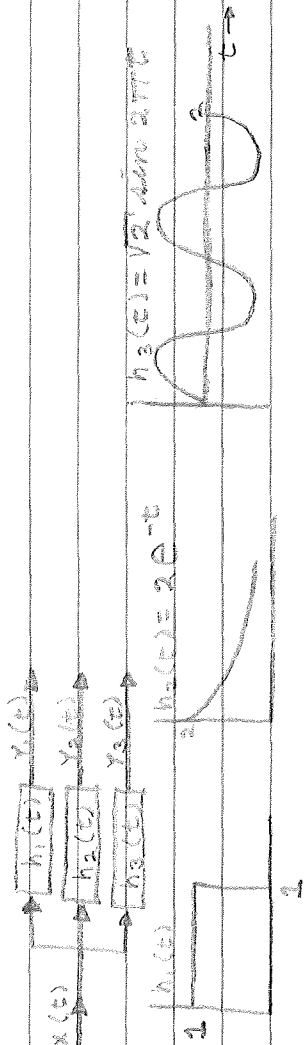
$$R_Y(t,s) = E[(X(t) + X(t-T))(X(s) + X(s-T))]$$

1) $m_Y(t) = 2m_X = \text{CONSTANT}$

2) $d_Y(t-s, 0) = E[(X(t-s) + X(t-s-T) - 2m_X)(X(0) + X(-T) - 2m_X)]$

$= d_X(t,s) \Rightarrow \text{STATIONARITY}$

3-7)



a) $Y_i(t) = X(t) \int_0^\infty h(\lambda) d\lambda$

$X(t) = 0 \Rightarrow Y_i(t) = 0; i = 1, 2, 3$

$Y_i^2(t) = \frac{N_0}{2} \int_0^\infty h^2(\lambda) d\lambda$

$Y_1^2(t) = \frac{N_0}{2} \int_0^\infty d\lambda = \frac{N_0}{2}$

$Y_2^2(t) = 2N_0 \int_0^\infty e^{-2\lambda} d\lambda = N_0 [e^{-2\lambda}]_0^\infty = N_0$

$Y_3^2(t) = N_0 \int_0^\infty \sin^2(2\pi\lambda) d\lambda = N_0 \left[\frac{\lambda}{2} - \frac{\sin(4\pi\lambda)}{8\pi} \right]_0^\infty = N_0$

b) $Y_i(t) Y_j(t) = \frac{N_0}{2} \int_0^\infty h_i(\lambda) h_j(\lambda) d\lambda = Y_i^2(t) Y_j^2(t)$

$Y_1(t) Y_2(t) = N_0 \int_0^\infty (e^{-\lambda} - \mu(t) e^{-(t-\tau)}) e^{-\tau} d\tau$

$= N_0 \int_0^\infty e^{-t} dt = N_0 e^{-t} \int_0^\infty [1 - e^{-\tau}] d\tau$

$Y_1(t) Y_3(t) = \frac{N_0}{\sqrt{2}} \int_0^\infty \sin(2\pi\lambda) d\lambda = 0$

$Y_2(t) Y_3(t) = \sqrt{2} N_0 \int_0^\infty e^{-t} \sin(2\pi\lambda) d\lambda = 0$

$= \frac{1 + \sqrt{2} N_0}{1 + \sqrt{2} N_0} [e^{-t} (\sin(2\pi\lambda) + 2\pi t \cos(2\pi\lambda))]_0^\infty$

c) $Y_1(t) Y_2(t) Y_3(t) = \frac{N_0}{2} \int_0^\infty d\lambda_1 \int_0^\infty d\lambda_2 \int_0^\infty h(\lambda_1) h(\lambda_2) h(\lambda_3) d\lambda_1 d\lambda_2 d\lambda_3 = Y_1^2(t) Y_2(t) Y_3(t)$

$Y_1(t) Y_2(t) = N_0 \int_0^\infty d\lambda_1 \int_0^\infty h(\lambda_1) h(\lambda_2) e^{-t} d\lambda_1 d\lambda_2$

$= N_0 \int_0^\infty h(\lambda_1) d\lambda_1 = N_0$

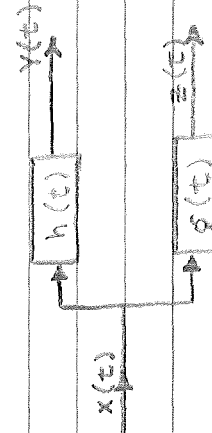
$Y_1(t) Y_3(t) = \frac{N_0}{\sqrt{2}} \int_0^\infty d\lambda_1 \int_0^\infty h(\lambda_1) h(\lambda_2) d\lambda_1 d\lambda_2$

$= \frac{N_0}{\sqrt{2}} \int_0^\infty \sin(2\pi t) dt = 0$

$Y_2(t) Y_3(t) = \sqrt{2} \int_0^\infty d\lambda_1 \int_0^\infty \sin(2\pi t) h(\lambda_2) d\lambda_1 d\lambda_2$

$\neq 0$

3-8)



a) $R_x(\tau) = \int_{-\infty}^{\infty} x(t)x(t+\tau) dt = m_x^2 + m_x \int_{-\infty}^{\infty} h(\lambda) d\lambda$
 $\bar{y} = m_x = m_x \int_{-\infty}^{\infty} h(\lambda) d\lambda$; $\bar{z} = m_x \int_{-\infty}^{\infty} h(\lambda) d\lambda$
 $\bar{y}^2 = \int_{-\infty}^{\infty} R_x(\tau) h^2(\tau) d\tau$; $\bar{z}^2 = \int_{-\infty}^{\infty} R_x(\tau) g^2(\tau) d\tau$
 $\sigma_y^2 = (\bar{y}^2 - \bar{y}^2)^{1/2}$; $\sigma_z^2 = (\bar{z}^2 - \bar{z}^2)^{1/2}$
 $\bar{y}\bar{z} = \int_{-\infty}^{\infty} d\lambda \int_{-\infty}^{\infty} h(\lambda_1)g(\lambda_2) d\lambda_2$; $\rho_{yz} = (\bar{y}\bar{z} - \bar{y}\bar{z}) / \sigma_y \sigma_z$

USING ABOVE VALUES

$$\rho_{yz}(\alpha, \beta) = \frac{1}{\sigma_y \sigma_z \sqrt{1-\rho_{xy}^2}} \exp \left[\frac{-1}{2(1-\rho_{xy}^2)} \left[\frac{(\alpha-\bar{y})^2}{\sigma_y^2} - \frac{2\rho_{xy}(\alpha-\bar{y})(\beta-\bar{z})}{\sigma_y \sigma_z} + \frac{(\beta-\bar{z})^2}{\sigma_z^2} \right] \right]$$

b) $\bar{y}(t)x(t-\tau) = E [x(t-T)Y(t)]$
 $= E [x(t-T) \int_{-\infty}^{\infty} x(t-\lambda)h(\lambda) d\lambda]$
 $= \int_{-\infty}^{\infty} E [x(t-\tau)x(t-\lambda)] h(\lambda) d\lambda$
 $= \int_{-\infty}^{\infty} R_x(\tau-\lambda)h(\lambda) d\lambda$
 $= \int_{-\infty}^{\infty} [R_x(\tau-\lambda) + m_x^2] h(\lambda) d\lambda$

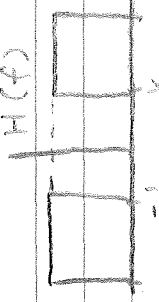
$$R_x(\tau) = S_0 \delta(\tau)$$

$$\Rightarrow \bar{y}(t)x(t-\tau) = \int_{-\infty}^{\infty} S_0 \delta(\tau-\lambda) h(\lambda) d\lambda = S_0 h(\tau)$$

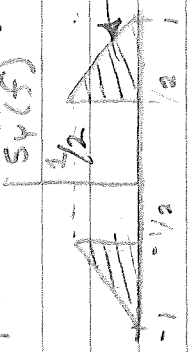
c) $\bar{y}(t)z(t) = Y(t)\bar{z}(t)$; $\bar{y}(t_1, t_2) = 0$

$$\int_{-\infty}^{\infty} d\lambda \int_{-\infty}^{\infty} h(\lambda_1)g(\lambda_2) d\lambda_2 = \int_{-\infty}^{\infty} h(\lambda) d\lambda \int_{-\infty}^{\infty} g(\lambda) d\lambda$$

d) $m_x = 0 \Rightarrow R_x(\tau) = R_x(\tau) = (\sin \pi \tau / \pi \tau) \Rightarrow S_x(f) = \text{rect}(f)$



$$S_y(f) = S_x(f) |H(f)|^2$$



$$S_y(f) = 2 - |f| = \frac{df}{f}$$

$$\Delta P = \int_{-1/2}^{1/2} (2 - |f|) df$$

FOR $\frac{1}{2} < |f| < 1$
 $\frac{1}{2} < f < 1$
 0 ELSEWHERE

$$\bar{y}\bar{z} = \int_{-\infty}^{\infty} S_y(f) df = \frac{1}{4}$$

10/10

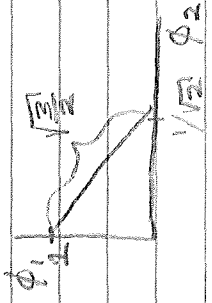
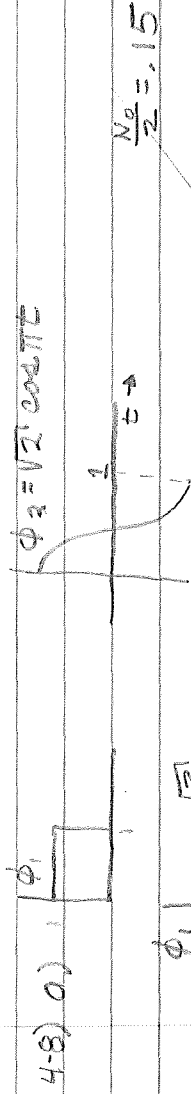
()

()

()

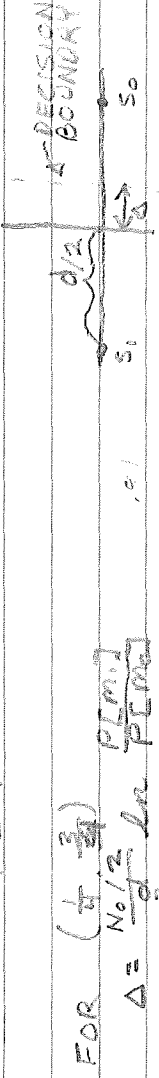
()

()



$$P[\varepsilon] = Q\left[\frac{d}{\sqrt{2}N_0}\right] = Q\left[\frac{3}{\sqrt{4(0.3)}}\right]$$

$$= Q[1.5] = 0.06$$

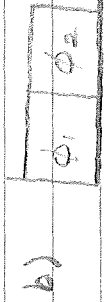


$$= \frac{1/2}{\sqrt{2}N_0} \ln 3 = 4.05$$

$$P[\varepsilon] = P[m_0] Q\left[\frac{d-2\Delta}{\sqrt{2}N_0}\right] + P[m_1] Q\left[\frac{d+2\Delta}{\sqrt{2}N_0}\right]$$

$$= \frac{1}{4} Q[4.13] + \frac{3}{4} Q[2.76]$$

$$= \frac{1}{4} (3 \times 10^{-1}) + \frac{3}{4} (2 \times 10^{-3}) = 0.075 + 0.0015 = 0.077$$



$$s_0 = (2, 0)$$

$$s_1 = (2, 2) \Rightarrow d = 2$$

$$P[\varepsilon] = Q\left[\frac{d}{\sqrt{2}N_0}\right] = Q[2.6] = 4 \times 10^{-3}$$

FOR $(\frac{1}{4}, \frac{3}{4})$

$$2\Delta = \frac{N_0}{d} \ln 3 = (1.5)(1.1) = 1.65$$

$$P[\varepsilon] = \frac{1}{4} Q\left[\frac{d-2\Delta}{\sqrt{2}N_0}\right] + \frac{3}{4} Q\left[\frac{d+2\Delta}{\sqrt{2}N_0}\right]$$

$$= \frac{1}{4} Q[4.5] + \frac{3}{4} Q[4.7]$$

$$= \frac{1}{4} (0.3) + \frac{3}{4} (1.5 \times 10^{-3}) = 0.075$$

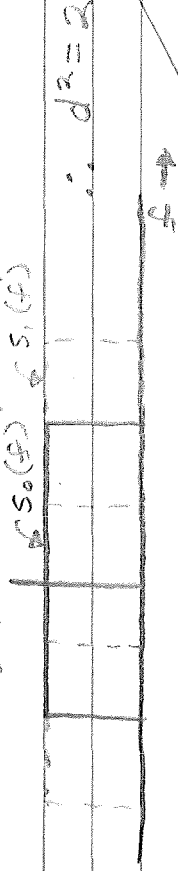
should be lower when the message is not equiprobable



c) BY PARSEVAL'S THEM:

$$d^2 = \int_{-\infty}^{\infty} [s_1(f) - s_0(f)]^2 df$$

$$= \int_{-\infty}^{\infty} [s_1^2(f) - 2s_1(f)s_0(f) + s_0^2(f)] df$$



$$P[\varepsilon] = Q\left[\frac{d}{\sqrt{2N_0}}\right] = Q[1.83] = 4 \times 10^{-2}$$

FOR $\left(\frac{1}{4}, \frac{3}{4}\right)$

$$\Delta = \sqrt{\frac{15}{\pi}} \ln 3 = 1.17 \Rightarrow 2\Delta = 2.34$$

$$P[\varepsilon] = \frac{1}{4} Q\left[\frac{4.18}{1.65}\right] + \frac{3}{4} Q\left[\frac{1.65}{1.65}\right]$$

$$= \frac{1}{4} Q[2.53] + \frac{3}{4} Q[1]$$

$$= \frac{1}{4} (6 \times 10^{-2}) + \frac{3}{4} (10^{-2})$$

$$= 2.25 \times 10^{-2}$$

4-9) $\phi_i(t)$

1	$\phi_0(t)$	$\phi_1(t)$
0	1	2

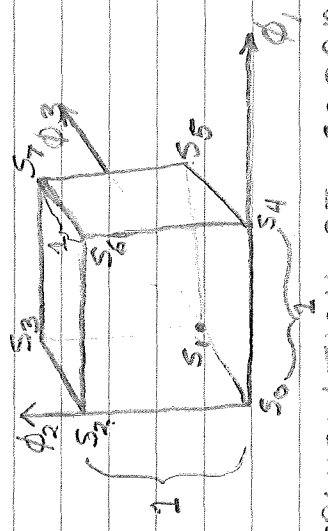
\rightarrow

\Rightarrow ORTHONORMAL BASIS FUNCTIONS

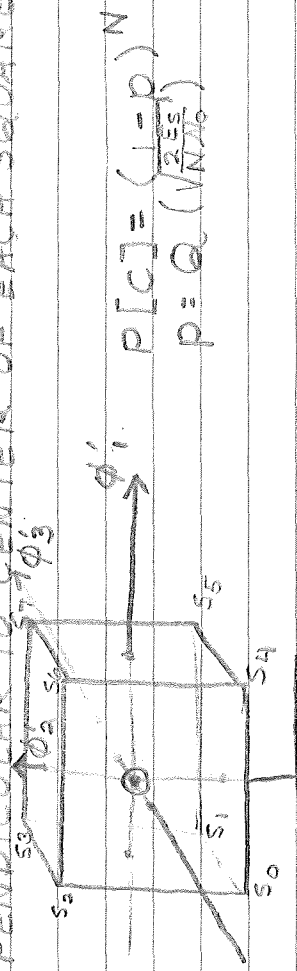
$\int_{-\infty}^{\infty} \phi_i(t) \phi_j(t) dt = 0 \quad i \neq j$

$\int_{-\infty}^{\infty} \phi_i^2(t) dt = 1 \quad i = 1, 2, 3$

- $S_0 = (0, 0, 0)$
- $S_1 = (0, 0, 1)$
- $S_2 = (0, 1, 0)$
- $S_3 = (0, 1, 1)$
- $S_4 = (1, 0, 0)$
- $S_5 = (1, 0, 1)$
- $S_6 = (1, 1, 0)$
- $S_7 = (1, 1, 1)$



TRANSLATION OF COORDINATES DOES NOT AFFECT VALUE OF $P[C]$. DEFINE $\phi'_i(t), i = 1, 2, 3$ PERPENDICULAR TO CENTER OF EACH SQUARE FACE:



$P[C] = (1-p)^N$
 $p = Q\left(\sqrt{\frac{2Es}{N_0}}\right)$

$\sqrt{E_s} = \sqrt{\frac{1}{2} + \frac{1}{2}} \Rightarrow E_s = 3/2$
 $N = 3$

$\Rightarrow P = Q\left(\sqrt{\frac{3}{2} N_0}\right) = Q\left(\sqrt{\frac{3}{2}}\right)$
 $\Rightarrow P[C] = (1 - Q\left(\sqrt{\frac{3}{2}}\right))^3$

$\therefore P[E] = 1 - P[C] = 1 - [1 - Q\left(\sqrt{\frac{3}{2}}\right)]^3$

$$4-11) s_0(t) = \sqrt{10^3} \cos 2\pi \cdot 10^6 t \quad \text{C.S.T. } 2 \cdot 10^{-3}$$

$$s_1(t) = \sqrt{10^3} \cos 2\pi (10^6 + \Delta) t \quad \text{C.S.T. } 2 \cdot 10^{-3}$$

$$\begin{aligned} \sqrt{10^3} \int_{-\infty}^{\infty} s_0(t) s_1(t) dt &= \int_0^{10^{-3}} \cos 2\pi 10^6 t \cos 2\pi (10^6 + \Delta) t dt \\ &= \frac{1}{2} \int_0^{10^{-3}} (\cos 2\pi \Delta t + \cos 2\pi (2 \cdot 10^6 + \Delta) t) dt \\ &= \frac{1}{2} \left[\frac{\sin 2\pi \Delta t}{2\pi \Delta} + \frac{\sin 2\pi (2 \cdot 10^6 + \Delta) t}{2\pi (2 \cdot 10^6 + \Delta)} \right]_0^{10^{-3}} \end{aligned}$$

$$= 0 \quad \text{FOR } \Delta = 500, 250$$

$\Rightarrow s_0(t)$ AND $s_1(t)$ ARE ORTHOGONAL

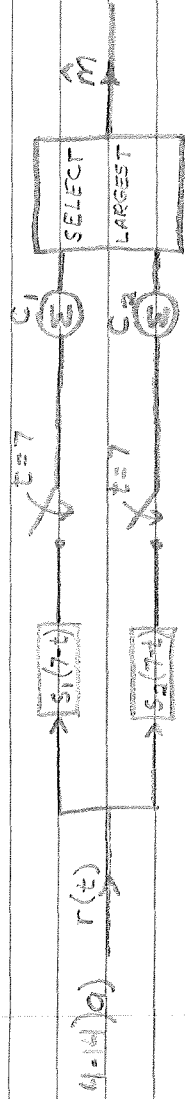
$$10 \log_{10} \frac{E}{W} = 10 \log_{10} 6$$

$$= 7.78$$

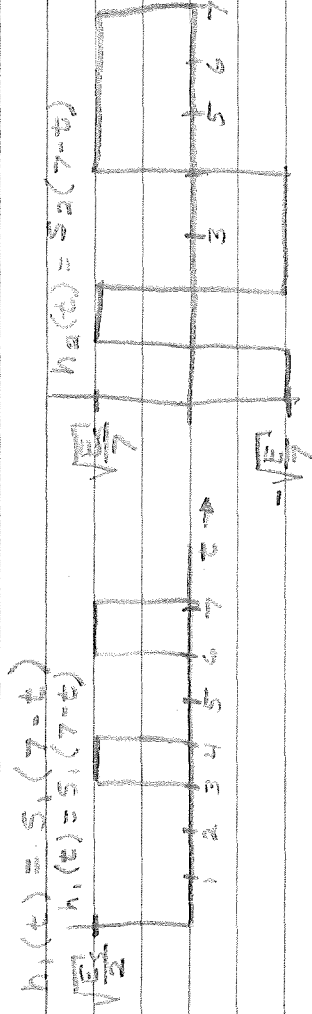
FROM FIG. 4-37:

$$P[E] \approx 0.0093$$

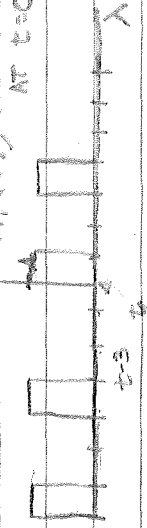
$$(0.007)$$



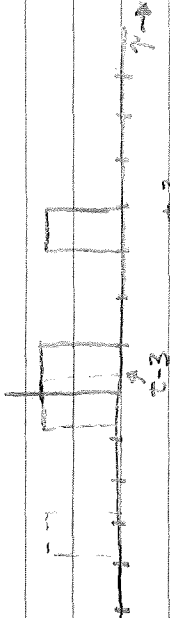
$$s_i = \frac{1}{2} (N_0 \ln P[m_i] - |s_i|^2)$$



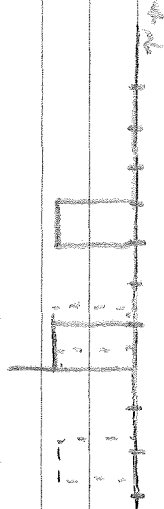
GIVEN $s_1(t)$ INTO FILTER WITH IMPULSE RESPONSE $h_1(t)$, OUTPUT $u_1(t) = s_1(t) * h_1(t)$ AT $t=0$ ($A^2 = E/7$)



$$s_1(t) * h_1(t) = 0 \quad \infty < t < 3$$

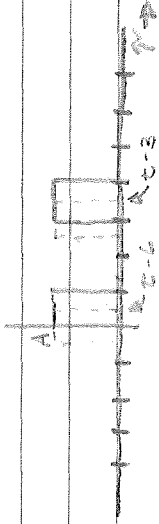


$$s_1(t) * h_1(t) = \int_0^{t-3} A^2 d\gamma = A^2(t-3) \quad 3 \leq t \leq 4$$



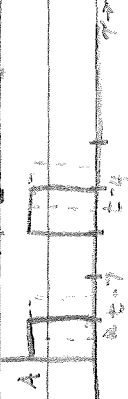
$$s_1(t) * h_1(t) = \int_{t-1}^1 A^2 dt = A^2 [t]_{t-1}^1 = A^2 [1 - (t-4)] = A^2 (5-t) \quad 4 \leq t \leq 5$$

$$s_1(t) * h_1(t) = 0 \quad 5 \leq t \leq 6$$



$$s_1(t) * h_1(t) = \int_0^{t-3} A^2 d\tau + \int_0^{t-6} A^2 d\tau$$

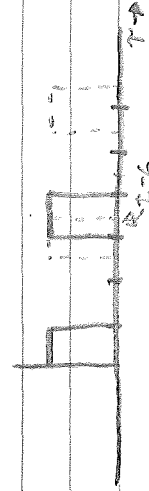
$$= A^2 [t-3-3] + A^2 [t-6] = A^2 [2t-12] \quad 6 \leq t \leq 7$$



$$s_1(t) * h_1(t) = \int_0^{t-7} A^2 d\tau + \int_0^{t-4} A^2 d\tau$$

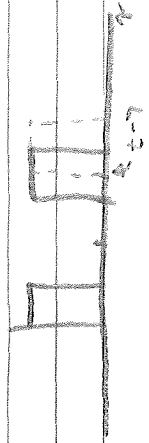
$$= A^2 [1-t+7+4-t+4] = A^2 [-2t+16] \quad 7 \leq t \leq 8$$

$$s_1(t) * h_1(t) = 0 \quad ; \quad 8 \leq t \leq 9$$



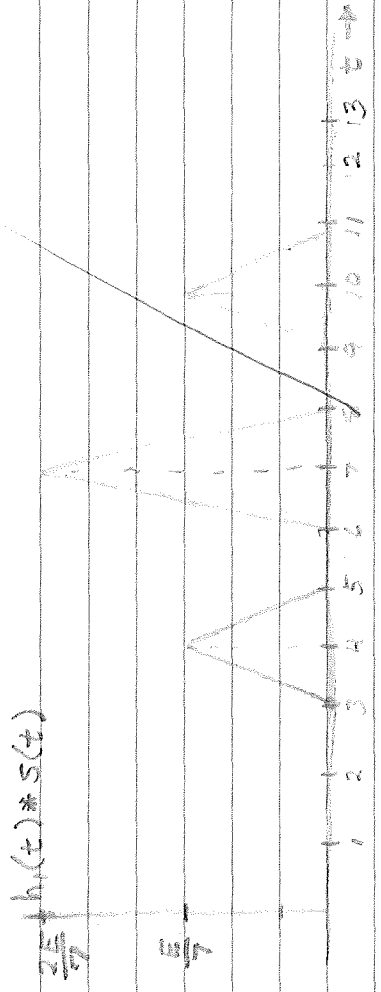
$$s_1(t) * h_1(t) = \int_0^{t-6} A^2 d\tau = A^2 [t-6-3] = A^2 [t-9]$$

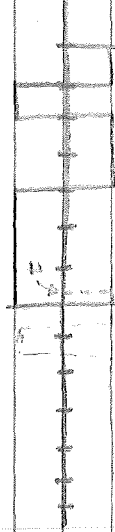
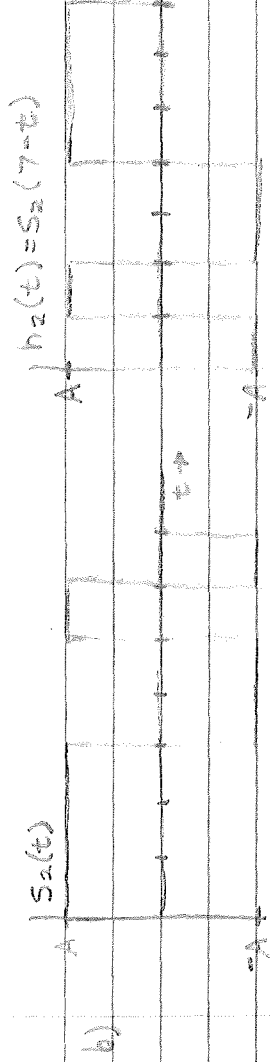
$$9 \leq t \leq 10$$



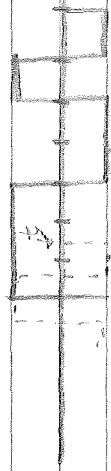
$$s_1(t) * h_1(t) = \int_0^{t-7} A^2 d\tau = A^2 (4-t+7) = A^2 (-t+11)$$

$$10 \leq t \leq 11$$





$$S_2(t) * h_2(t) = \int_0^t A^2 d\tau = A^2 t \quad 0 \leq t \leq 1$$



$$S_2(t) * h_2(t) = \int_{t-1}^t A^2 d\tau + \int_0^{t-1} A^2 d\tau = A^2 [t - (t-1)] + A^2 [t-1] = A^2 [t-1] \quad 1 \leq t \leq 3$$



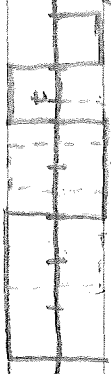
$$S_2(t) * h_2(t) = \int_0^{t-2} A^2 d\tau + \int_{t-2}^{t-1} A^2 d\tau + \int_{t-1}^t A^2 d\tau = A^2 [2 - (t-2)] + A^2 [(t-1) - (t-2)] + A^2 [(t-1) - (t-1)] = A^2 (2-t) \quad 3 \leq t \leq 4$$



$$S_2(t) * h_2(t) = \int_0^t A^2 d\tau + \int_{t-1}^t A^2 d\tau + \int_{t-2}^{t-1} A^2 d\tau + \int_0^{t-2} A^2 d\tau = A^2 [(t-3) + (t-4) + (1) + (2-t)] = A^2 (t-4) \quad 4 \leq t \leq 5$$

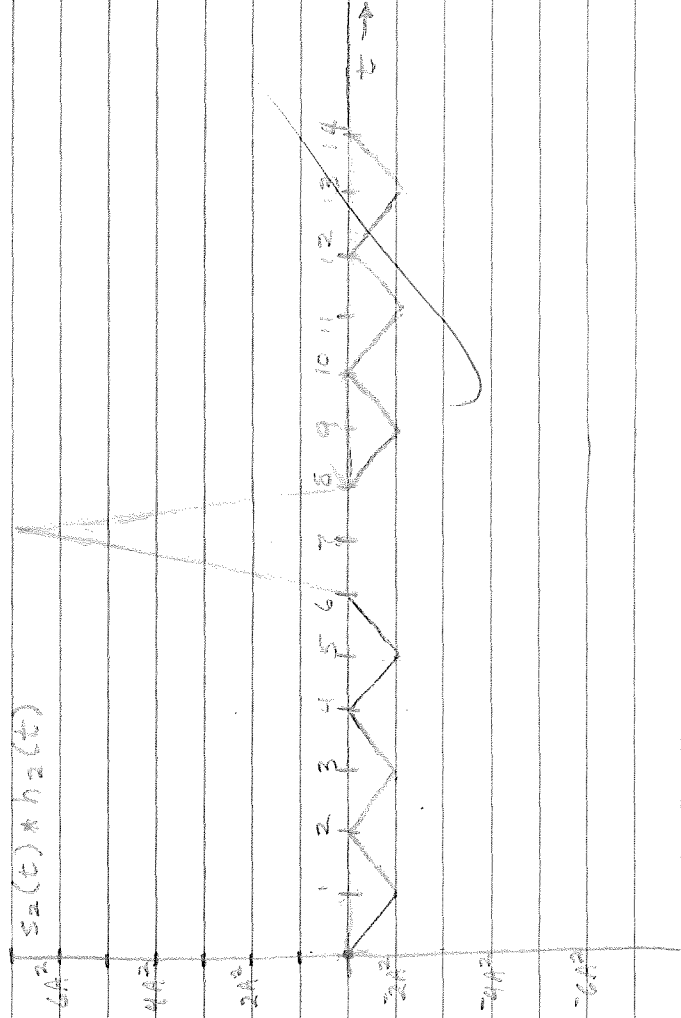


$$S_2(t) * h_2(t) = \int_{t-1}^t A^2 d\tau + \int_0^{t-1} A^2 d\tau + \int_{t-2}^{t-1} A^2 d\tau + \int_{t-3}^{t-2} A^2 d\tau + \int_0^{t-3} A^2 d\tau = A^2 [(1) + (5-t) + (-2) + (t-4)] = A^2 (4-t) \quad 5 \leq t \leq 6$$



$$S_2(t) * h_2(t) = \int_0^{t-4} A^2 d\tau + \int_0^{t-5} A^2 d\tau + \int_{t-1}^t A^2 d\tau + \int_{t-2}^{t-1} A^2 d\tau + \int_0^{t-2} A^2 d\tau + \int_{t-3}^{t-2} A^2 d\tau = A^2 [(5-t) + (6-t) + (1) + (t-5) + (t-4)] = A^2 (t-6) \quad 6 \leq t \leq 7$$

$$S_2(t) * h_2(t) = A^2(t-14) \quad 13 \leq t \leq 14$$



c) $s_1(t) * h_2(t)$

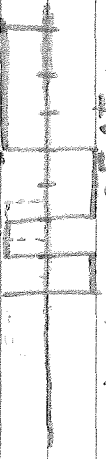


$$s_1(t) * h_2(t) = \int_0^t -d\gamma \quad A^2 = A^2 [-t] \quad 0 \leq t \leq 1$$



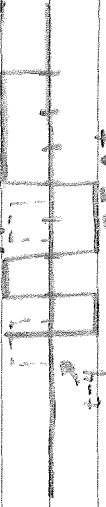
$$s_1(t) * h_2(t) = A^2 \left[\int_1^t d\gamma + \int_{t-1}^t -d\gamma \right] = A^2 [(t-1) + (t-2)] \quad 1 \leq t \leq 2$$

$$= A^2 [2t-3]$$



$$s_1(t) * h_2(t) = A^2 \left[\int_2^t d\gamma + \int_{t-2}^t -d\gamma \right] = A^2 [(2-t) + (t-3)] \quad 2 \leq t \leq 3$$

$$= A^2 [-2t+5]$$

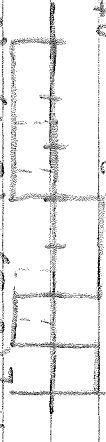


$$s_1(t) * h_2(t) = A^2 \left[\int_{t-1}^t -d\gamma + \int_0^{t-3} d\gamma \right] = A^2 [-1-t+3] = A^2 [-t+2] \quad 3 \leq t \leq 4$$



$$s_1(t) * h_2(t) = A^2 \left[\int_{t-4}^t d\gamma + \int_{t-1}^{t-4} -d\gamma + \int_4^t d\gamma \right]$$

$$= A^2 [(t-5) + (t-4) + (t-5) + (t-4)] = A^2 [4t-18] \quad 4 \leq t \leq 5$$



$$s_1(t) * h_2(t) = A^2 \left[\int_{t-5}^t d\gamma + \int_{t-2}^{t-5} -d\gamma + \int_{t-1}^t -d\gamma \right]$$

$$= A^2 [(t+6) + (-t+5) + 1] = A^2 (-2t+12) \quad 5 \leq t \leq 6$$

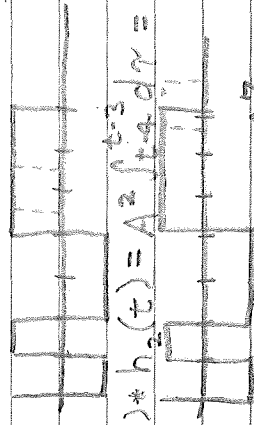


$$s_1(t) * h_2(t) = A^2 \left[\int_{t-6}^{t-3} -d\gamma + \int_{t-1}^t d\gamma \right] = 0 \quad 6 \leq t \leq 7$$



$$s_1(t) * h_2(t) = A^2 \left[\int_{t-4}^t d\gamma + \int_{t-3}^{t-4} d\gamma + \int_{t-1}^t -d\gamma \right]$$

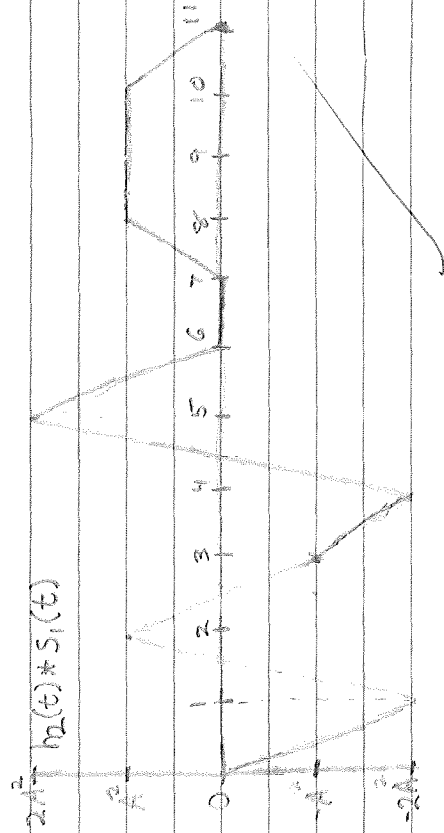
$$= A^2 [(t-8) + (t-7) + (-t+8)] = A^2 [t-7] \quad 7 \leq t \leq 8$$



$$s_1(t) * h_2(t) = A^2 \int_{t-4}^{t-3} d\tau = A^2 \quad 8 \leq t \leq 10$$



$$s_1(t) * h_1(t) = A^2 \int_{t-4}^{t-1} d\tau = A^2(-t+1) \quad 10 \leq t \leq 11$$



4-18)

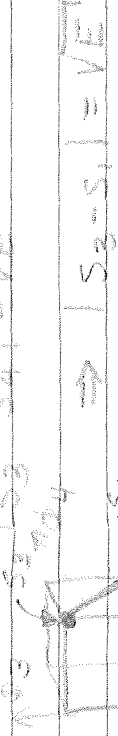
1	2	3	4
ϕ_1	ϕ_2	ϕ_3	ϕ_4

(A) $s_1 = \sqrt{E/2} [1001]$ (B) $s_1 = \sqrt{E} [0001]$
 $s_2 = \sqrt{E/2} [0110]$ $s_2 = \sqrt{E} [0100]$
 $s_3 = \sqrt{E/2} [1010]$ $s_3 = \sqrt{E} [0010]$
 $s_4 = \sqrt{E/2} [0101]$ $s_4 = \sqrt{E} [1000]$

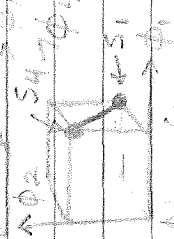
a) $\int_{-\infty}^{\infty} s_i^2(t) dt = E \quad \forall i=1,2,3,4$ IN A OR B

b) s_1, \dots, s_4 ARE ORTHOGONAL TO EACH OTHER
 $\Rightarrow |s_i - s_j| = \sqrt{E}$

s_1, \dots, s_4 ARE ORTHOGONAL TO EACH OTHER
 $|s_3 - s_4| = \sqrt{E}$

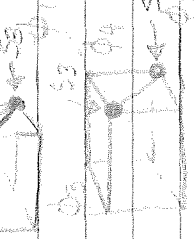


$\Rightarrow |s_3 - s_1| = \sqrt{E}$



$\Rightarrow |s_4 - s_1| = \sqrt{E}$

$\Rightarrow |s_3 - s_2| = \sqrt{E}$



$\Rightarrow |s_4 - s_2| = \sqrt{E}$

$\therefore P_A[E] = P_A[E/m_i] = \sum_{k=0}^{M-1} \sum_{j \neq k} P_2[s_i, s_k]$
 $= \sum_{i=0}^{M-1} \sum_{j \neq k} Q \left[\frac{|s_i - s_k|}{\sqrt{2}N_0} \right] = 3 Q \left[\frac{\sqrt{E}}{\sqrt{2}N_0} \right]$

FOR SET B (ORTHOGONAL): $P[E] = P[E/m_i] \leq 3 Q \left[\frac{\sqrt{E}}{N_0} \right]$

$$P_A[\epsilon] = 30 \left[\frac{\epsilon}{2N_0} \right]; P_B[\epsilon] = 30 \left[\frac{\epsilon}{N_0} \right]$$

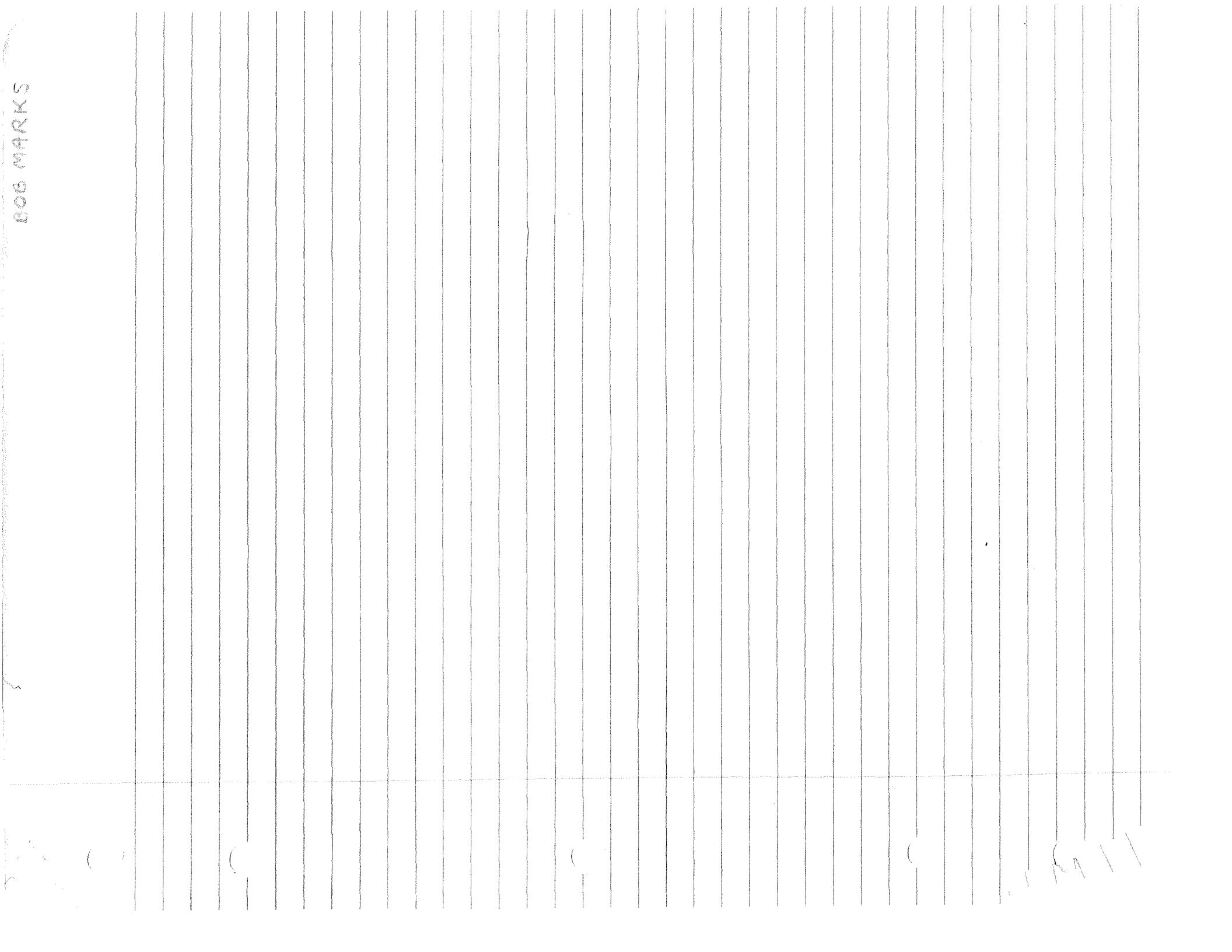
FOR SMALL $P[\epsilon] \approx 10^{-7}$

$$10 \log_{10} \left[\frac{\epsilon}{2N_0} \right] \approx 11 \text{ dB}; 10 \log_{10} \left[\frac{\epsilon}{N_0} \right] \approx 14 \text{ dB}$$

\Rightarrow B COMMUNICATES ABOUT 3 dB

MORE EFFECTIVELY THAN A

DOG MARKS



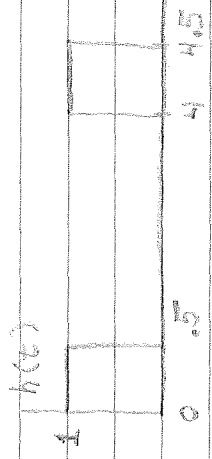
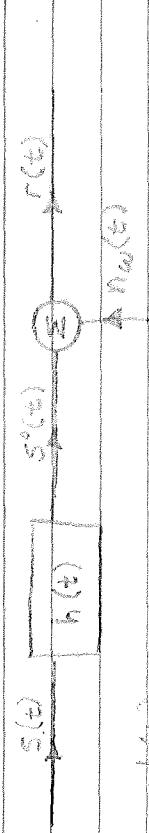
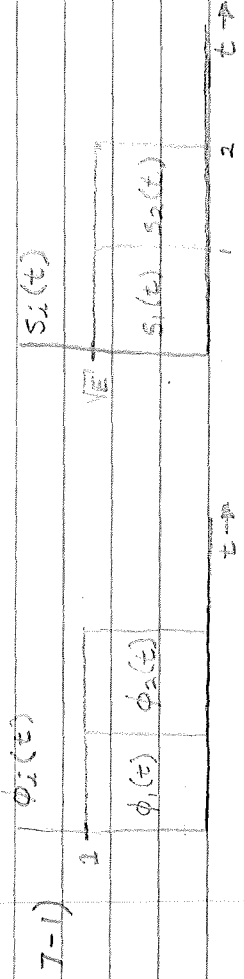
(

(

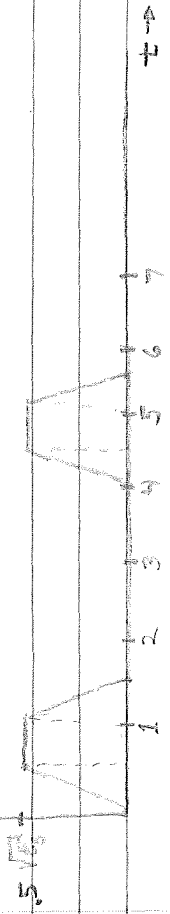
(

(

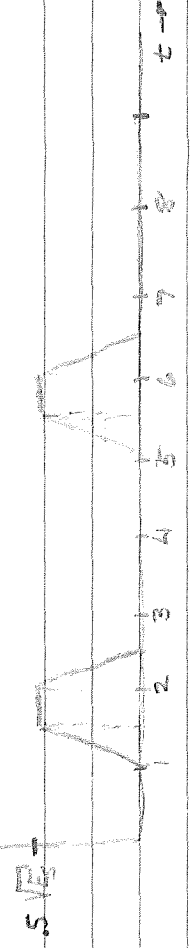
1/27/11



a) $S^o(t) = S_i(t) * h(t)$
 $S^o(t) = \sqrt{E_s} \int_0^t dt = \sqrt{E_s} t \quad 0 \leq t \leq .5$
 $S^o(t) = \sqrt{E_s} \int_0^{.5} dt + \sqrt{E_s} \int_{.5}^t dt = (.5) \sqrt{E_s} + \sqrt{E_s} (t - .5) \quad .5 \leq t \leq 4.5$
 $S^o(t) = \sqrt{E_s} \int_0^{.5} dt + \sqrt{E_s} \int_{.5}^{1.5} dt = \sqrt{E_s} (1.5 - t) \quad 1 \leq t \leq 1.5$
 $S^o(t) = 0 \quad t > 1.5$

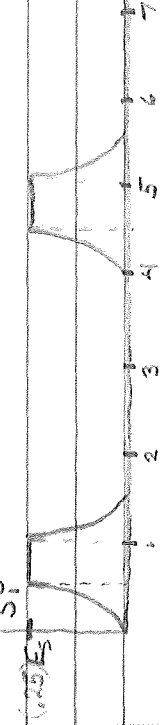


SIMILARLY
 $S^o(t) = S^o(t-1)$



$$d^2 = \int_{-\infty}^{\infty} [s_1^2(t) - s_2^2(t)]^2 dt$$

$$= \int_{-\infty}^{\infty} [s_1^2(t) - 2s_1^2(t)s_2^2(t) + s_2^2(t)] dt$$

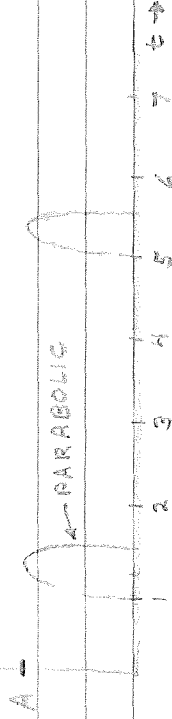


$$\int_{-\infty}^{\infty} s_1^2(t) dt = \int_{-\infty}^{\infty} s_2^2(t) dt$$

$$= \left(\frac{1}{4} E_s\right) + \left(\frac{1}{4} E_s \frac{1}{2}\right)$$

$$= \frac{3}{8} E_s$$

$$s_1^2(t) s_2^2(t)$$



ANALYSIS TO FIND A

$$\frac{\sqrt{E_s}}{4} \left(\frac{\sqrt{E_s}}{2} - \frac{\sqrt{E_s}}{2} t \right) \left(\frac{\sqrt{E_s}}{2} - t \right)$$

$$= \frac{E_s}{8} t - \frac{E_s}{4} t^2$$

MAX OCCURS AT $t = \frac{1}{4}$

$$\Rightarrow A = E_s \left(\frac{1}{8} \cdot \frac{1}{4} - \frac{1}{4} \cdot \left(\frac{1}{4}\right)^2 \right) = \frac{1}{64} E_s$$

$\frac{1}{2}$ $t \rightarrow$

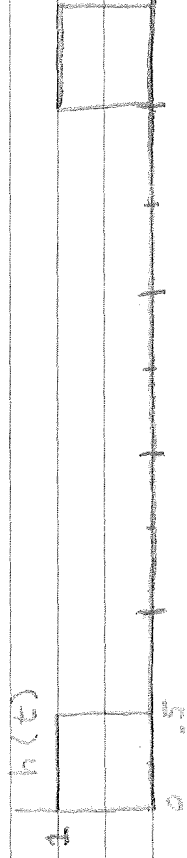
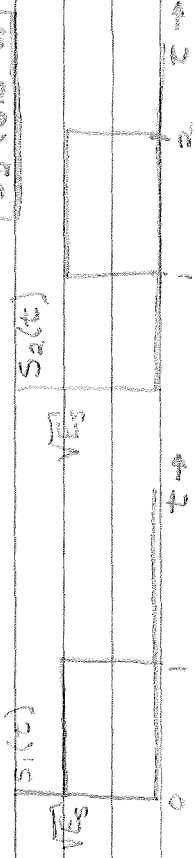
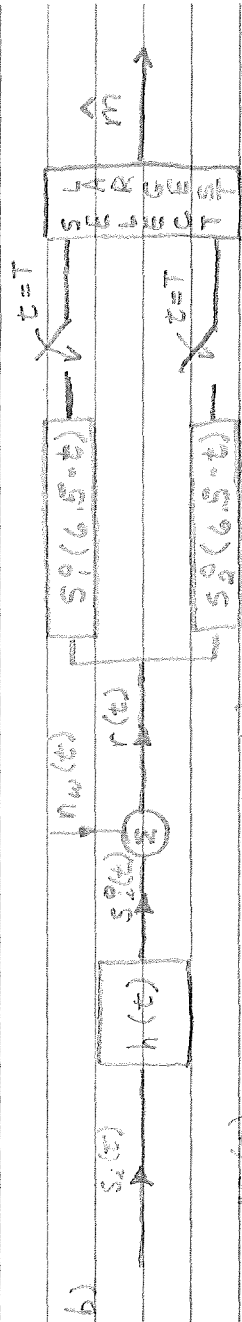
$$\Rightarrow \int_{-\infty}^{\infty} 2 s_1^2(t) s_2^2(t) dt = 2 \left[\frac{1}{8} \left(\frac{1}{4} \right) \frac{1}{4} E_s \right] = \frac{1}{8} E_s$$

$$\therefore d^2 = (843 \cdot 0.21) E_s = 8.22 E_s$$

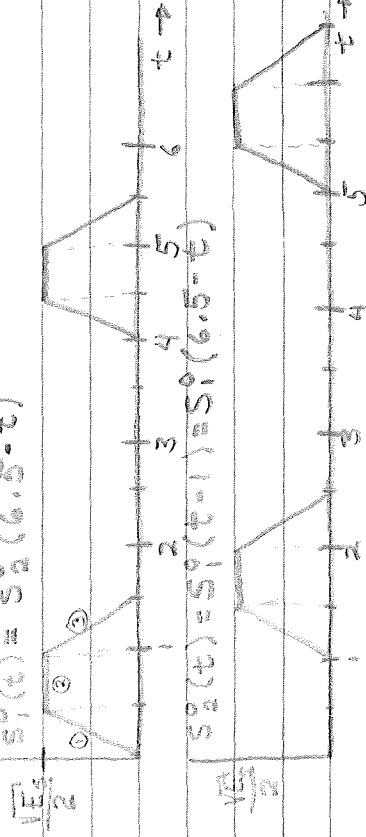
$$\Rightarrow d = 90.8 \sqrt{E_s}$$

$$P[E] = Q \left[\frac{d}{\sqrt{2} N_0} \right] = Q \left[\frac{90.8 \sqrt{E_s}}{\sqrt{2} N_0} \right]$$

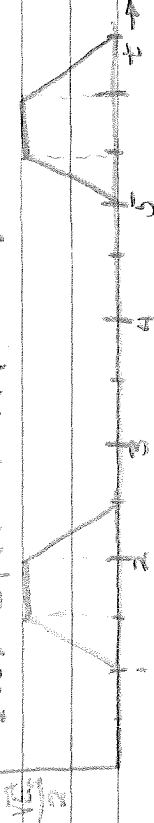
$$= Q \left[\frac{90.8 \sqrt{5}}{1.44} \right] = Q[1.44] = 5.66 \times 10^{-2}$$



$$S_1^0(t) = S_2^0(6.5-t)$$



$$S_2^0(t) = S_1^0(t-1) = S_1^0(6.5-t)$$



IN ABSENCE OF NOISE, OUTPUT OF $S_1^0(6.5-t)$ FILTER GIVEN $S_1(t)$ TRANSMITTED IS SAME AS $S_2^0(6.5-t)$ FILTER GIVEN $S_2(t)$ TRANSMITTED.

$$\text{i.e. } S_1^0(t) * S_1^0(6.5-t) = S_2^0(6.5-t) * S_2^0(t)$$

ALSO, OUTPUT OF $S_1^0(6.5-t)$ FILTER GIVEN $S_2(t)$ WAS TRANSMITTED IS $S_1^0(t) * S_1^0(6.5-t)$ SHIFTED TO THE LEFT ONE TIME UNIT

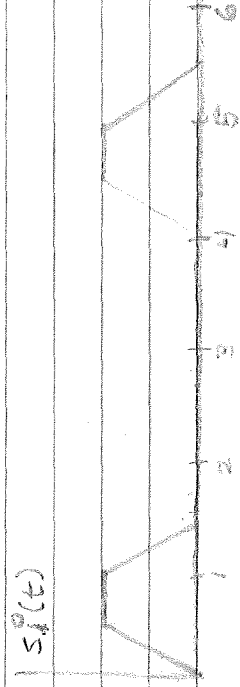
$$\text{i.e. } X(t) = S_1^0(t) * S_1^0(6.5-t);$$

$$S_2^0(t) * S_1^0(6.5-t) = X(t+1)$$

SIMILARLY,

$$\text{GIVEN } X(t) = S_2^0(t) * S_2^0(6.5-t);$$

$$S_1^0(t) * S_2^0(6.5-t) = X(t-1)$$

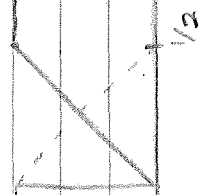


$$\begin{aligned}
 s_1^p(t) &= \sqrt{E_3} t & 0 \leq t \leq 1 \\
 s_1^p(t) &= \frac{1}{2} \sqrt{E_3} & 1 \leq t \leq 2 \\
 s_1^p(t) &= \sqrt{E_3} \left(\frac{3}{2} - t\right) & 2 \leq t \leq 3 \\
 s_1^p(t) &= \sqrt{E_3} (t-4) & 3 \leq t \leq 4 \\
 s_1^p(t) &= \frac{1}{2} \sqrt{E_3} & 4 \leq t \leq 5 \\
 s_1^p(t) &= \sqrt{E_3} (t - \frac{1}{2}) & 5 \leq t \leq 6
 \end{aligned}$$

AT $t=0$, $x(t+1) = 0$

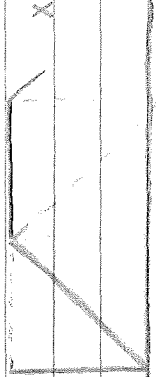
AT $t=1/2$

$$\begin{aligned}
 x(t+1) &= \int_0^{1/2} \lambda \left(\frac{1}{2} - \lambda\right) d\lambda \\
 &= \left[\frac{1}{4} \lambda^2 - \frac{1}{3} \lambda^3 \right]_0^{1/2} \\
 &= \frac{1}{16} - \frac{1}{24} = \frac{1}{48}
 \end{aligned}$$



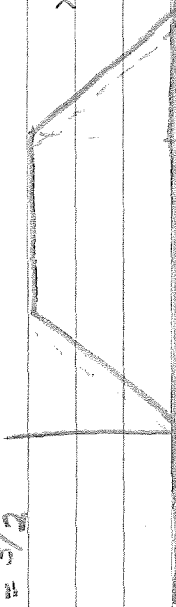
AT $t=1$

$$\begin{aligned}
 x(t+1) &= \int_{1/2}^1 (1-\lambda) d\lambda + \int_0^{1/2} \frac{1}{2} \lambda d\lambda \\
 &= \left[\lambda - \frac{1}{2} \lambda^2 \right]_{1/2}^1 + \frac{1}{4} \lambda^2 \Big|_0^{1/2} \\
 &= \frac{1}{4} = \frac{1}{32}
 \end{aligned}$$

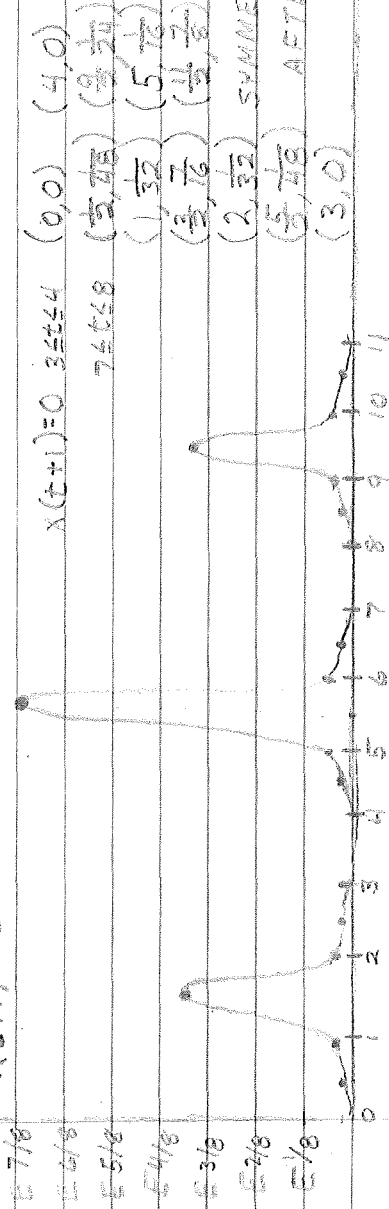


AT $t=3/2$

$$\begin{aligned}
 x(t+1) &= \int_{3/2}^2 (\frac{3}{2} - \lambda) \left(\frac{3}{2} - \lambda + \lambda\right) d\lambda \\
 &\quad + \int_{1/2}^1 \frac{1}{4} d\lambda \\
 &\quad + \int_0^{1/2} \lambda \left(\frac{3}{2} - \lambda\right) d\lambda \\
 &= \frac{3}{4} \lambda - \frac{1}{4} \lambda^2 \Big|_{3/2}^2 + \frac{1}{4} \lambda \Big|_{1/2}^1 + \frac{1}{4} \lambda^2 - \frac{1}{3} \lambda^3 \Big|_0^{1/2} \\
 &= \frac{3}{4} - \frac{3}{4} + \frac{3}{8} + \frac{1}{8} + \frac{1}{8} - \frac{1}{24} = \frac{7}{16}
 \end{aligned}$$

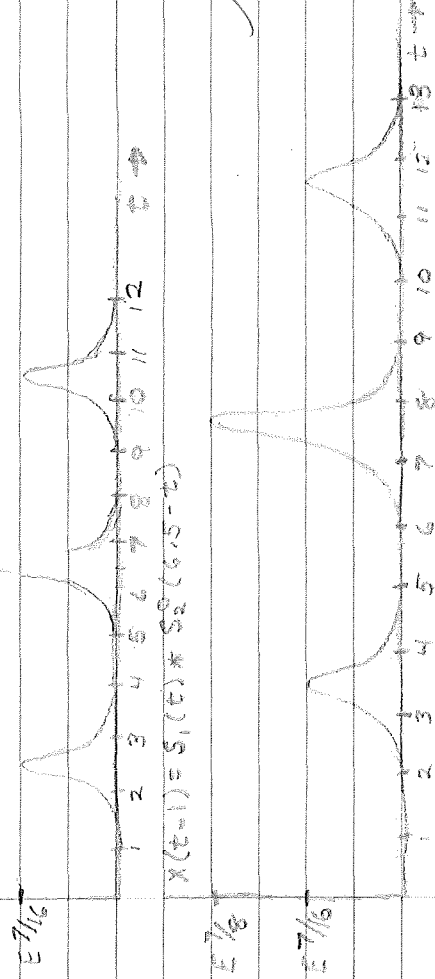


$$x(t+1) = S_2(t) * S_1^2(6.5-t)$$



THE RIGHT HALF OF THE FIRST PULSE IS SYMMETRIC WITH THE COMPUTED LEFT HALF. THE SECOND PULSE IS TWICE THE AMPLITUDE OF THE FIRST, AND THE LAST PULSE IS SIMILAR TO THE FIRST. ALL SEGMENTS CONNECTING DARKENED POINTS ABOVE ARE CUBICS.

$$x(t) = S_1^2(t) * S_1^2(6.5-t) = S_2^2(t) * S_2^2(6.5-t)$$



$$7-2) \quad H(s) = \frac{s^2 - 5s^2 + 11s - 15}{s^4 + 5s^3 + 8s^2 + 6s}$$

$$a) \quad \frac{S_W(s)}{S_D(s)} \quad \boxed{H(s)} \quad S_D(s)$$

$$S_W(s) H(s) H(-s) = S_A(f) \quad ; \quad S_D(s) = 1$$

$$\Rightarrow S_A(s) = \frac{s^4 + 5s^3 + 8s^2 + 6s}{s^3 - 5s^2 + 11s - 15} = \frac{s^4 - 5s^3 + 8s^2 - 6s}{-s^3 - 5s^2 - 11s - 15}$$

$$\frac{s^2 - 2s + 5}{s^3 - 5s^2 + 11s - 15} \quad \frac{s^2 - 2s - 5}{s^3 - 5s^2 - 11s - 15}$$

$$\frac{-2s^2 + 11s}{-2s^2 + 6s} \quad \frac{-2s^2 - 11s}{-2s^2 - 6s}$$

$$\frac{5s - 15}{5s - 15}$$

$$\frac{5s - 15}{5s - 15}$$

$$s^2 + 2s + 2$$

$$+s^2 - 2s + 2$$

$$s + 3 \quad \frac{s^3 + 5s^2 + 8s + 6}{s^3 + 3s^2} \quad s - 3 \quad \frac{s^3 - 5s^2 + 8s - 6}{s^3 - 3s^2}$$

$$2s^2 + 2s$$

$$2s^2 + 6s$$

$$2s^2 + 8s$$

$$2s^2 + 6s$$

$$-2s^2 + 6s$$

$$2s + 6$$

$$2s - 6$$

$$2s + 6$$

$$2s - 6$$

$$\therefore S_A(s) = \frac{s(s+3)(s^2+2s+2)}{(s-3)(s^2-2s+5)} = \frac{s(s+3)(s^2-2s+2)}{(s-3)(s^2+2s+5)}$$

$$= \frac{s(s^2+2s+2)}{(s^2-2s+5)} = \frac{s(s^2-2s+2)}{s^2+2s+5}$$

$$= \frac{s(s+1+j)(s+1-j)}{(s-1+j)(s-1-j)} \cdot \frac{s(s-1+j)(s-1-j)}{s(s-1+j)(s-1-j)}$$

b) $S_P(S) \boxed{G(S)} S_W(S) = 1$

$S_P(S) G(S) G(-S) = S_W(S) = 1$

$\Rightarrow G(S) G(-S) = \frac{(s+1-j2)(s+1+j2)}{s(s+1+j)(s+1-j)} \cdot \frac{(s-1-j2)(s-1+j2)}{s(s-1+j)(s-1-j)}$

FOR REALIZABLE $G(S)$ AND $[G(S)]^{-1}$

$G(S) = \frac{(s+1-j2)(s+1+j2)}{s(s+1+j)(s+1-j)} = \frac{s^2+2s+5}{s(s^2+2s+2)}$

SINCE POLES ARE IN LEFT HALF OF S PLANE

$s \Rightarrow j2\pi f$

$= -4\pi^2 f^2 + j4\pi f + 5$

$\therefore G(f) = j2\pi f \frac{(s^2+2s+5)}{s^2+2s+5} = \frac{B5+C}{s^2+2s+5}$

$\frac{B5+C}{s^2+2s+5} = \frac{A}{s} + \frac{Bs+C}{s^2+2s+2}$

$s^2+2s+5 = A(s^2+2s+2) + (Bs+C)s$

$5=0 \Rightarrow 5=2A \Rightarrow A=5/2$

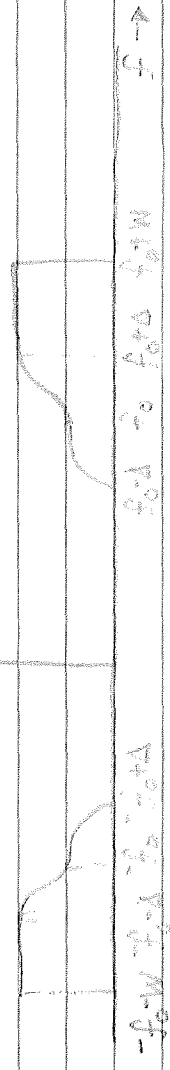
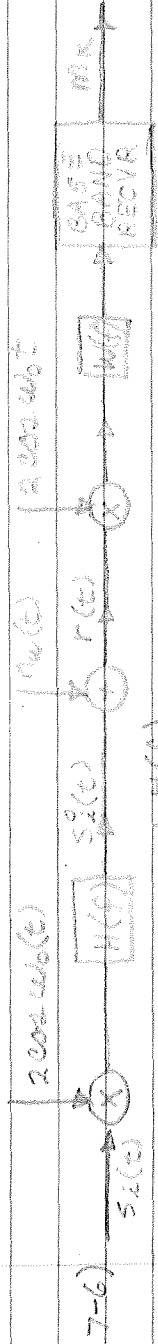
$\therefore \frac{3}{2}s^2 - 3s = (Bs+C)s$

$-\frac{3}{2}s - 3 = Bs+C \Rightarrow B = -\frac{3}{2}; C = -3$

$G(S) = \frac{5/2}{s} - \frac{3/2 s + 3}{s^2 + 2s + 2} = \frac{5/2}{s} - \frac{3}{2} \frac{(s+1)}{s^2 + 2s + 2}$

$= \frac{5/2}{s} - \frac{3}{2} \frac{(s+1)}{(s+1)^2 + 1}$

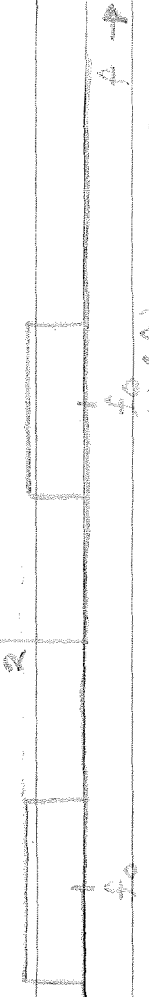
$\therefore g(t) = \left(\frac{5}{2} - \frac{3}{2} e^{-t} \cos t\right) \mu(t)$



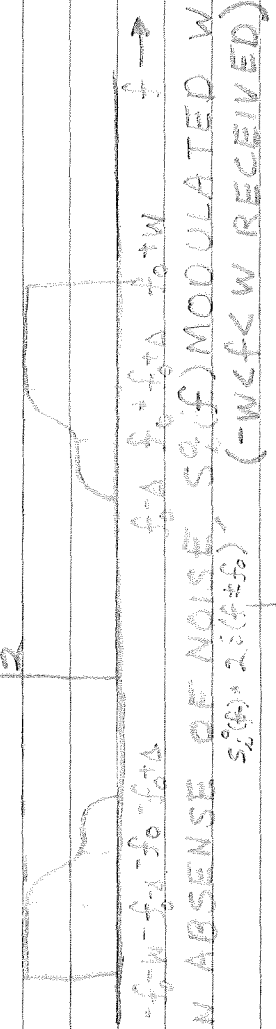
FOR ANALYSIS, LET $S_1(f) = W(f)$



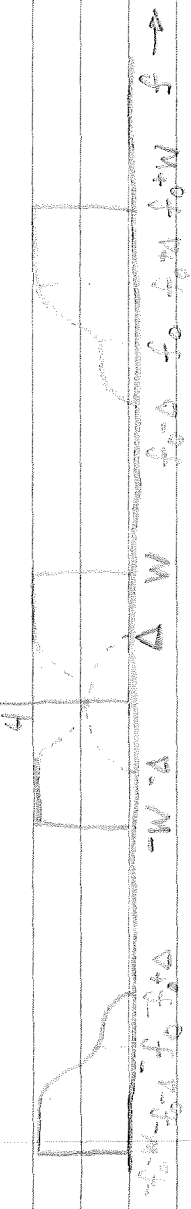
AFTER MODULATION WITH 2 cos 2πf0t
 $S_1(f) * 2δ(f ± f0)$



AFTER PASSING THRU $H(f)$ FILTER
 $S_1(f) = [S_1(f) * 2δ(f ± f0)] H(f) = H(f)$

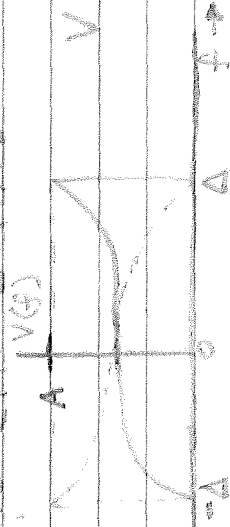


IN ABSENCE OF NOISE, $S_1(f)$ MODULATED WITH 2 cos 2πf0t
 $S_1(f) * 2δ(f ± f0)$ (-W ≤ f ≤ W RECEIVED)



IT IS CLEAR THAT IN ORDER FOR THE RECEIVER TO OBTAIN THE AMPLIFIED VERSION OF THE TRANSMITTED SIGNAL, THE GAIN OVER THE $-Δ < f < Δ$ INTERVAL IN THE RECEIVED SIGNAL (CONT.)

BE EQUAL TO THE CONSTANT GAIN OVER THE INTERVALS $|A| < f < |A|$, IN THIS CASE, $f < A$. THEREFORE, THE INTERVAL $-A < f < A$ FOR VESTIGIAL SIDEBAND MUST FOLLOW THE FOLLOWING CRITERIA:



$$V(f) + V(-f) = A; \quad f < |A|$$

IN THAT, UNDER THESE CONDITIONS, THE RECEIVED SIGNAL IS EQUIVALENT TO THAT OF A SIMILAR SIGNAL TRANSMITTED OVER SSB OR DSB-SC, IT CAN BE ASSUMED THAT THE PROBABILITY OF ERROR IS ALSO EQUIVALENT.

$$\frac{28}{30}$$

4

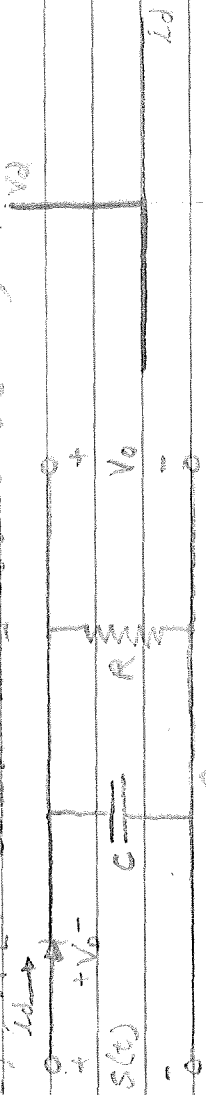
0

0

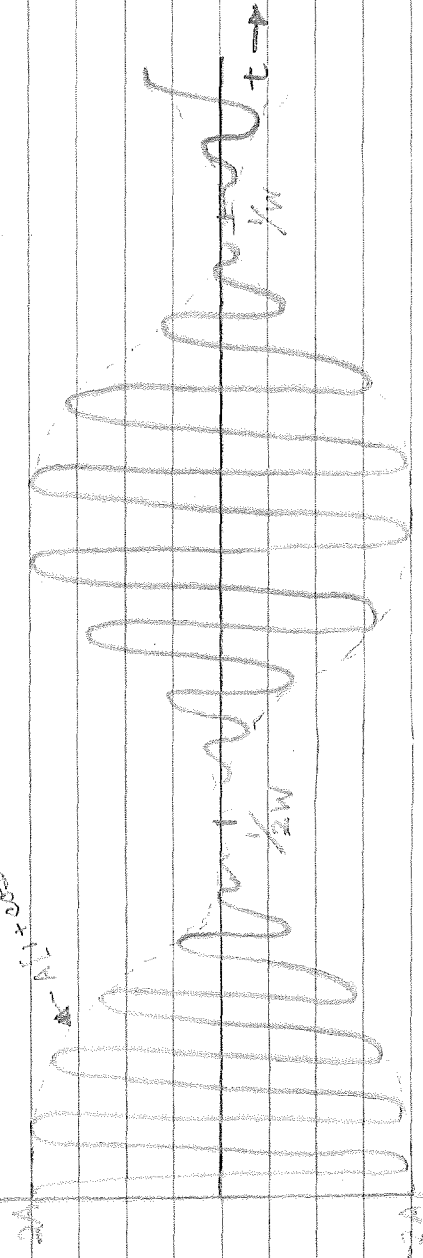
0

0

8-6) $s(t) = A [1 + \cos 2\pi f_0 t] \cos 2\pi f_c t$; $f_c \gg W$

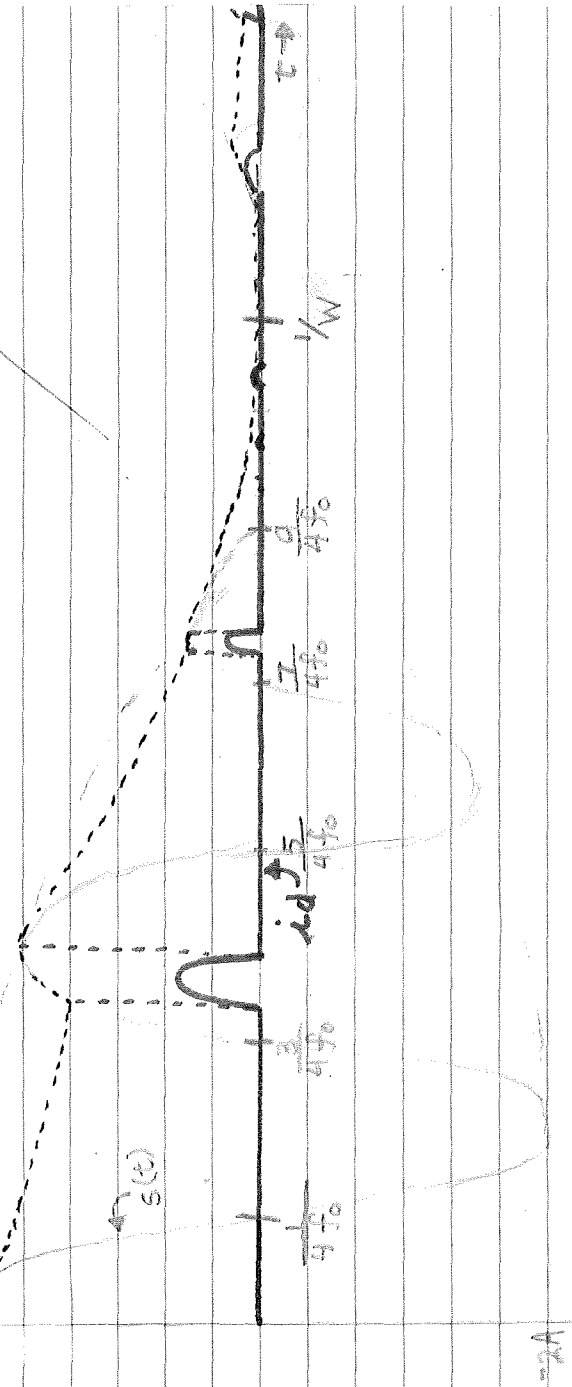


$s(t) = A [1 + \cos 2\pi f_0 t]$



V_h, V_0 (EXPONENTIAL)

$A [1 + \cos 2\pi f_0 t]$



b) WISH TO CHOOSE $\gamma_{\max} = RC \omega$ THE TWO
RELATIVE MAXIMA WHOSE DISTANCE FROM
EACH OTHER IS MAXIMUM WILL BE
CONNECTED IN SUCH A MANNER BY THE
VOLTAGE FROM THE DRAINING
CAPACITOR AS TO PRODUCE NO
RIIDE CURRENT. IF $\gamma > \gamma_{\max}$, CERTAIN
RELATIVE MAXIMA OF THE CARRIER
WILL BE MISSED. IF $\gamma < \gamma_{\max}$, ALL
RELATIVE MAXIMA WILL BE UNNECESSARILY
"UNDERSHOT," CLEARLY, BOTH OF THESE
CONDITIONS YIELD A LOSS OF
OPTIMALITY.

IN THAT $f_0 \gg W$, LINEAR ANALYSIS
CLOSELY APPROXIMATES THE EXPONENTIAL
DECAY.

MAXIMUM DISTANCE BETWEEN RELATIVE
MAXIMA OCCURS WHEN THE SLOPE OF
THE ENVELOPE IS MAX, OR

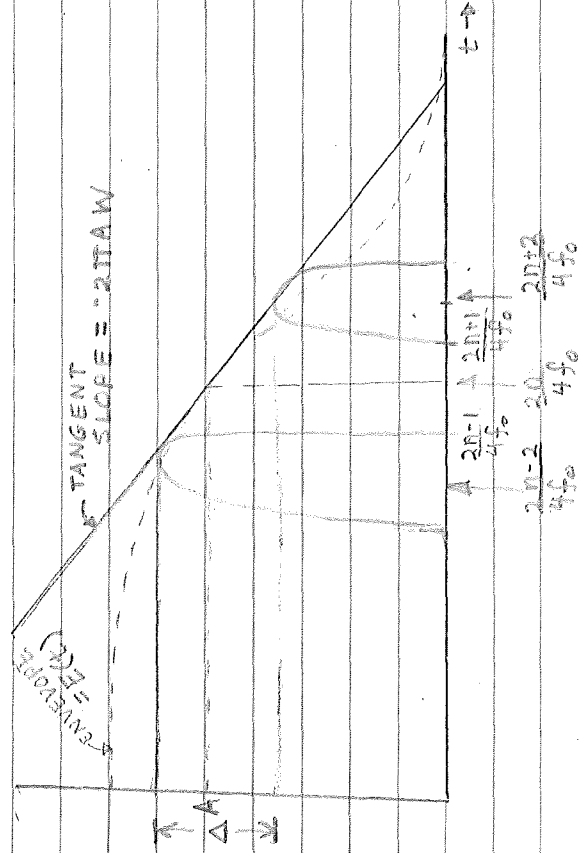
$$\frac{d}{dt} [A + A \cos 2\pi W t] = -A 4\pi^2 W^2 \cos 2\pi W t = 0$$

OR $t = \frac{1}{2} W$

SLOPE OF ENVELOPE AT $\frac{1}{2} W$:

$$\frac{d}{dt} [A + A \cos 2\pi W t]_{t=\frac{1}{2}W} = -A 2\pi W$$

AGAIN, BECAUSE $f_0 \gg W$, ENVELOPE
MAY BE REPRESENTED BY TANGENT
AT POINT OF INTEREST. FURTHERMORE,
CARRIER MAY BE PLACED AT
CONVENIENCE, FOR SAME REASON



$$\frac{3\pi}{4} \frac{1}{f_0} = \frac{1}{2\omega} \Rightarrow \omega = \frac{f_0}{2}$$

$$\Delta = E \left[\frac{20-1}{2f_0} \right] - E \left[\frac{20+1}{2f_0} \right]$$

$$E(t) \approx -2\pi A \omega t + C$$

$$E(t) = A \Leftrightarrow t = \frac{1}{2\omega}$$

$$A \approx -\pi A + C \Rightarrow C = A + \pi A = A(1 + \pi)$$

$$\therefore E(t) \approx -2\pi A \omega t + A(1 + \pi)$$

$$\Rightarrow \Delta = \left| 2\pi A \omega \left(\frac{20-1}{2f_0} \right) - 2\pi A \omega \left(\frac{20+1}{2f_0} \right) \right|$$

$$= 2\pi A \frac{\omega}{f_0}$$

\therefore THE EXPONENTIAL SHOULD DROP ABOUT

$\Delta = 2\pi A \frac{\omega}{f_0}$ IN THE TIME INTERVAL $\frac{1}{f_0}$

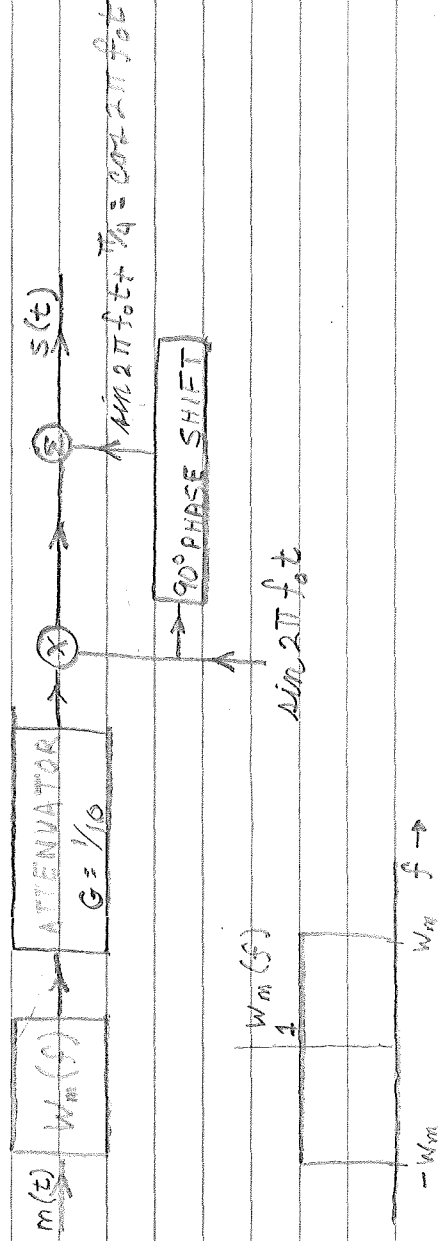
$$E(t) = Ae^{-t/\tau}$$



$$A - 2\pi A \frac{\omega}{f_0} = e^{-\frac{1}{f_0 \tau}} \Rightarrow \frac{1}{f_0 \tau} = \ln \left[A - 2\pi A \frac{\omega}{f_0} \right]$$

$$\text{OR } \tau_{\text{MAX}} = RC \approx \left\{ \frac{1}{f_0} \ln \left[A - 2\pi A \frac{\omega}{f_0} \right] \right\}^{-1} \approx \left[-f_0 \ln A \right]^{-1}$$

8-16)



a) OUTPUT OF ATTENUATOR: $= Gm(t)$

$$\Rightarrow s(t) = Gm(t) \sin 2\pi f_0 t + \cos 2\pi f_0 t$$



$$s(t) = (1 + G^2 m^2(t))^{1/2} \cos(2\pi f_0 t - \phi)$$

FOR $|m(t)| \leq 1$ AND $G < 1/10$; $|Gm(t)| \ll 1$

$$\text{AND } |Gm(t)|^2 \ll 0.01$$

$$\Rightarrow [1 + G^2 m^2(t)]^{1/2} \approx 1$$

$$\therefore s(t) \approx \cos(2\pi f_0 t) - Gm(t) \Rightarrow \phi \approx Gm(t)$$

WHICH IS EQUIVALENT TO PHASE MODULATION:

$$s(t) = A\sqrt{2} \cos 2\pi [f_0 t + W_2 m(t)] \quad (\text{pg 659})$$

WITH $-W_2 = G < 1/10$; $A = 1/\sqrt{2}$

$$b) S_m(t)_{FM} = A\sqrt{2} \cos 2\pi [f_0 t + W \int m(t) dt] \quad (\text{Pg 659})$$

$$S_m(t)_{PM} = A\sqrt{2} \cos 2\pi [f_0 t + W_m m(t)]$$

ASSUME SINUSOIDAL SIGNAL: $m(t) = \cos 2\pi W_m t$

$$S_m(t)_{FM} = A\sqrt{2} \cos 2\pi [f_0 t + \beta_{FM} \cos 2\pi W_m t]$$

$$S_m(t)_{PM} = A\sqrt{2} \cos 2\pi [f_0 t + \beta_{PM} \cos 2\pi W_m t]$$

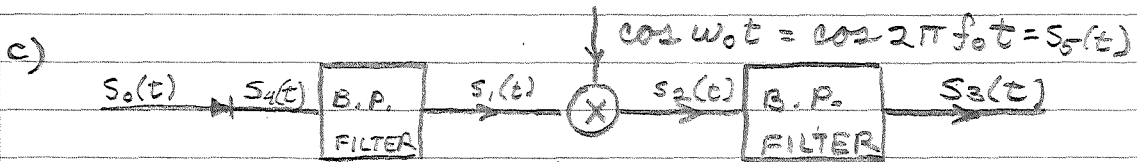
$$\beta_{FM} = W_i / W_m \quad \beta_{PM} = 2\pi W_m \quad (\text{SAMPLING FREQUENCY})$$

$$S(t) \equiv \frac{m(t) G \sin 2\pi f_0 t + \cos 2\pi f_0 t}{\sqrt{1 + G^2 m^2(t)}}$$

$$= \sqrt{1 + G^2 m^2(t)} \cos(2\pi f_0 t - \phi) \quad \phi = \tan^{-1} G m(t)$$

$$\approx \cos(2\pi f_0 t - G m(t))$$

$$\text{FOR } S(t), \beta = G = 1/10$$



$$S_0(t) = \cos 2\pi (f_0 t + \phi) \quad \phi = G m(t)$$

$$= \cos [2\pi f_0 t + \beta_0 m(t)]$$

$$S_4(t) = S_0^2(t)$$

$$= \cos^2 [2\pi f_0 t + \beta_0 m(t)]$$

$$= \frac{1}{2} + \frac{1}{2} \cos [2\omega_0 t + 2\beta_0 m(t)] \quad \omega_0 = 2\pi f_0$$

B.P. FILTER FILTERS OUT D.C. IN $S_4(t)$

$$\Rightarrow S_1(t) = \frac{1}{2} \cos [2\omega_0 t + 2\beta_0 m(t)]$$

$$S_2(t) = S_1(t) S_5(t)$$

$$= \frac{1}{2} \cos [2\omega_0 t + 2\beta_0 m(t)] (\cos \omega_0 t)$$

$$= \frac{1}{4} \cos (3\omega_0 t + 2\beta_0 m(t)) + \frac{1}{4} \cos (\omega_0 t + 2\beta_0 m(t))$$

SECOND B.P. FILTER, CENTERED AT $f_0 (= \frac{\omega_0}{2\pi})$ FILTERS

OUT HIGHER FREQ. COMPONENT $\cos (3\omega_0 t + 2\beta_0 m(t))$

$$\Rightarrow S_3(t) = \frac{1}{4} \cos (\omega_0 t + 2\beta_0 m(t))$$

$$\equiv \frac{1}{4} \cos (\omega_0 t + \beta_1 m(t))$$

$$\therefore \beta_1 = 2\beta_0$$

d) IF $S(t)$ IS PASSED THRU A SECOND STAGE:

$$B_2 = 2B_1 = 2(2B_0) = 2^2 B_0$$

IF $S(t)$ IS PASSED THRU K STAGES

$$B_K = 2 B_{K-1} = 2(2 B_{K-2}) = 2 [2(2 B_{K-3})] = 2^K B_0$$

$$\frac{N_0}{2} = 10^{-11} \text{ Hz}; N^2(t) = 10^{-4}; W_M = 3 \text{ kHz}; P_S = 10^{-6} \text{ W}$$

$$N^2(t) = \frac{1}{(2\pi W_M)^2} \frac{N_0}{2 E_s} = \frac{1}{B_K^2} \frac{N_0}{2 E_s}$$

$$E_s = A^2 / 2 W_M = P_S / 2 W_M \quad P_S = 10^{-6} \text{ W}$$

$$10^{-4} = \frac{1}{B_K^2} \frac{10^{-11} (6 \times 10^3)^2}{10^{-6}} \Rightarrow B_K^2 = 6 \times 10^2$$

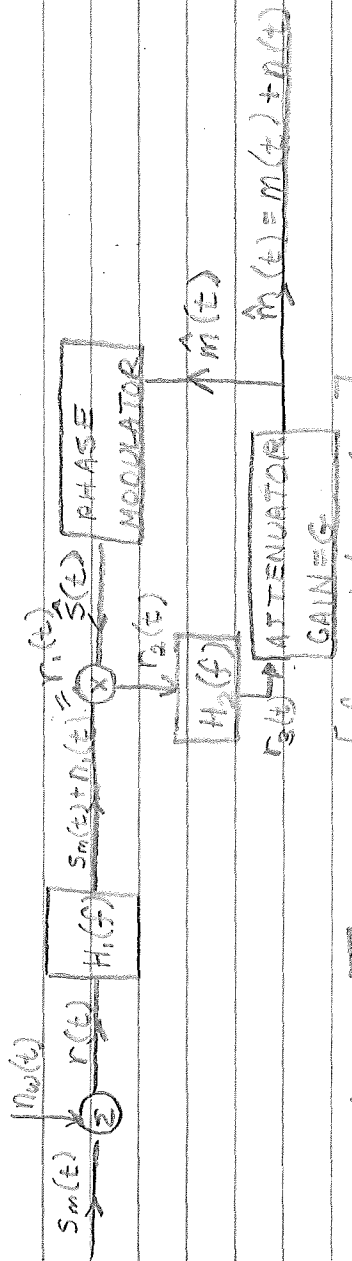
$$\therefore B_K = 24.5 = 2^K B_0$$

$$B_0 = 2\pi f = 2\pi (10) = 628; \frac{1}{B_0} = 1.59$$

$$\Rightarrow K = \frac{\log(B_K/B_0)}{\log 2} = \frac{\log 39}{\log 2} = 3.65 \approx 4$$

~~\therefore AT LEAST 6 STAGES ARE NEEDED~~

8-13)



$$s_m(t) = A\sqrt{2} \cos(2\pi [f_0 t + W_2 m(t)])$$

$$\hat{s}(t) = \sqrt{2} \cos(2\pi [f_0 t + \hat{W} \hat{m}(t)]) \quad , \quad \hat{W} \leq W_2$$

$$r_2 = s_m(t) \hat{s}(t)$$

$$= 2A \cos(2\pi [f_0 t + W_2 m(t)]) \cos(2\pi [f_0 t + \hat{W} \hat{m}(t)])$$

$$\Theta(t) \triangleq 2\pi W_2 m(t)$$

$$\hat{\Theta}(t) \triangleq 2\pi \hat{W} \hat{m}(t)$$

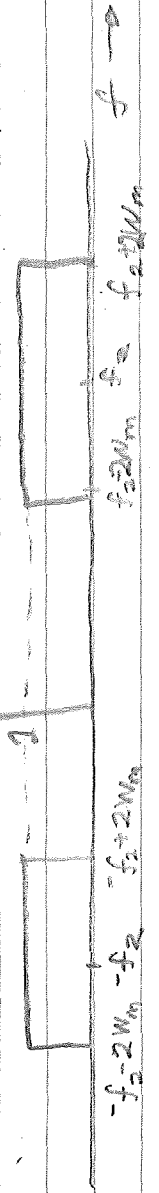
$$W_0 \triangleq 2\pi f_0$$

$$\Rightarrow r_2(t) = A \cos(2W_0 t + \Theta(t) + \hat{\Theta}(t)) + A \cos(2W_0 t + \Theta(t) - \hat{\Theta}(t))$$

$H_2(f)$ SHOULD FILTER OUT CARRIER AND PASS $A \cos[\Theta(t) - \hat{\Theta}(t)] = r_3(t)$

CARRIER TERM, AND PASS $A \cos[\Theta(t) - \hat{\Theta}(t)] = r_3(t)$

$$H_2(f)$$



$$r_3(t) = A \cos[\Theta(t) - \hat{\Theta}(t)]$$

$$\hat{m}(t) = GA \cos[W_2 m(t) - \hat{W} \hat{m}(t)]$$

$$= GA \sin[W_2 m(t) - \hat{W} \hat{m}(t) + \pi/2]$$

$$-1 \ll [W_2 m(t) - \hat{W} \hat{m}(t) + \pi/2] = \psi \ll 1$$

$$\Rightarrow \sin \psi = \psi$$

$$\therefore \hat{m}(t) = GA [W_2 m(t) - \hat{W} \hat{m}(t)]$$

$$\hat{m} (1 + GA \hat{W}) = GA (W_2 m(t) + W_2 \hat{m}(t))$$

$$\text{OR } \hat{m}(t) = \frac{GA W_2}{1 + GA \hat{W}} m(t) + \frac{GA \pi}{2(1 + GA)}$$

PASSING $\hat{m}(t)$ THRU A DIFFERENTIATOR, AND THEN AN INTEGRATOR (WITH 0 INITIAL VALUE) FILTERS OUT CONSTANT $G\pi/2(1+GA)$, YIELDING

$$\hat{m}(t) = \left[GA\omega_2 \frac{1+GA\hat{W}}{1+GA\hat{W}} \right] m(t)$$

SETTING $\hat{m}(t) = m(t)$

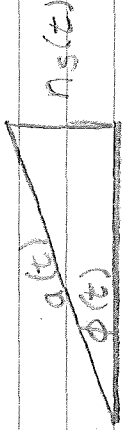
$$\Rightarrow 1 + \hat{W}GA = GA\omega_2 ; GA(\omega_2 - \hat{W}) = 1$$

$$\therefore G = [A(\omega_2 - \hat{W})]^{-1}$$

b) $n_1(t) = n_c(t)\sqrt{2} \cos 2\pi f_0 t + n_s(t)\sqrt{2} \sin 2\pi f_0 t$

FOR ANALYSIS, LET $m(t) = 0$

$$\Rightarrow n_1(t) = [A + n_c(t)]\sqrt{2} \cos \omega_0 t + n_s(t)\sqrt{2} \sin \omega_0 t ; \omega_0 = 2\pi f_0$$



$$A + n_c(t)$$

$$a(t) = \left[n_s^2(t) + (A + n_c(t))^2 \right]^{1/2}$$

$$n_c(t) \ll A \Rightarrow n_s(t) \Rightarrow a(t) \approx A$$

$$\phi(t) = \tan^{-1} n_s(t) / [A + n_c(t)]$$

$$n_c(t) \ll A \Rightarrow n_s(t) \Rightarrow \phi(t) \approx n_s(t) / [A + n_c(t)]$$

$$\Rightarrow n_1(t) = a(t)\sqrt{2} \cos [\omega_0 t + \phi(t)]$$

$$\approx A\sqrt{2} \cos [\omega_0 t - n_s(t) / [A + n_c(t)]]$$

$$n_2(t) = n_1(t) \hat{s}(t)$$

$$= 2a(t) \cos [\omega_0 t + \phi(t)] \cos 2\pi [f_0 t + \hat{W}\hat{m}(t)]$$

$$\hat{\theta}(t) = 2\pi \hat{W}\hat{m}(t)$$

$$\Rightarrow n_2(t) = 2a(t) \cos [\omega_0 t + \phi(t)] \cos [2\pi f_0 t + \hat{\theta}(t)]$$

$$= a(t) [\cos(\omega_0 t + \phi(t) + \hat{\theta}(t)) + \cos(\phi(t) - \hat{\theta}(t))]$$

$H_2(f)$ FILTERS OUT CARRIER COMPONENT $2\omega_0$

$$\Rightarrow n_3(t) = A \cos(\phi(t) - \hat{\theta}(t))$$

$$\therefore n(t) = \hat{m}(t) = GA \cos [\phi(t) - \hat{\theta}(t)] = n_3(t)$$

$$\approx GA \sin [\phi(t) - \hat{\theta}(t) + \pi/2]$$

$$\approx GA [\phi(t) - \hat{\theta}(t) + \pi/2]$$

$$\approx GA [-n_s(t)/A - 2\pi \hat{W}\hat{m}(t) + \pi/2]$$

2 July 1970

Solutions of 2.12, 2.23, 2.24.

$$\begin{aligned} (2.12). \quad (a) \quad & P[a,0] = P[0] P[a|0] = 0.49 \\ & P[b,0] = P[0] P[b|0] = 0.14 \\ & P[c,0] = P[0] P[c|0] = 0.07 \\ & P[a,1] = P[1] P[a|1] = 0.09 \\ & P[b,1] = P[1] P[b|1] = 0.06 \\ & P[c,1] = P[1] P[c|1] = 0.15. \end{aligned}$$

Thus, optimum decision rule:

$$\begin{aligned} \hat{m}(a) &= 0 \\ \hat{m}(b) &= 0 \\ \hat{m}(c) &= 1. \end{aligned}$$

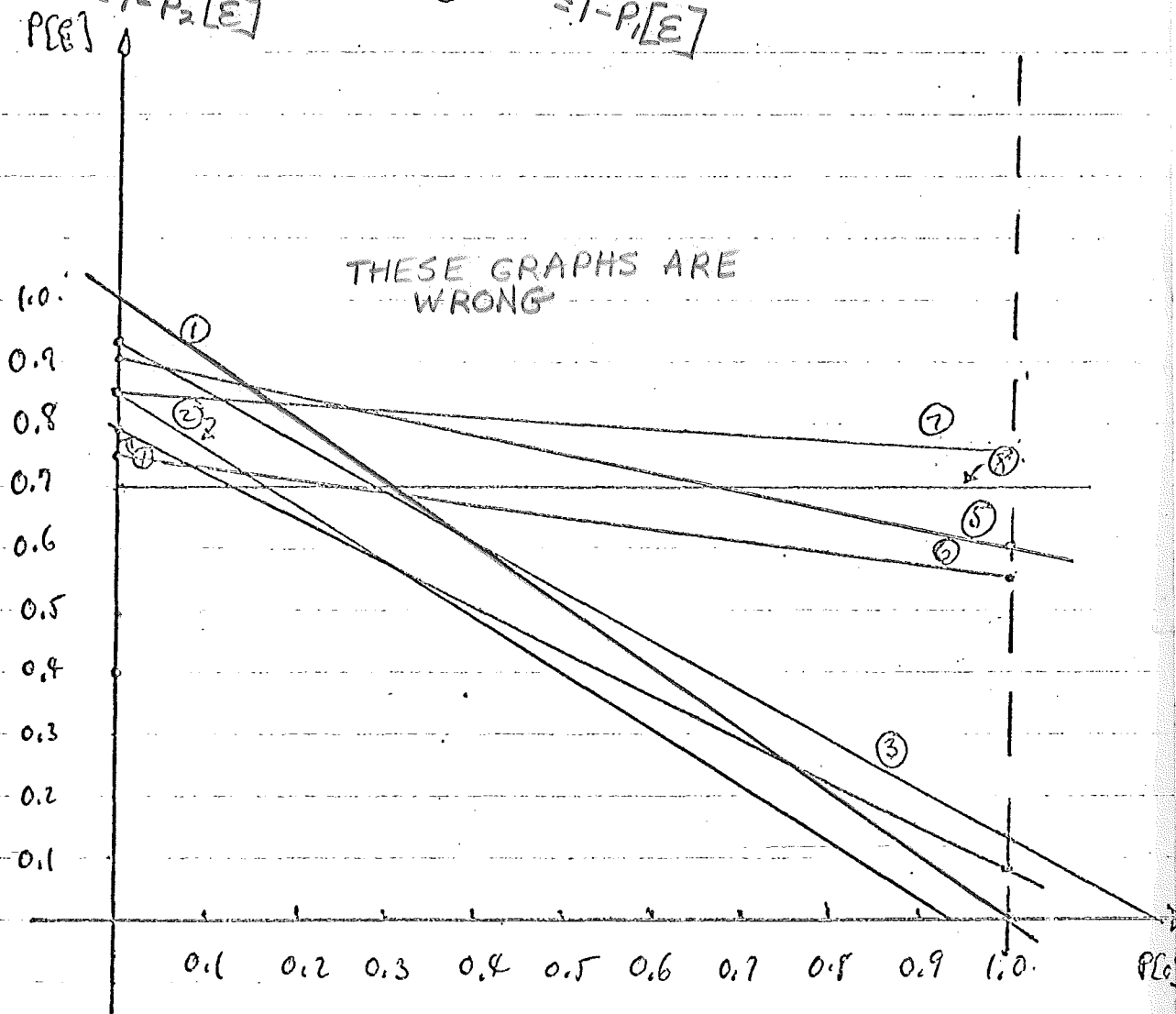
$$\begin{aligned} \text{Prob of error} &= 1 - \text{Prob of correct choice} = 1 - 0.49 - 0.14 - 0.15 \\ &= \boxed{0.22} \end{aligned}$$

(b) Each letter, a, b, c , is associated with a 0 or 1. Hence, we have the following 8 possibilities

$$(a, b, c) = \underset{\textcircled{1}}{(0,0,0)}, \underset{\textcircled{2}}{(0,0,1)}, \underset{\textcircled{3}}{(0,1,0)}, \underset{\textcircled{4}}{(0,1,1)}, \underset{\textcircled{5}}{(1,0,0)}, \underset{\textcircled{6}}{(1,0,1)}, \underset{\textcircled{7}}{(1,1,0)}, \underset{\textcircled{8}}{(1,1,1)}$$

$$\begin{aligned} \text{Now } P[a,0] &= 0.7 P[0], & P[a,1] &= 0.09 = \textcircled{3} [1 - P[0]] \\ P[b,0] &= 0.2 P[0], & P[b,1] &= 0.06 = \textcircled{2} [1 - P[0]] \\ P[c,0] &= 0.1 P[0], & P[c,1] &= 0.15 = \textcircled{5} [1 - P[0]] \end{aligned}$$

$\therefore P_1[E] = P[O], P_2[E] = .9P[O] + .5[1 - P[O]] \Rightarrow .5 + .4P[O] = P_2(E)$
 $P_3[E] = .8P[O] + .06$
 $P_4[E] = .8 - .6P[O]$
 $P_5[E] = .7P[O] + .21$, $P_6[E] = .7 - 1 - P_4[E] = 0.09$
 $P_7[E] = .3P[O] + .09$, $P_8[E] = .2 + .6P[O]$
 $P_9[E] = .2P[O] + .24 = 1 - P_3[E]$
 $P_{10}[E] = .5 + .4P_0$
 $P_{11}[E] = .4P[O] + .15$, $P_{12}[E] = \frac{P[O]}{0.3} = 1 - P_1[E]$



(c) Minimizing decision rule = $\hat{u}(a) = 0, \hat{u}(b) = 1, \hat{u}(c) = 1$.
 All other decision rules have a larger maximum $P[E]$.
 Obviously, the best decision rule is (2) when $P[O] \geq 0.3$.

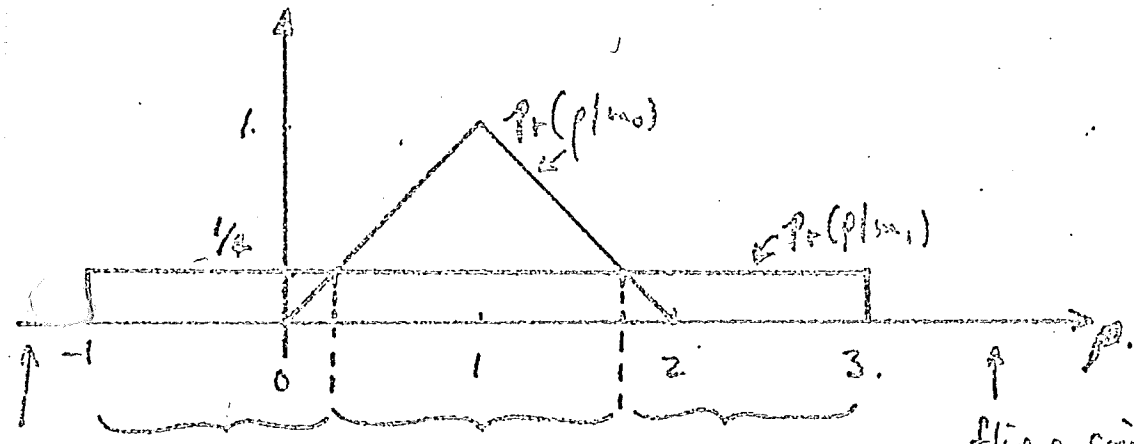
Communication Theory: Problem Set #1 Solutions

(2.23) Decision rule

$$\hat{m}(p) = m_0 \text{ iff } Pr(p/m_0)P[m_0] > Pr(p/m_1)P[m_1]$$

Because $P[m_0] = P[m_1]$ we have the maximum likelihood receiver decision rule

$$\hat{m}(p) = m_0 \text{ iff } Pr(p/m_0) > Pr(p/m_1)$$



Flip a coin out here.
Choose m_1 if p lies here.

Choose m_0 if p falls in here.
Choose m_1 if p lies here

Flip a coin out here
Actually the probability of the received voltage lying here, or less than -1, is zero.

$$P[C|m_0] = \int_{1/4}^{2} Pr(p/m_0) dp = \frac{15}{16}$$

$$P[C|m_1] = \int_{-1}^{1/4} Pr(p/m_1) dp + \int_{2}^{3} Pr(p/m_1) dp = \frac{5}{8}$$

$$P[C] = P[m_0]P[C|m_0] + P[m_1]P[C|m_1] = \frac{25}{32}$$

$$P[E] = 1 - \frac{25}{32} = \frac{7}{32}$$

(2)

(2.29). We must calculate $P\{r'=j | m_i\}$, $i=0,1$
 $j=3,2,1,0,-1,-2$.

$$P\{r'=3 | m_0\} = P\{r > 2.5 | m_0\} = \int_{2.5}^{\infty} p_r(x | m_0) dx = 0$$

$$P\{r'=2 | m_0\} = P\{1.5 < r < 2.5 | m_0\} = \int_{1.5}^{2.5} p_r(x | m_0) dx = 1/8.$$

$$P\{r'=1 | m_0\} = 3/8$$

$$P\{r'=0 | m_0\} = 1/8.$$

$$P\{r'=-1 | m_0\} = 0$$

$$P\{r'=-2 | m_0\} = 0.$$

$$P\{r'=3 | m_1\} = P\{r > 2.5 | m_1\} = \int_{2.5}^{\infty} p_r(x | m_1) dx = 1/8.$$

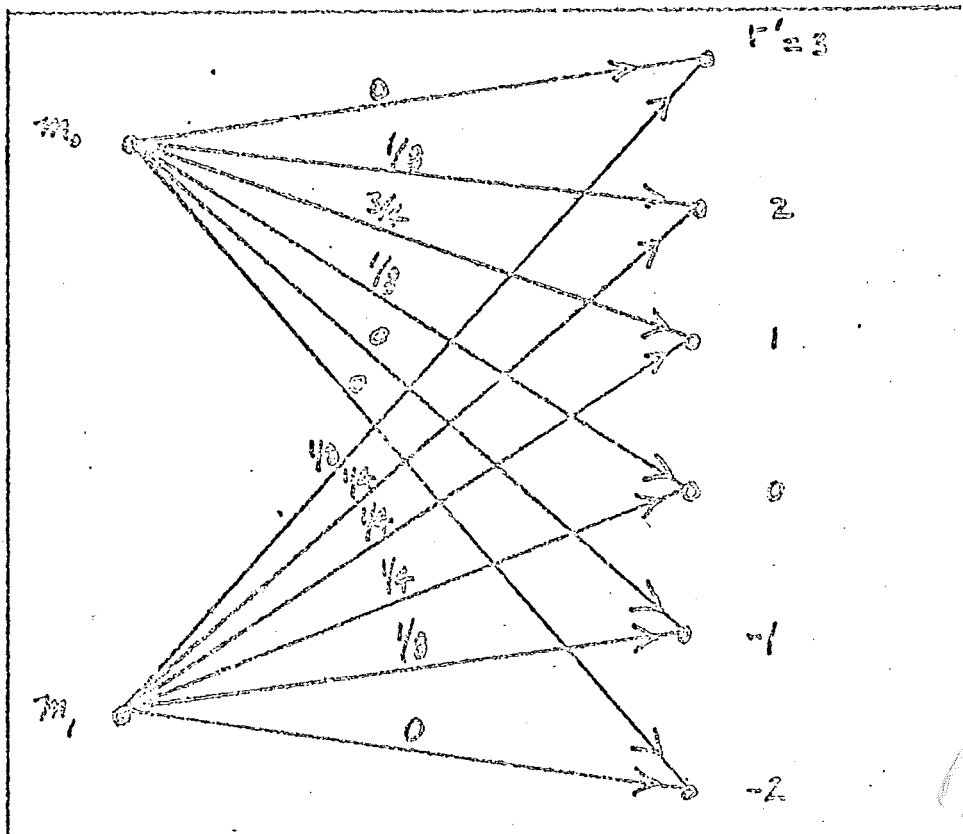
$$P\{r'=2 | m_1\} = 1/8$$

$$P\{r'=1 | m_1\} = 1/8$$

$$P\{r'=0 | m_1\} = 1/8$$

$$P\{r'=-1 | m_1\} = 1/8.$$

$$P\{r'=-2 | m_1\} = 0.$$



Hence, the decision rule becomes

$$\hat{m}(j) = m_i \text{ iff}$$

$$P[m_i] P[r_j | m_i] > P[m_k] P[r_j | m_k] \quad i \neq k.$$

Since $P[m_0] = P[m_1] = 1/2$, we need only consider

$$P[r_j | m_0] \text{ and } P[r_j | m_1].$$

$$\text{Thus } \hat{m}(3) = m_1$$

$$\hat{m}(2) = m_1$$

$$\hat{m}(1) = m_0$$

$$\hat{m}(0) = m_1$$

$$\hat{m}(-1) = m_1$$

$$\hat{m}(-2) = \text{either (actually } -2 \text{ cannot occur)}$$

$$P[C | m_0] = 3/4$$

$$P[C | m_1] = 1/8 + 1/4 + 1/4 + 1/8 = 3/4.$$

$$\therefore P[C] = P[m_0] 3/4 + P[m_1] 3/4 = 3/4.$$

$\therefore P[E] = 1 - 3/4 = 1/4$ which is slightly greater than that in the unquantized system, as to be expected.

Hence, the decision rule becomes

$$\hat{m}(j) = m_i \text{ iff}$$

$$P[m_i] P[r_j | m_i] > P[m_k] P[r_j | m_k] \quad i \neq k.$$

Since $P[m_0] = P[m_1] = 1/2$, we need only consider

$$P[r_j | m_0] \text{ and } P[r_j | m_1].$$

$$\text{Thus } \hat{m}(3) = m_1$$

$$\hat{m}(2) = m_1$$

$$\hat{m}(1) = m_0$$

$$\hat{m}(0) = m_1$$

$$\hat{m}(-1) = m_1$$

$$\hat{m}(-2) = \text{either (actually } -2 \text{ cannot occur)}$$

$$P[C | m_0] = 3/4$$

$$P[C | m_1] = 1/8 + 1/4 + 1/4 + 1/8 = 3/4.$$

$$\therefore P[C] = P[m_0] 3/4 + P[m_1] 3/4 = 3/4.$$

$$\therefore \boxed{P[C] = 1 - 3/4 = 1/4} \text{ which is slightly greater than that}$$

in the unquantized system, as to be expected.

Hence, the decision rule becomes

$$\hat{m}(j) = m_i \text{ iff}$$

$$P[m_i] P[r_j | m_i] > P[m_k] P[r_j | m_k] \quad i \neq k.$$

Since $P[m_0] = P[m_1] = 1/2$, we need only consider

$$P[r_j | m_0] \text{ and } P[r_j | m_1].$$

$$\text{Thus } \hat{m}(3) = m_1$$

$$\hat{m}(2) = m_1$$

$$\hat{m}(1) = m_0$$

$$\hat{m}(0) = m_1$$

$$\hat{m}(-1) = m_1$$

$$\hat{m}(-2) = \text{either (actually } -2 \text{ cannot occur)}$$

$$P[C | m_0] = 3/4$$

$$P[C | m_1] = 1/8 + 1/4 + 1/4 + 1/8 = 3/4.$$

$$\therefore P[C] = P[m_0] 3/4 + P[m_1] 3/4 = 3/4.$$

$$\therefore \boxed{P[E] = 1 - 3/4 = 1/4} \text{ which is slightly greater than that}$$

in the quantized system, as to be expected.

①

Communications Systems EE592
Solutions of 3.4, 3.6, 3.7, 3.8.

11 July, 1970.

(3.4). Since the means of the jointly Gaussian random variables x_1, x_2 , and x_3 are zero, the joint density function p_{x_1, x_2, x_3} is

determined by the covariances

$$\sigma_1^2 = \sigma_2^2 = \sigma_3^2 = R_{11}(0) = 1$$

$$r_{12} = \frac{u_1(0)u_1(1)}{u_1(0)u_1(0)} = R_{11}(1) = 0$$

$$r_{13} = \frac{u_1(0)u_2(0)}{u_1(0)u_2(0)} = R_{12}(0) = 1/2$$

$$r_{23} = \frac{u_1(1)u_2(0)}{u_1(1)u_2(0)} = R_{12}(1) = 0.$$

Thus, x_2 is independent of both x_1 and x_3 . Thus,

$$p_{x_1, x_2, x_3}(\alpha_1, \alpha_2, \alpha_3) = p_{x_2}(\alpha_2) p_{x_1, x_3}(\alpha_1, \alpha_3)$$

$$= \left(\frac{1}{2\pi}\right)^{3/2} e^{-\alpha_2^2/2} \cdot \frac{1}{\sqrt{1-1/4}} \exp\left[-\frac{\alpha_1^2 + \alpha_3^2 - 2r_{13}\alpha_1\alpha_3}{2(1-1/4)}\right]$$

$$= \boxed{\frac{1}{(6\pi^3)^{1/2}} e^{-2/3(\alpha_1^2 + \frac{3}{4}\alpha_2^2 + \alpha_3^2 - \alpha_1\alpha_3)}}$$

(2)

$$3.6. \quad y(t) = x(t) + x(t-T)$$

(a) $x(t-T)$ is Gaussian if $x(t)$ is, hence, $y(t)$ is Gaussian (sum of Gaussian r.v. is Gaussian).

$$\begin{aligned} (b) \quad m_y(t) &= \overline{y(t)} = \overline{x(t) + x(t-T)} = \overline{x(t)} + \overline{x(t-T)} \\ &= \boxed{m_x(t) + m_x(t-T)} \end{aligned}$$

$$\begin{aligned} R_x(t, s) &= E \{ (x(t) - m_x(t)) (x(s) - m_x(s)) \} \\ &= R_x(t, s) - m_x(t) m_x(s). \end{aligned}$$

$$\begin{aligned} R_y(t, s) &= R_y(t, s) - m_y(t) m_y(s) \\ &= E \{ y(t) y(s) \} - m_y(t) m_y(s) \\ &= E \{ x(t) x(s) + x(t-T) x(s) + x(t) x(s-T) + x(t-T) x(s-T) \} \\ &\quad - m_y(t) m_y(s) \end{aligned}$$

$$= \boxed{R_x(t, s) + R_x(t-T, s) + R_x(t, s-T) + R_x(t-T, s-T)}$$

(c) Yes, $y(t)$ is stationary if $x(t)$ is stationary, because then the mean of $y(t)$ is constant and the covariance depends on $t-s=\tau$.

(3.7). (a) $y_i(t) = \int_{-\infty}^{\infty} X(\alpha) h_i(t-\alpha) d\alpha$

$$\begin{aligned} \overline{y_i(t)} &= \int_{-\infty}^{\infty} \overline{X(\alpha)} h_i(t-\alpha) d\alpha \\ &= 0, \quad \forall i. \end{aligned}$$

$$\overline{y_i^2(t)} = R_{y_i}(0)$$

$$R_{y_i}(\tau) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_x(\alpha, \beta) h_i(t+\tau-\alpha) h_i(t-\beta) d\alpha d\beta.$$

(Eq. 3.108).

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{N_0}{2} \delta(\alpha-\beta) h_i(t+\tau-\alpha) h_i(t-\beta) d\alpha d\beta$$

white noise

$$= \frac{N_0}{2} \int_{-\infty}^{\infty} h_i(t+\tau-\beta) h_i(t-\beta) d\beta.$$

(4)

Thus $\overline{y_i^2(t)} = R_{y_i}(0) \stackrel{t=0}{=} \frac{N_0}{2} \int_{-\infty}^{\infty} h_i^2(t-\beta) d\beta.$

$$\therefore \overline{y_1^2(t)} = \frac{N_0}{2} \int_{t-1}^t 1 \cdot d\beta = \frac{N_0}{2}.$$

$$\overline{y_2^2(t)} = \frac{N_0}{2} \int_{-\infty}^t 4 e^{2(\beta-t)} d\beta = N_0$$

$$\overline{y_3^2(t)} = \frac{N_0}{2} \int_{t-2}^t 2 \sin^2 2\pi(\beta-t) d\beta.$$

$$= N_0 \int_{t-2}^t \left(\frac{1}{2} - \frac{1}{2} \cos 4\pi(\beta-t) \right) d\beta.$$

$$= N_0 - \frac{N_0}{8\pi} \sin 4\pi(\beta-t) \Big|_{t-2}^t =$$

$$= N_0$$

(5)

(b) The cross-correlation function $E\{y_i(t) y_j(s)\}$ is given by

$$\begin{aligned} R_{ij}(t, s) &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_x(\alpha, \beta) h_i(t-\alpha) h_j(s-\beta) d\alpha d\beta \\ &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{N_0}{2} \delta(\alpha-\beta) h_i(t-\alpha) h_j(s-\beta) d\alpha d\beta \\ &= \frac{N_0}{2} \int_{-\infty}^{\infty} h_i(t-\beta) h_j(s-\beta) d\beta \end{aligned}$$

Now $R_{ij}(t, t) = \frac{N_0}{2} \int_{-\infty}^{\infty} h_i(t-\beta) h_j(t-\beta) d\beta$

let $\beta = t - \tau$, then

$$R_{ij}(t, t) = \frac{N_0}{2} \int_{-\infty}^{\infty} h_i(\tau) h_j(\tau) d\tau$$

$$R_{13}(t, t) = \frac{N_0}{2} \int_0^1 \sqrt{2} e^{-2\pi\tau} d\tau$$

$= 0 \quad \forall t$. This is the only pair for which this holds for all t .

$$(c) \quad R_{ij}(t, \beta) = \frac{N_0}{2} \int_{-\infty}^{\infty} h_i(\xi) h_j(\beta - \tau) d\xi, \quad \tau = t - \beta.$$

$$= R_{ij}(\tau).$$

The only pair of interest (which could possibly give $R_{ij}(\tau) = 0 \forall \tau$) is $i=1, j=3$, again.

$$\therefore R_{13}(\tau) = \frac{N_0}{2} \int_0^1 \sqrt{2} \sin 2\pi(\xi - \tau) d\xi.$$

$$= \frac{N_0 \cdot \sqrt{2}}{2 \cdot 2\pi} \cos 2\pi(\xi - \tau) \Big|_0^1 =$$

$$= -\frac{N_0}{2\sqrt{2}\pi} [\cos 2\pi(1 - \tau) - \cos 2\pi\tau]$$

$$= \frac{-N_0}{2\sqrt{2}\pi} (\cos 2\pi \cos 2\pi\tau + \sin 2\pi \sin 2\pi\tau - \cos 2\pi\tau)$$

$$= 0 \quad \forall \tau.$$

$$(3.8) \quad y(t) = \int_{-\infty}^{\infty} x(\alpha) h(t - \alpha) d\alpha.$$

$$z(t) = \int_{-\infty}^{\infty} x(\beta) g(t - \beta) d\beta.$$

(a) $m_{y_1} = \int_{-\infty}^{\infty} m_x h(t_1 - \alpha) d\alpha = m_x \int_{-\infty}^{\infty} h(t_1 - \alpha) d\alpha$

$m_{y_2} = m_x \int_{-\infty}^{\infty} g(t_2 - \beta) d\beta$

$\sigma_1^2 = E[(y_1 - m_{y_1})^2] = E[y_1^2] - m_{y_1}^2$

$= E\left[\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x(\alpha) x(\beta) h(t_1 - \alpha) h(t_1 - \beta) d\alpha d\beta\right] - m_{y_1}^2$

$= \iint_{-\infty}^{\infty} R_x(\alpha - \beta) h(t_1 - \alpha) h(t_1 - \beta) d\alpha d\beta - m_{y_1}^2$

$= \iint_{-\infty}^{\infty} (L_x(\alpha - \beta) + m_x^2) h(t_1 - \alpha) h(t_1 - \beta) d\alpha d\beta - m_{y_1}^2$

$= \iint_{-\infty}^{\infty} (L_x(\alpha - \beta) + m_x^2) h(t_1 - \alpha) h(t_1 - \beta) d\alpha d\beta - m_x^2 \left(\int_{-\infty}^{\infty} h(t_1 - \alpha) d\alpha \int_{-\infty}^{\infty} h(t_1 - \beta) d\beta \right)$

$= \iint_{-\infty}^{\infty} L_x(\alpha - \beta) h(t_1 - \alpha) h(t_1 - \beta) d\alpha d\beta$

$\sigma_2^2 = \iint_{-\infty}^{\infty} L_x(\alpha - \beta) g(t_2 - \alpha) g(t_2 - \beta) d\alpha d\beta$

(8)

$$\rho_{12} = \frac{E[y_1 z_2]}{\sigma_1 \sigma_2} - \frac{m_{y_1} m_{z_2}}{\sigma_1 \sigma_2}$$

$$= \frac{1}{\sigma_1 \sigma_2} \left[\iint_{-\infty}^{\infty} h_x(x-\beta) h(t_1-x) g(t_2-\beta) d\alpha d\beta - m_{y_1} m_{z_2} \right]$$

$$= \frac{1}{\sigma_1 \sigma_2} \left[\iint_{-\infty}^{\infty} h_x(x-\beta) h(t_1-x) g(t_2-\beta) d\alpha d\beta \right]$$

Thus $f_{y_1, z_2}(\rho_1, \rho_2) = \frac{1}{2\pi \sigma_1 \sigma_2 (1-\rho_{12}^2)^{1/2}} \times$

$$\times \exp \left\{ -\frac{1}{2(1-\rho_{12}^2)} \left[\frac{(\rho_1 - m_{y_1})^2}{\sigma_1^2} - \frac{2\rho_{12}(\rho_1 - m_{y_1})(\rho_2 - m_{z_2})}{\sigma_1 \sigma_2} \right. \right.$$

$$\left. \left. + \frac{(\rho_2 - m_{z_2})^2}{\sigma_2^2} \right] \right\}. \quad (\text{Eqn. 3.47})$$

with $\rho_{12}, \sigma_1, \sigma_2, m_{y_1}, m_{z_2}$ defined as above (see also 3.44).

(9)

$$(b) \quad y(t) = \int_{-\infty}^{\infty} x(\alpha) h(t-\alpha) d\alpha$$

$$\overline{y(t) x(t-\tau)} = \int_{-\infty}^{\infty} \frac{x(\alpha) x(t-\tau)}{x(\alpha) x(t-\tau)} h(t-\alpha) d\alpha$$

$$= \int_{-\infty}^{\infty} R_x(\alpha - (t-\tau)) h(t-\alpha) d\alpha.$$

If $x(t)$ is white noise, then $R_x(\alpha - (t-\tau)) = \frac{N_0}{2} \delta(\alpha - (t-\tau))$

$$\text{and } \overline{y(t) x(t-\tau)} = \frac{N_0}{2} \int_{-\infty}^{\infty} \delta(\alpha - (t-\tau)) h(t-\alpha) d\alpha$$

$$= \frac{N_0}{2} h(\tau).$$

Thus, the cross-correlation of the output of a linear filter with white noise input yields a means of "identifying the system", i.e., computing the system impulse response.

$$(c) \quad E[y(t_1) z(t_2)] = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_x(\alpha - \beta) h(t_1 - \alpha) g(t_2 - \beta) d\alpha d\beta$$

must ~~also~~ satisfy

$$E[y(t_1) z(t_2)] - \overline{y(t_1)} \overline{z(t_2)} = R_{yz}(t_1, t_2) = 0.$$

$$m_{y_1, m_{z_2}} = m_{x^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(t_1 - \alpha) g(t_2 - \beta) d\alpha d\beta$$

$$\int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_x(\alpha - \beta) h(t_1 - \alpha) g(t_2 - \beta) d\alpha d\beta$$

$$= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_x(\alpha - \beta) h(t_1 - \alpha) g(t_2 - \beta) d\alpha d\beta + m_{x^2} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(t_1 - \alpha) g(t_2 - \beta) d\alpha d\beta$$

$$\therefore \boxed{L_{yz}(t_1, t_2) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} R_x(\alpha - \beta) h(t_1 - \alpha) g(t_2 - \beta) d\alpha d\beta = 0}$$

for statistical independence of $y(t_1), z(t_2), \forall t_1, t_2$.

$$(d). \overline{y^2(t)} = \int_{-\infty}^{\infty} S_y(f) df = \int_{-\infty}^{\infty} S_x(f) |H(f)|^2 df$$

$$S_x(f) = \mathcal{F}\{R_x(\tau)\} = \mathcal{F}\{L_x(\tau)\} \quad (\text{if } m_x = 0)$$

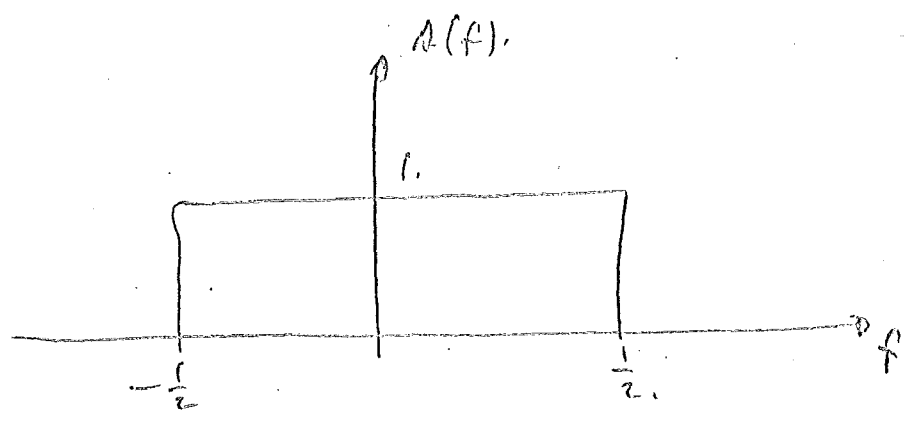
$$= \mathcal{F}\left\{\left(\frac{\sin \pi \tau}{\pi \tau}\right)^2\right\} = \mathcal{F}\left\{\frac{\sin \pi \tau}{\pi \tau}\right\} * \mathcal{F}\left\{\frac{\sin \pi \tau}{\pi \tau}\right\}$$

Convolution in f space.

$$= \int_{-\infty}^{\infty} A(f') A(f-f') df', \quad \text{where } A(f) = \mathcal{F}\left\{\frac{\sin \pi \tau}{\pi \tau}\right\}$$

What is $A(f)$?

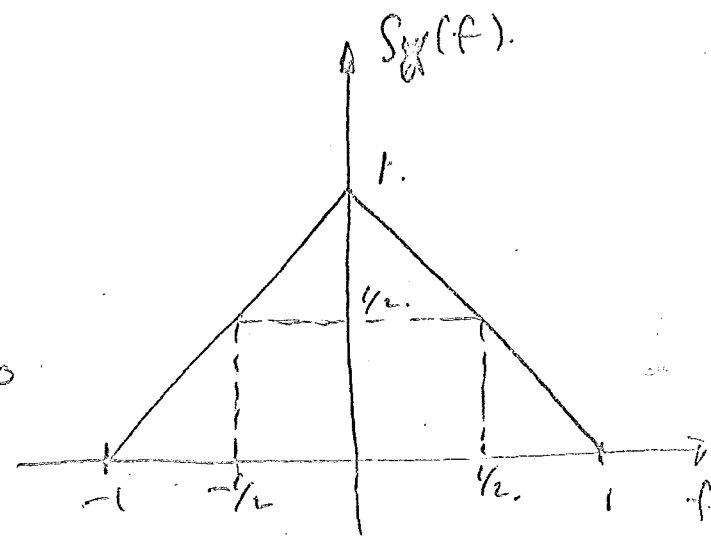
$$A(f) = \int_{-\infty}^{\infty} e^{-j2\pi ft} \frac{1 - \pi t}{\pi t} dt = \begin{cases} 1, & -\frac{1}{2} \leq f \leq \frac{1}{2} \\ 0, & \text{elsewhere} \end{cases}$$



$$Theo S_x(f) = \int_{-\infty}^{\infty} A(f') A(f-f') df' = \int_{-\frac{1}{2}}^{\frac{1}{2}} A(f-f') df'$$

$$= \int_{f-\frac{1}{2}}^{f+\frac{1}{2}} A(s) ds \quad (\text{for } s = f-f')$$

$$\begin{aligned} &= 0, & f < -\frac{1}{2} \\ &= f+1, & -\frac{1}{2} < f < 0 \\ &= 1-f, & 0 < f < \frac{1}{2} \\ &= 0, & f > \frac{1}{2} \end{aligned}$$



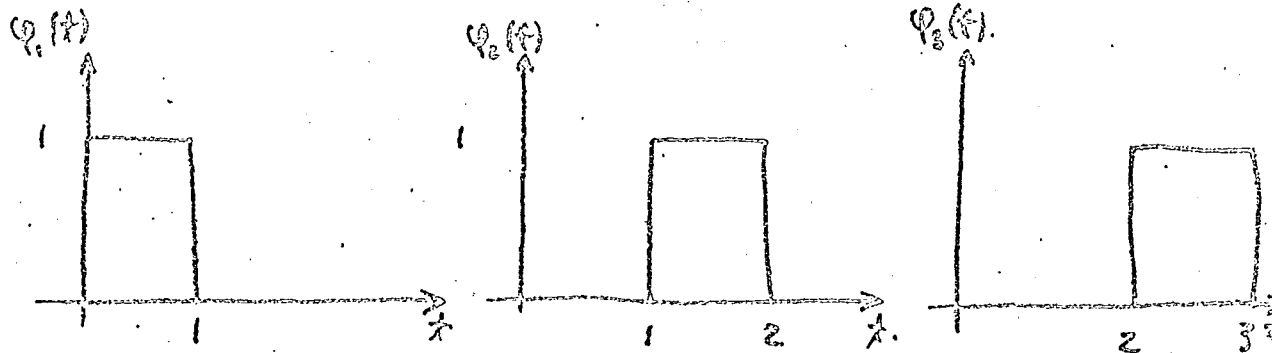
(12)

$$\therefore \overline{y^2(t)} = \int_{-\infty}^{\infty} S_{xx}(f) |H(f)|^2 df = \int_{-1}^{-1/2} S_{xx}(f) df + \int_{1/2}^1 S_{xx}(f) df.$$

$$= \boxed{\frac{1}{4}}$$

Common Theory Solutions to Prof. Set # 3.

(1) (4.9).



clearly: $S_1(t) = \varphi_1(t) \Rightarrow \bar{S}_1 = [1, 0, 0]$.

$$S_2(t) = \varphi_2(t) \Rightarrow \bar{S}_2 = [0, 1, 0]$$

$$S_3(t) = \varphi_1(t) + \varphi_2(t) \Rightarrow \bar{S}_3 = [1, 1, 0]$$

$$S_4(t) = \varphi_3(t) \Rightarrow \bar{S}_4 = [0, 0, 1]$$

$$S_5(t) = \varphi_1(t) + \varphi_3(t) \Rightarrow \bar{S}_5 = [1, 0, 1]$$

$$S_6(t) = \varphi_2(t) + \varphi_3(t) \Rightarrow \bar{S}_6 = [0, 1, 1]$$

$$S_7(t) = \varphi_1(t) + \varphi_2(t) + \varphi_3(t) \Rightarrow \bar{S}_7 = [1, 1, 1]$$

$$S_8(t) = 0 \Rightarrow \bar{S}_8 = [0, 0, 0]$$

$\int_{-\infty}^{\infty} \varphi_i(t) \varphi_j(t) dt = \delta_{ij}$. Incidentally, note the similarity to three-place binary numbers.

$$\bar{n} = [n_1, n_2, n_3]$$

$$n_1 = \int_{-\infty}^{\infty} n_{10}(t) \varphi_1(t) dt, \quad n_2 = \int_{-\infty}^{\infty} n_{20}(t) \varphi_2(t) dt, \quad n_3 = \int_{-\infty}^{\infty} n_{30}(t) \varphi_3(t) dt.$$

$\bar{n}_1 = \bar{n}_2 = \bar{n}_3 = 0$. Because $\varphi_1(t), \varphi_2(t), \varphi_3(t)$ are orthogonal we know from our treatment of prob. (4.7) that $n_1, n_2,$ and n_3 are statistically independent r.v.'s and that $f_{\bar{n}}(n_1, n_2, n_3) = \frac{1}{(2\pi \frac{n_0}{2})^{3/2}} e^{-\frac{(n_1^2 + n_2^2 + n_3^2)}{n_0}}$.

(2)

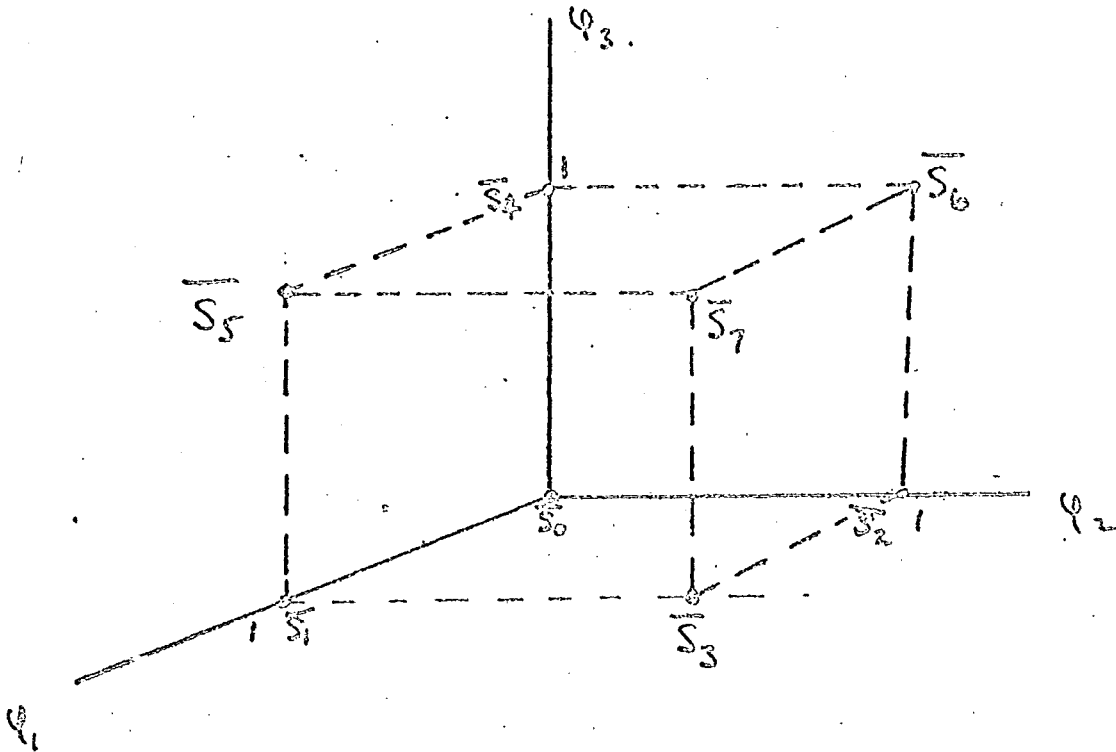
Because the messages are equally likely, our decision function is $P_F(\bar{p} | \bar{s} = \bar{s}_i) = p_u(\bar{p} - \bar{s}_i)$. Thus

$\hat{m}_i(\bar{p}) = m_i$ iff $p_u(\bar{p} - \bar{s}_i) > p_u(\bar{p} - \bar{s}_j)$.
Our i^{th} decision interval is

$$I_i: \text{ set of } \bar{p} \ni p_u(\bar{p} - \bar{s}_i) > p_u(\bar{p} - \bar{s}_j).$$

$$P[C | m_i] = \int_{I_i} p_u(\bar{p} - \bar{s}_i) d\bar{p}$$

$$P[\mathcal{E}] = 1 - P[C] = 1 - \frac{1}{8} \sum_i \int_{I_i} p_u(\bar{p} - \bar{s}_i) d\bar{p}.$$



The boundaries of the decision regions are the perpendicular bisectors of the lines connecting the various lattice points $(\bar{s}_0, \dots, \bar{s}_7)$.

(3)

$$I_0 = -\infty < p_1 \leq 1/2, \quad -\infty < p_2 \leq 1/2, \quad -\infty < p_3 \leq 1/2.$$

$$I_1 = 1/2 \leq p_1 < \infty, \quad -\infty < p_2 \leq 1/2, \quad -\infty < p_3 \leq 1/2.$$

$$I_2 = -\infty < p_1 \leq 1/2, \quad \cancel{-\infty < p_2 \leq 1/2}, \quad -\infty < p_3 \leq 1/2.$$

$$1/2 \leq p_2 < \infty$$

$$I_3 = 1/2 \leq p_1 < \infty, \quad 1/2 \leq p_2 < \infty, \quad -\infty < p_3 \leq 1/2.$$

$$I_4 = -\infty < p_1 \leq 1/2, \quad -\infty < p_2 \leq 1/2, \quad 1/2 \leq p_3 < \infty.$$

$$I_5 = 1/2 \leq p_1 < \infty, \quad -\infty < p_2 \leq 1/2, \quad 1/2 \leq p_3 < \infty.$$

$$I_6 = \cancel{1/2 \leq p_1 < \infty}, \quad 1/2 \leq p_2 < \infty, \quad 1/2 \leq p_3 < \infty.$$

$$-\infty < p_1 \leq 1/2.$$

$$I_7 = 1/2 \leq p_1 < \infty, \quad 1/2 \leq p_2 < \infty, \quad 1/2 \leq p_3 < \infty.$$

$$\int_{I_0} p_{\bar{n}}(\bar{p} - \bar{s}_0) = \frac{1}{(\pi N_0)^{3/2}} \int_{-\infty}^{1/2} e^{-[p_1^2 + p_2^2 + p_3^2]/N_0} dp_1 \int_{-\infty}^{1/2} dp_2 \int_{-\infty}^{1/2} dp_3.$$

$$= \left[\left(\frac{1}{\pi N_0} \right)^{1/2} \int_{-\infty}^{1/2} e^{-p^2/N_0} dp \right]^3 = \left[1 - Q\left(\frac{1}{\sqrt{2N_0}} \right) \right]^3 = Q^3 \left[\frac{-1}{\sqrt{2N_0}} \right]$$

$$\int_{I_1} p_{\bar{n}}(\bar{p} - \bar{s}_1) = \left(\frac{1}{\pi N_0} \right)^{3/2} \int_{1/2}^{\infty} e^{-(p_1-1)^2/N_0} dp_1 \int_{-\infty}^{1/2} e^{-p_2^2/N_0} dp_2 \int_{-\infty}^{1/2} e^{-p_3^2/N_0} dp_3.$$

$$= Q^3 \left[\frac{-1}{\sqrt{2N_0}} \right].$$

$$\int_{I_7} p_{\bar{n}}(\bar{p} - \bar{s}_7) = \left(\frac{1}{\pi N_0} \right)^{3/2} \int_{1/2}^{\infty} e^{-(p_1-1)^2/N_0} dp_1 \int_{1/2}^{\infty} e^{-(p_2-1)^2/N_0} dp_2 \int_{1/2}^{\infty} e^{-(p_3-1)^2/N_0} dp_3.$$

$$= Q^3 \left[\frac{-1}{\sqrt{2N_0}} \right].$$

$$P[E] = 1 - \frac{1}{8} \cdot 8 \cdot Q^3 \left[\frac{1}{\sqrt{2}K_0} \right] = 1 - Q^3 \left[\frac{1}{\sqrt{2}K_0} \right]$$

$$= 1 - \left[1 - Q \left(\frac{1}{\sqrt{2}K_0} \right) \right]^3$$

(2). (4, 13). If $w = w_0$, then $v(t) = \alpha_1 S_0(t - \tau_1) + u_1(t)$
 (a) $+ \alpha_2 S_0(t - \tau_2) + u_2(t)$
 $+ \alpha_3 S_0(t - \tau_3) + u_3(t)$.

If $w = w_1$, then $v(t) = -\alpha_1 S_0(t - \tau_1) + u_1(t)$
 $- \alpha_2 S_0(t - \tau_2) + u_2(t)$
 $- \alpha_3 S_0(t - \tau_3) + u_3(t)$.

Let $S_a(t) \equiv \alpha_1 S_0(t - \tau_1) + \alpha_2 S_0(t - \tau_2) + \alpha_3 S_0(t - \tau_3)$
 $- S_a(t) = -(\alpha_1 S_0(t - \tau_1) + \alpha_2 S_0(t - \tau_2) + \alpha_3 S_0(t - \tau_3))$.

We would sketch these two functions but the results are not worth it.

Define $\|S_a(t)\| \equiv \int_{-\infty}^{\infty} S_a^2(t) dt$. Then the G-S orthogonalization

process gives us $\varphi(t) = \frac{S_a(t)}{\|S_a(t)\|} \equiv \frac{S_a(t)}{A}$. Hence, the one-dimensional

vector representation is:
 $w_0 \iff S_a(t) \iff S_0 = A$
 $w_1 \iff -S_a(t) \iff S_1 = -A$.

$$n = \int_{-\infty}^{\infty} \varphi(t) [u_1(t) + u_2(t) + u_3(t)] dt = \int_{-\infty}^{\infty} \varphi(t) u_1(t) dt + \int_{-\infty}^{\infty} \varphi(t) u_2(t) dt + \int_{-\infty}^{\infty} \varphi(t) u_3(t) dt$$

$= u_1 + u_2 + u_3$. u_1, u_2, u_3 are Gaussian r.v.'s. with mean 0 and

variance: $\overline{u_1^2} = 0.002$, $\overline{u_2^2} = 0.006$, $\overline{u_3^2} = 0.004$. n , being the sum of Gaussian r.v.'s is also Gaussian. $\overline{n} = \overline{u_1} + \overline{u_2} + \overline{u_3} = 0$.

$$\overline{n^2} = \overline{u_1^2} + \overline{u_2^2} + \overline{u_3^2} + 2\overline{u_1 u_2} + 2\overline{u_1 u_3} + 2\overline{u_2 u_3} = \overline{u_1^2} + \overline{u_2^2} + \overline{u_3^2} = 0.012$$

because u_1, u_2, u_3 and $u_2, u_3 = 0$ (independent r.v.'s).

$$p_u(r) = \frac{1}{\sqrt{2\pi(0.012)}} e^{-r^2/2(0.012)}$$

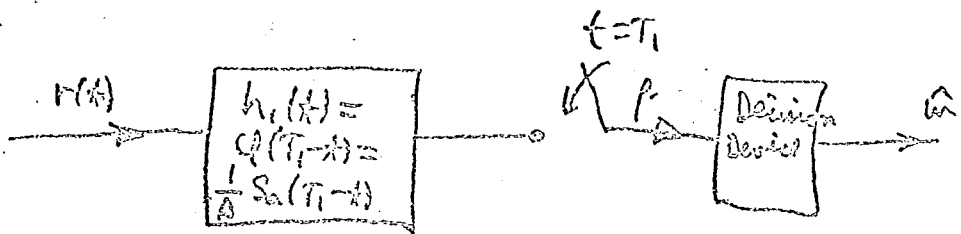
$$r = \int_{-\infty}^{\infty} r(t) \varphi(t) dt, \quad S_0 = \int_{-\infty}^{\infty} S_a(t) \varphi(t) dt, \quad S_1 = \int_{-\infty}^{\infty} -S_a(t) \varphi(t) dt$$

$\therefore r = S_0 + n$. Because the messages are equally likely the decision function becomes $p_r(p | S = S_i) = p_u(p - S_i)$.

$$\text{Thus, } \hat{m}(p) = m_0 \text{ iff } \frac{1}{\sqrt{2\pi(0.012)}} e^{-(p-A)^2/2(0.012)} > \frac{1}{\sqrt{2\pi(0.012)}} e^{-(p+A)^2/2(0.012)}$$

$$\text{Thus, } \hat{m}(p) = m_0 \text{ iff } p > 0 \\ \hat{m}(p) = m_1 \text{ iff } p < 0.$$

But p is a particular value of $\int_{-\infty}^{\infty} r(t) \varphi(t) dt = \int_{-\infty}^{\infty} r(t) \varphi(T_1 - t) dt$ where $t = T_1$.



The decision device simply determines the sign of p and sets $\hat{m}(p) = m_0$ iff $p > 0$ $\hat{m}(p) = m_1$ iff $p < 0$.

$$T_1 = \frac{5}{7.5} \cdot 10^{-3} \text{ sec.}$$

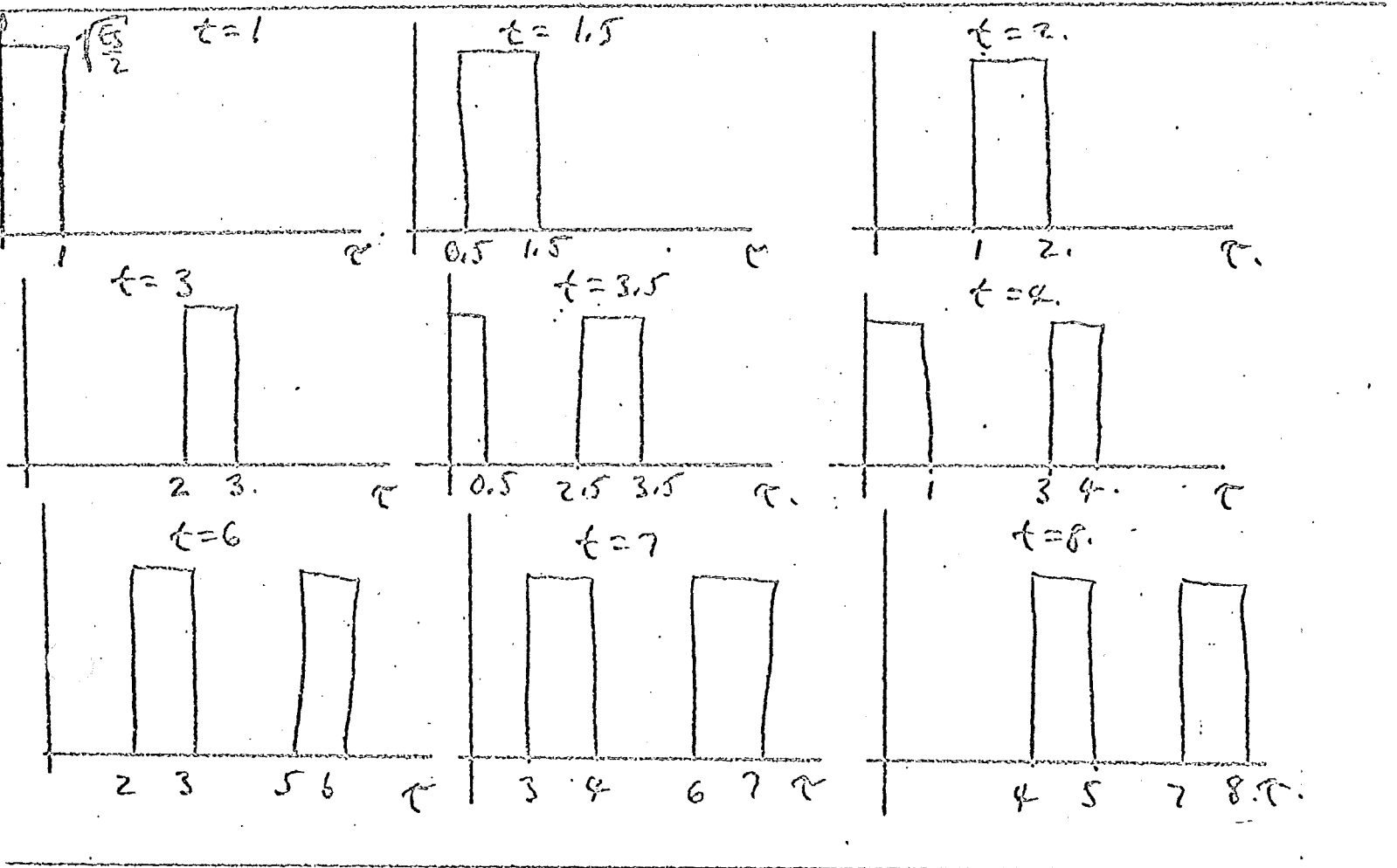
$$P[E] = 1 - \frac{1}{2} \int \frac{1}{\sqrt{2\pi(0.012)}} e^{-(p-A)^2/2(0.012)} dp = 1 - Q\left(\frac{-A}{\sqrt{0.012}}\right)$$

$A \equiv \|S_a(t)\| = \int_{-\infty}^{\infty} S_a^2(t) dt$ may be determined easily and $P[E]$ computed.

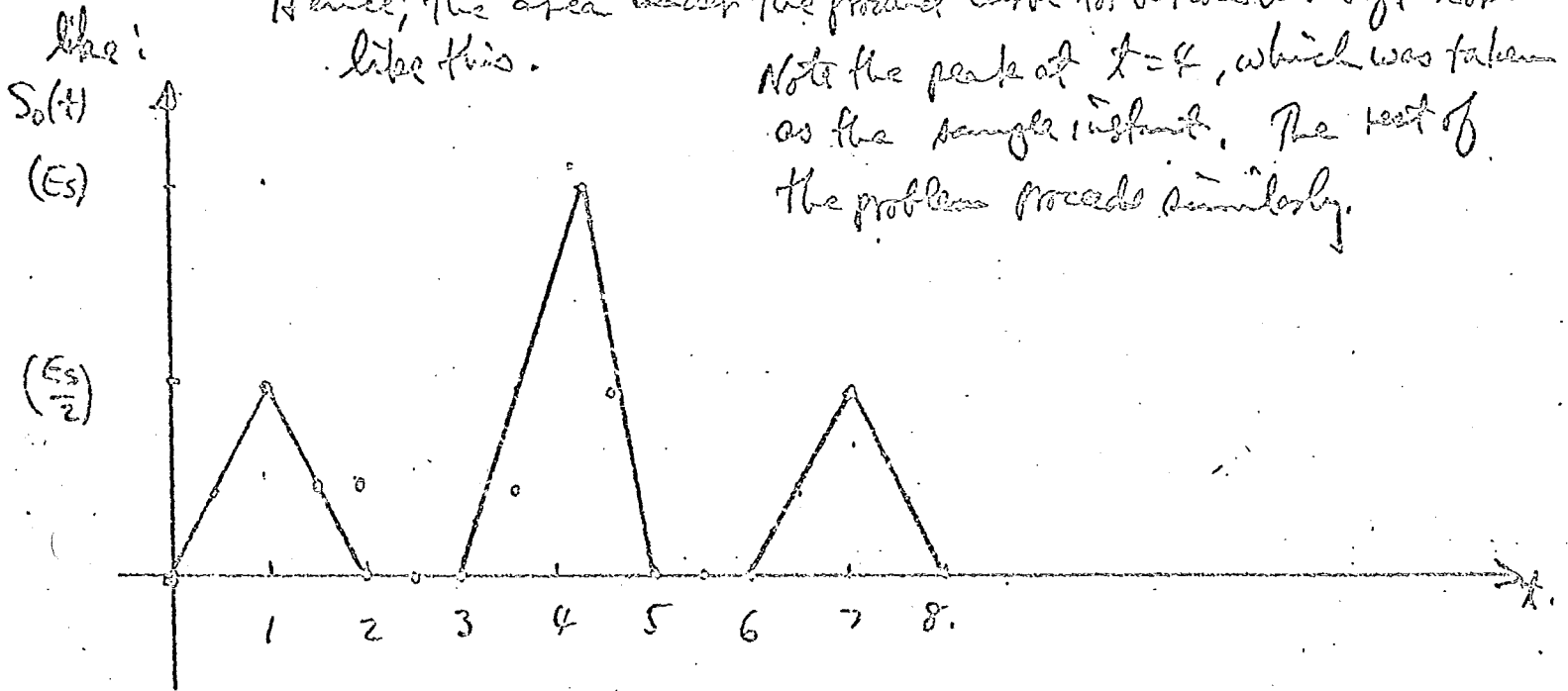
(6)

(3) (4, 4). Match the input at $T=4$ sec. Then $h(t) = S_1(4-t)$.

() $S_0(t) = \int_{-\infty}^{\infty} S_1(4-t+\tau) S_1(\tau) d\tau$. We match $S_1(4-t+\tau)$ for various values of t .



Hence, the area under the product curve for various values of t looks like this. Note the peak at $t=4$, which was taken as the sample instant. The rest of the problem proceeds similarly.



①

(4). (4.18). (a) The area under the square of each signal is the same for each set, namely E_s .

(b) The union bound depends on the ratio $\frac{|\bar{s}_i - \bar{s}_k|}{\sqrt{2N_0}}$ (eqn. 4.110).

For the signals of set (b), $\frac{|\bar{s}_i - \bar{s}_k|}{\sqrt{2N_0}} = \sqrt{\frac{E_s}{N_0}}$ for every pair $i-k$.

Hence, the average is also $\sqrt{\frac{E_s}{N_0}}$.

For the signals of set (a): $\frac{|\bar{s}_i - \bar{s}_k|}{\sqrt{2N_0}} = \sqrt{\frac{E_s}{N_0}}$ for $i-k = 1-2, 3-$

$\frac{|\bar{s}_i - \bar{s}_k|}{\sqrt{2N_0}} = \sqrt{\frac{E_s}{2N_0}}$ for $i-k = 1-3, 1-4,$
 $2-3, 2-4.$

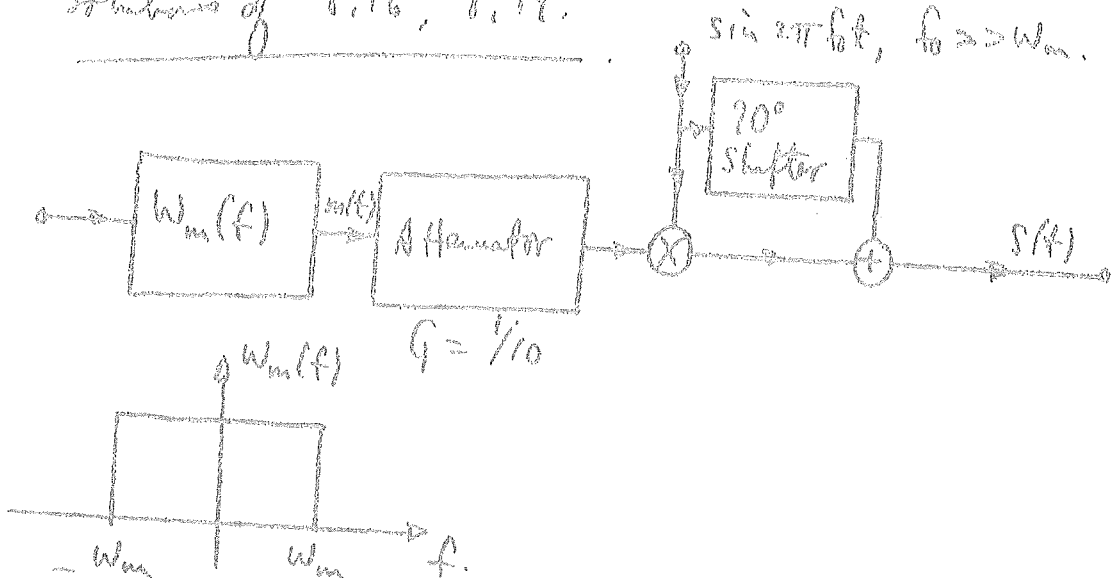
Thus, the average $\frac{|\bar{s}_i - \bar{s}_k|}{\sqrt{2N_0}}$ for set (a) is approximately

$$\sqrt{\frac{E_s}{(1.8)N_0}}$$

If it were $\sqrt{\frac{E_s}{2N_0}}$ we would have exactly a 3-dB degradation in performance (the ^{signal} energy would be effectively halved). Thus, because "1.8 is close to 2" we have approximately 3-dB poorer performance with the signals of set (a) than (b).

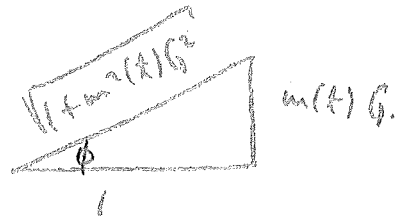
Solutions of P. 16, P. 19.

(8.16)



$$\begin{aligned}
 (a) \quad S_m(t) &= m(t) \cdot G \sin 2\pi f_0 t + \sin(2\pi f_0 t + 90^\circ) \\
 &= m(t) G \sin 2\pi f_0 t + \cos 2\pi f_0 t \\
 &= \sqrt{(1 + m^2(t) G^2)} \cos(2\pi f_0 t - \varphi)
 \end{aligned}$$

$$\varphi = \tan^{-1}(m(t)G)$$



For $|m(t)G| \ll 1$,

$$\tan^{-1} G m(t) \approx G m(t)$$

$$\text{and } \sqrt{1 + m^2(t)G^2} \approx 1$$

$$S_m(t) = \cos(2\pi f_0 t - G m(t)) \quad \text{— Phase modulation}$$

(b) For F.M. : $S_m(t) = A T e^i \cos 2\pi (f_0 t + W \int m(t) dt)$

For PM:
$$S_m(t)_{PM} = A\sqrt{2} \cos 2\pi (f_c t + W_m \int m'(t) dt)$$

$$= A\sqrt{2} \cos 2\pi (f_c t + W_m u(t)).$$

For sinusoidal signals, $m(t) = \begin{cases} \sin \\ \cos \end{cases} (2\pi W_m t)$, and in order for β_{PM} correspond in meaning to β_{FM} we must have

$$S_m(t)_{FM} = A\sqrt{2} \cos 2\pi (f_c t + \beta_{FM} \begin{cases} \sin \\ \cos \end{cases} (2\pi W_m t)).$$

$$S_m(t)_{PM} = A\sqrt{2} \cos 2\pi (f_c t + \beta_{PM} \begin{cases} \sin \\ \cos \end{cases} (2\pi W_m t)).$$

But $\beta_{FM} = \frac{W_1}{W_m}$ and $\beta_{PM} = 2\pi W_m$.

For SSB, $\beta = \frac{f}{2\pi} \times 2\pi = f \approx \frac{1}{10}$

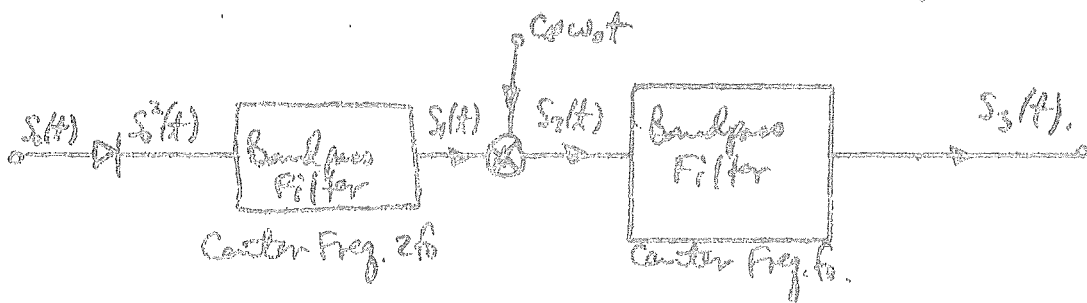
(8) A better reason for calling $2\pi W_m$ the modulation index stems from 8.15/6 wherein the mean-square output noise of the PM system is

$$\overline{n^2(t)} = \frac{1}{(2\pi W_m)^2} \cdot \frac{N_0}{2E_s}. \text{ Thus,}$$

$2\pi W_m$ plays the same role in PM as does β in FM (8.14/6).

Thus, $2\pi W_m$ is the modulation index of a PM system.

(c)



$$S_0(t) = \cos 2\pi (f_0 t + \varphi), \quad \text{where } \varphi = \int \omega_0 dt.$$

$$= \cos (\omega_0 t + \beta_0 \sin t).$$

$$S_0^2(t) = \frac{1}{2} [1 + \cos(2\omega_0 t + 2\beta_0 \sin t)].$$

$$S_1(t) = \frac{1}{2} \cos(2\omega_0 t + 2\beta_0 \sin t).$$

$$S_2(t) = \frac{1}{4} [\cos(3\omega_0 t + 2\beta_0 \sin t) + \cos(\omega_0 t + 2\beta_0 \sin t)].$$

$$S_3(t) = \frac{1}{4} \cos(\omega_0 t + 2\beta_0 \sin t).$$

$$\therefore \beta_1 = 2\beta_0 = 4\pi G.$$

In general, $\beta_K = 2^K \beta_0$, where $K = \#$ of stages.

(d). Required: $\overline{w^2(t)} = 10^{-8}$.

Given: $G = 1/10$, $\omega_m = 3,000 \text{ Hz}$, $N_0 = 10^{-11} \text{ J}$, $P_s = 10^{-6} \text{ W}$.

For max. likelihood reception of PM signals,

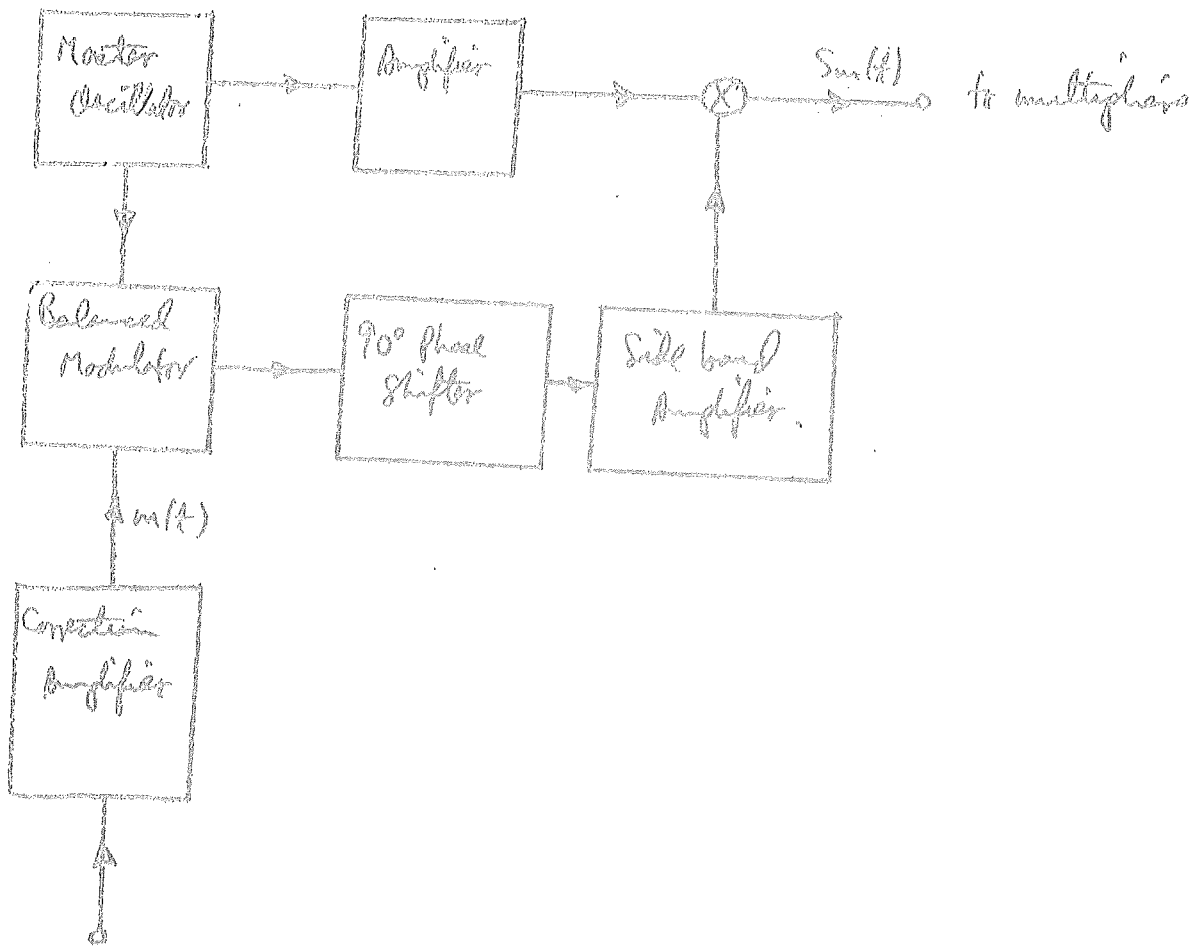
$$\overline{w^2(t)} = \frac{1}{\beta_K^2} \cdot \frac{N_0}{2E_s} \quad (\text{8.156.6 or 8.157c}).$$

From 8.158, $E_s = \frac{P_s}{2\omega_m} = \frac{10^{-6}}{6000} = 1.67 \cdot 10^{-10} \text{ J}$.

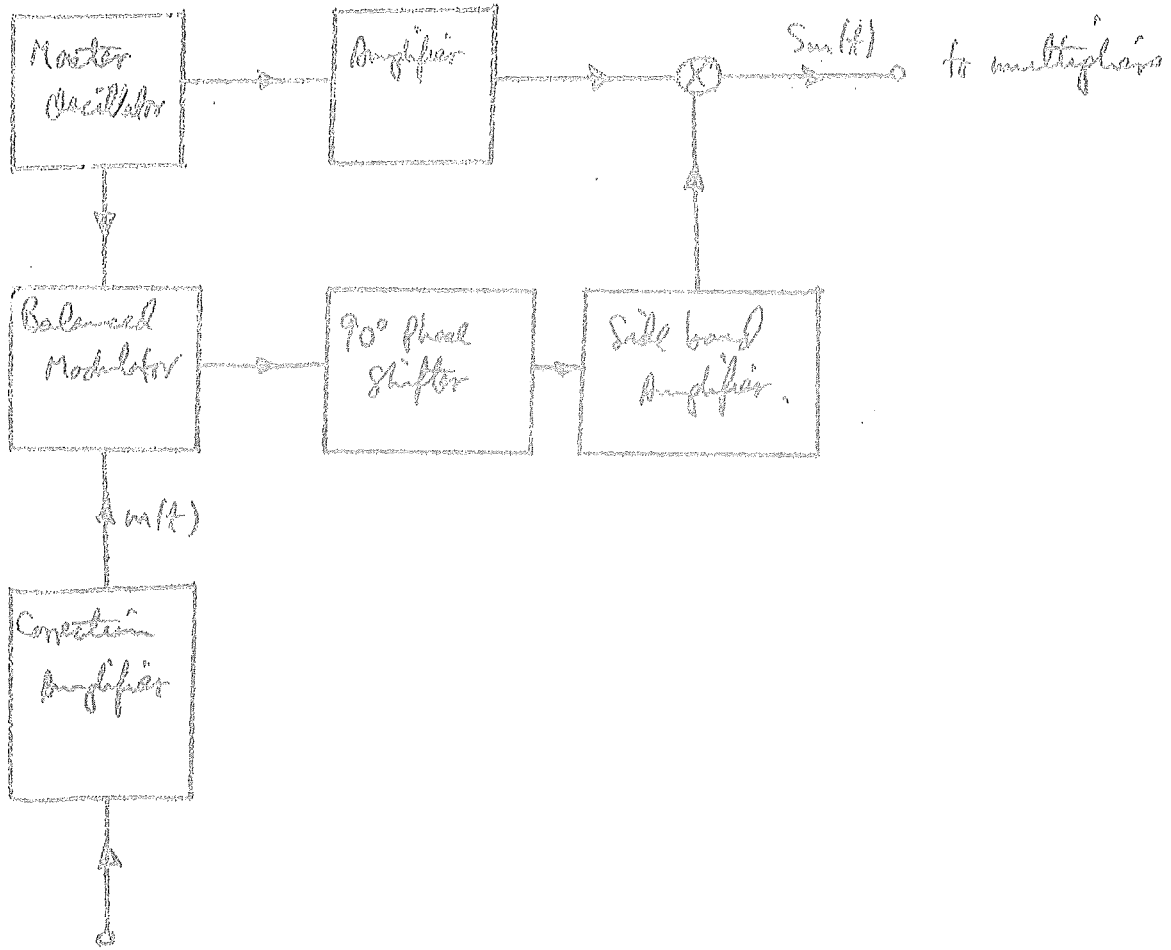
$$\therefore 10^{-8} \approx \frac{1}{\beta_K^2} \cdot \frac{10^{-11}}{1.67 \cdot 10^{-10}} = 0.06 \cdot \frac{1}{\beta_K^2} \Rightarrow \beta_K^2 \geq \frac{6 \cdot 10^{-2}}{10^{-8}} = 600.$$

$$\therefore \beta_K \approx 25, \text{ or } 2^K (0.628) \approx 25 \Rightarrow 2K \approx 40 \text{ or } \boxed{K = 6 \text{ stages}}$$

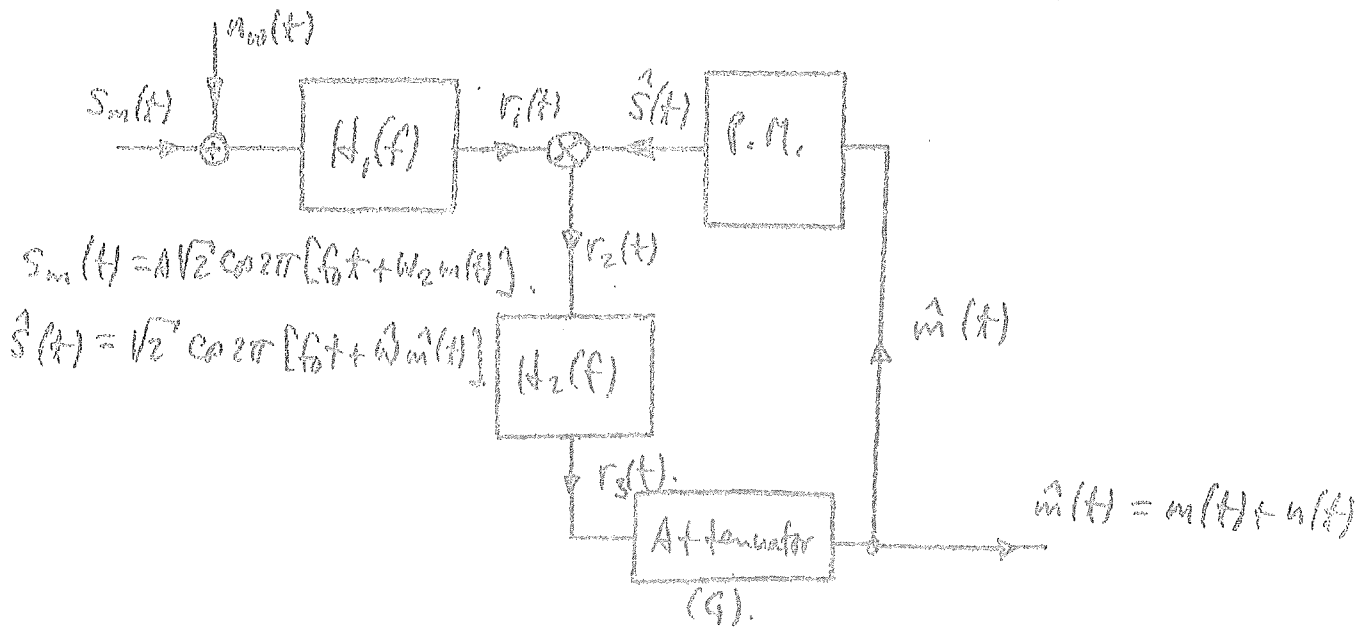
(c). Armstrong's F.M. system.



(e). Armstrong's FM System.



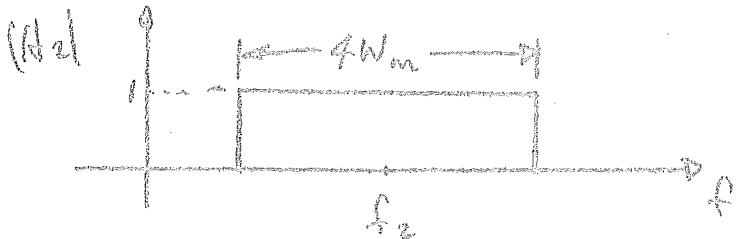
(8.19)



(a) $s_m(t) = B \cos(\omega_0 t + \theta)$

$\hat{s}(t) = B \cos(\omega_0 t + \hat{\theta})$

$r_2(t) = S(t) \hat{s}(t)$ (note $\omega_0(t) = 0 \Rightarrow r_1(t) = s_m(t)$)
 $= \frac{BB}{2} [\cos(2\omega_0 t + \theta + \hat{\theta}) + \cos(\theta - \hat{\theta})]$



H_2 must be narrow enough to block the carrier ($2\omega_0$) but wide enough to pass $\cos(\theta - \hat{\theta})(t)$. Thus $H_2(f)$ must be as shown above.

$$r_3(t) = \frac{BB^2}{2} \cos[\theta(t) - \theta'(t)], \text{ and } \hat{w}(t) = \frac{BB^2 G}{2} \cos[\theta(t) - \theta'(t)].$$

$$= \frac{G BB^2}{2} \cos[\omega_2 m(t) - \omega \hat{w}(t)].$$

$$= \frac{G BB^2}{2} \sin\left[\frac{\pi}{2} + \omega_2 m(t) - \omega \hat{w}(t)\right].$$

$$\approx \frac{G BB^2}{2} \left[\frac{\pi}{2} + \omega_2 m(t) - \omega \hat{w}(t)\right], \text{ if the argument of the sine function is small, i.e.,}$$

$$\hat{w}(t) \approx \frac{\pi}{2} + \omega_2 m(t).$$

Hence, for small "linear approximation", we have

$$\hat{w}(t) \left[1 + \frac{G BB^2 \omega}{2}\right] = \frac{G BB^2}{2} \left[\frac{\pi}{2} + \omega_2 m(t)\right].$$

and

$$\hat{w}(t) = \frac{\frac{G BB^2 \omega_2}{2} m(t) + \frac{G BB^2 \pi}{4}}{1 + \frac{G BB^2 \omega}{2}}$$

Upon setting $G BB^2 = \frac{2}{\omega_2 - \omega}$ or $G = \frac{2}{BB^2(\omega_2 - \omega)}$

we get $\hat{w}(t) = m(t) + K$, where K is a constant. Hence, up to an additive constant (which can be eliminated by a differentiation)

$$\hat{w}(t) = m(t).$$

For simplicity let $m(t) = 1$. Then

$$r_1(t) = \cos(\omega t) + u_1(t)$$

$$u_1(t) = u_c(t) \sqrt{2} \cos \omega t + u_s(t) \sqrt{2} \sin \omega t.$$

$u_c(t)$ is the in-phase component of $u_1(t)$, and $u_s(t)$ is the out-of-phase component of $u_1(t)$.

$$r_1(t) = (A + u_c(t)) \sqrt{2} \cos \omega t + u_s(t) \sqrt{2} \sin \omega t.$$

$$= a(t) \sqrt{2} \cos(\omega t + \varphi(t)).$$

$$\varphi(t) = \tan^{-1} \frac{-u_s(t)}{A + u_c(t)} \approx \frac{-u_s(t)}{A} \quad \text{for weak-noise,}$$

$$a(t) = \left\{ [A + u_c(t)]^2 + u_s^2(t) \right\}^{1/2} \approx A.$$

$$r_2(t) = \hat{s}(t) \cdot r_1(t) = \frac{\sqrt{2} a(t) \sqrt{2}}{2} \left[\cos(2\omega t + \varphi(t) + \hat{\theta}(t)) + \cos(\varphi(t) - \hat{\theta}(t)) \right].$$

$$= a(t) \left[\cos(2\omega t + \varphi(t) + \hat{\theta}(t)) + \cos(\varphi(t) - \hat{\theta}(t)) \right].$$

$$= A \left[\cos(2\omega t + \varphi(t) + \hat{\theta}(t)) + \cos(\varphi(t) - \hat{\theta}(t)) \right].$$

$$r_3(t) = A \cos(\varphi(t) - \hat{\theta}(t)).$$

$$u_2(t) = \int A \cos(\varphi(t) - \hat{\theta}(t)).$$

$$u_2(t) = m(t) + u_1(t) = u_1(t),$$

(because $m(t) \equiv 0$, by assumption).

hence,

$$u(t) = GA \cos(\varphi(t) - \theta(t)).$$

$$\approx GA \left(\frac{\pi}{2} + \varphi(t) - \theta(t) \right)$$

$$= GA \left(\frac{\pi}{2} + \left(-\frac{u_s(t)}{A} \right) - 2\pi \hat{\omega} u \right)$$

$$= GA \left(\frac{\pi}{2} - \frac{u_s(t)}{A} - 2\pi \hat{\omega} u \right)$$

$$\therefore u(t) = \frac{GA \cdot \frac{\pi}{2} - G u_s(t)}{1 + 2\pi \hat{\omega} GA}$$

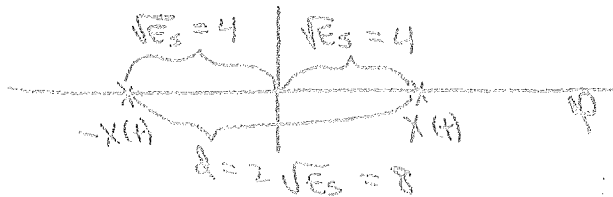
(4.7) Given $\int_0^T x^2(t) dt = \int_0^T y^2(t) dt = 16 \text{ J}$,
 and $\int_0^T x(t) y(t) dt = 0$

This information says (1) The total energy in $x(t)$ = the total energy in $y(t)$ = $E_s = 16 \text{ J}$.

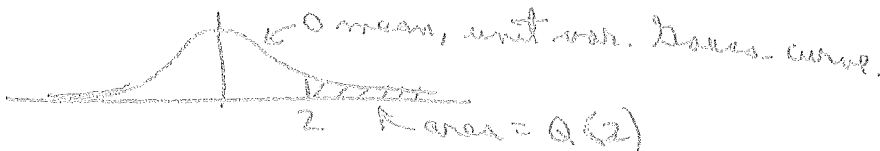
(2) $x(t)$ and $y(t)$ are orthogonal

Assuming equally likely messages, and $L_n(f) = \frac{\eta_0}{2} = 4 \frac{\text{watt-sec}}{\text{cycle}}$:

(a) Let $x(t)$ and $-x(t)$ be represented in signal space as:



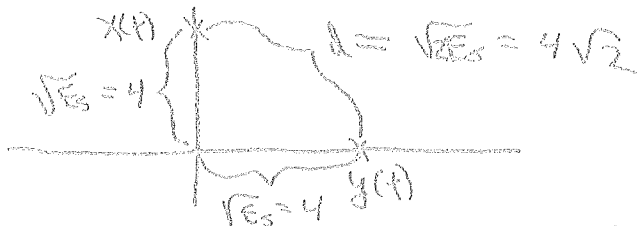
$P[\epsilon] = \frac{1}{2} P[\epsilon | x(t)] + \frac{1}{2} P[\epsilon | -x(t)] = Q\left(\frac{d}{\sqrt{2\eta_0}}\right) = Q\left(\frac{8}{\sqrt{2(8)}}\right)$



$= Q(2)$

From table books: $P[\epsilon] = Q(2) = .0227$

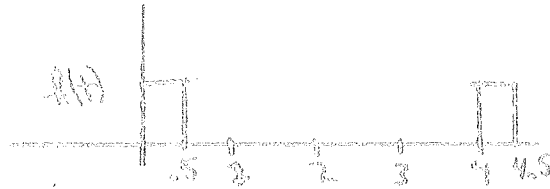
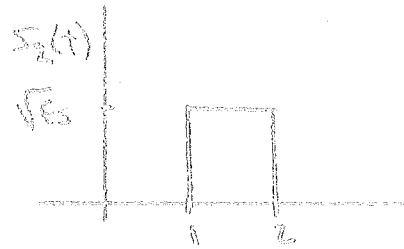
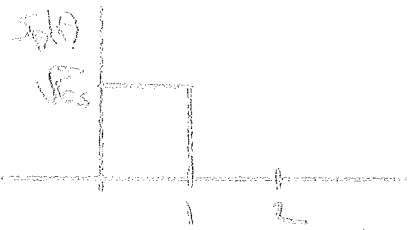
(b) $x(t)$ and $y(t)$ are represented in signal space as:



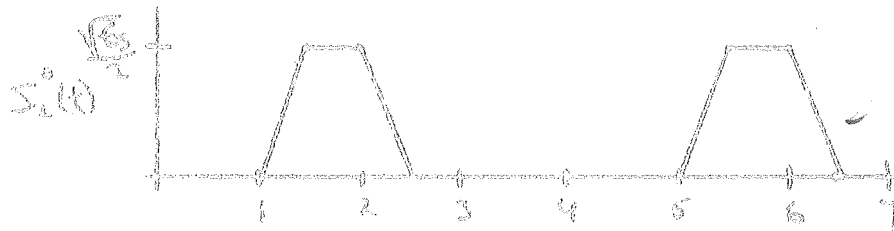
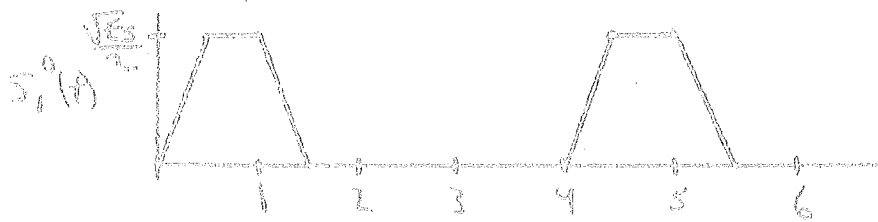
as before, $P[\epsilon] = Q\left(\frac{d}{\sqrt{2\eta_0}}\right) = Q\left(\frac{4\sqrt{2}}{\sqrt{2(8)}}\right) = Q(\sqrt{2})$

From table books: $P[\epsilon] = Q(\sqrt{2}) \approx .0788$

(1)



$S_1^o(t) = S_1(t) * h(t)$ and $S_2^o(t) = S_2(t) * h(t)$ (shown below)



Now $P\{E\} = Q\left(\frac{d}{\sqrt{2E_b}}\right)$ where d is the distance between S_1^o and S_2^o in an orthogonal space. This distance can be written in terms of the energy of the difference between $S_1^o(t)$ and $S_2^o(t)$ as follows:

$$d = \sqrt{\int_{-\infty}^{\infty} (S_1^o(t) - S_2^o(t))^2 dt}$$

